C SANCELLATION)

WORK ORDER JOHN SEVIER FOSSIL PLANT - CONSTRUCT FLY ASH POND ORDER NO. ____510633-20656

IN AREA J

AUTH, NO.

SYMBOL SE-27

GIVE DETAILS OF CHANGES IN THE COMPLETED WORK FROM THAT AUTHORIZED BY THE WORK ORDER OR JOB ORDER, LIST ANY AUTHORIZED WORK LEFT UNFINISHED, INDICATE THE ORGANIZATION RESPONSIBLE FOR FINAL COMPLETON OF SUCH UNFINISHED WORK, AND GIVE REFERENCE TO JOB ORDER OR FORM 1663 AUTHORIZING SAME.

Complete. This superseding completion notice is submitted to provide an overrun explanation for the work order.

The following conditions contributed to the overrun on the construction of Ash Pond "J".

- 1. Underestimated the amount of dirt needed to build dikes and the shortage of suitable dirt in the excavation.
- 2. Ran into layer of shale in the bottom of excavation which had to be sealed with clay.
- 3. A portion of the river bank slid into the river making it necessary to rip-rap the river bank for several hundred feet.
- 4. Leaks developed in the discharge culverts which had to be partially uncovered and the joints sealed.
- 5. A change in design criterion which made it necessary to change the dike configuration along Dodson Creek.

cc: Plant Accounting Branch, 278 HB-C Cost and Budget, 719 CBB-C Don G. Holden, 819 EB-C

SHOW BELOW DATES PERTAINING TO THE WORK ORDER AS A WHOLE. IF MAJOR PHASES OF THE WORK OR MAJOR ITEMS OF EQUIPMENT WERE PLACED IN SERVICE PRIOR TO WORK CRDER COMPLETION. SUCH DATES SHOULD BE LISTED IN THE SPACE ABOVE.

	DATE	PROVAL SIGNATURES	DATE SIGNED
construction 9/83	COMPLETED6/85	B. B. Street	8/29/85
READY FOR SERVICE ON	6/85		
PLACED IN OR REMOVED FROM SERVICE ON	6/85		
ACCEPTED BY OPERATING ORGANIZATION ON	6/85		

JOHN SEVIER STEAM PLANT ASH DISPOSAL AREA SOILS EXPLORATION AND TESTING EN DES SOILS SCHEDULE NO. 6.2



Knoxville, Tennessee

TENNESSEE VALLEY AUTHORITY
DIVISION OF CONSTRUCTION
SINGLETON MATERIALS ENGINEERING LABORATORY

Est. No. 82-19
Rev. No. R2

0. P. Thornton

TENNESSEE VALLEY AUTHORITY OFFICE OF ENGINEERING DIVISION OF ENGINEERING PROJECTS

DSP '84 1 2 1 7 0 0 1 ENGINEERING ESTIMATE OF FACILITY COST

Date December 14, 1964
PROJECT: _John Sevier Steam Plant
FEATURE: New Fly-Ash Disposal Area J
PURPOSE AND SCOPE: _Estimate the total project cost to move the centerline of the dike
along Dodson Creek on the north end of ash pond J and to complete the riverbank dike
adjacent to the spillway outfall. This revision is based on actual costs through
October 1984 with remaining field construction based on OC estimate number CSB 85-030.
ESTIMATE REQUESTED BY 0. P. Thornton DATE October 31, 1984
REFERENCE MEMO (IF ANY) 0. P. Thornton to W. D. Hall, 11/27/84 (FEP 841127 004)
Cost Estimate Request (if any) FEPJSF84-1002 (FEP 841031 004)
CLASSIFICATION OF ESTIMATE
1. Order of MagnitudeVariable accuracy usually based on previous similar cost information.
2. Preliminary EstimateAccuracy insufficient for budgeting, but a guide to further interest.
X 3. Budget or Authorization EstimateSuitable for budgeting.
4. Detailed EstimatePrepared from complete engineering specifications,
drawings, and site surveys.
5. Contract Bid Estimate - For purchase requisition or bid award evaluation.
6. Other -
ESTIMATED COST: \$ 3,613,700
COMMENTS: Total Engineering and Construction estimate based on Engineering starting in
October 1981 and completed in April 1985, and based on Construction starting in January
1982 and completed in April 1985. Excludes other Power organizations and other TVA organization expenses and overheads.
Attachment: Attachment:
cc: C. Bonine, Jr., 12-108 SB-K D. J. Cowser, 12-111 SB-K Submitted: D. C. Ritchey
R. G. Domer, W11A6 C-K D. C. Ritchey
W. D. Hall, W12C62 C-K
MEDS, W5B63 C-K Reviewed: // Review
O. P. Thornton, 102 SPT-K W. D. Hall
Annovade of the said of



Actual Expenditures Thru October 1984

Estimating Work Remaining

			•	Eqpt/					East/		`.
Account	Material	受	Labor Amount	Other	Total	Material	MH	Labor Amount	Other	Total	Total
-0 Gradework	\$ 54.325	5 35,375	\$ 564 605	8 815 510	61 434 440		ç	6	•		
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-2 Guardrail	5,800		35	20	7 855	1	!			!	46,465
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	41,115		7,590	7,740	56,445	1	}		}		104,300
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	8,855	5 95	1,395	290	10,840		1	1	1	;	078.01
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-64 Culvert Pipe - Access Road		5 1	06.1	010	1,500	3/8,200	1,940	30,655	77,190	(486,045)	487,845
-65 Railroad Crossing	i	1	1	1	i	7,330	978 876	11,150	7,720	26,200	2,300
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-81 Construction Facilities -80 Field General Expense	15,800	11,857 13,872	190,600	130,690	337,090		1,345	20,000	26,000	46,000	383,090 392,120
Total Field Construction	\$165,790	70,265	\$1,140,090	\$1,162,605	\$2,468,485	\$395,725	9,078	\$138,390	\$218,820	\$752,935	\$3.221.420
Rngineering											
Soils Investigation					1					200	006. 2
Other					79,600					23,100	102,700
Subtotal Engineering and Construction	c				£70 00E						
					44,340,003					\$781,335	\$3,32%,420
General Engineering and Construction Expense Contingency					101,915					31,265	133,180
Construction Engineering					11					148,600	148,600
Total Danks and									`	()	7,300
total bugineering and construction					\$2,650,000				J	\$963,700	\$3,613,700

and and construction based on engineering started in October 1981 and completed in April 1985; construction started in January 1982 and completed April 1985. Excludes other Power organization expenses and overheads.

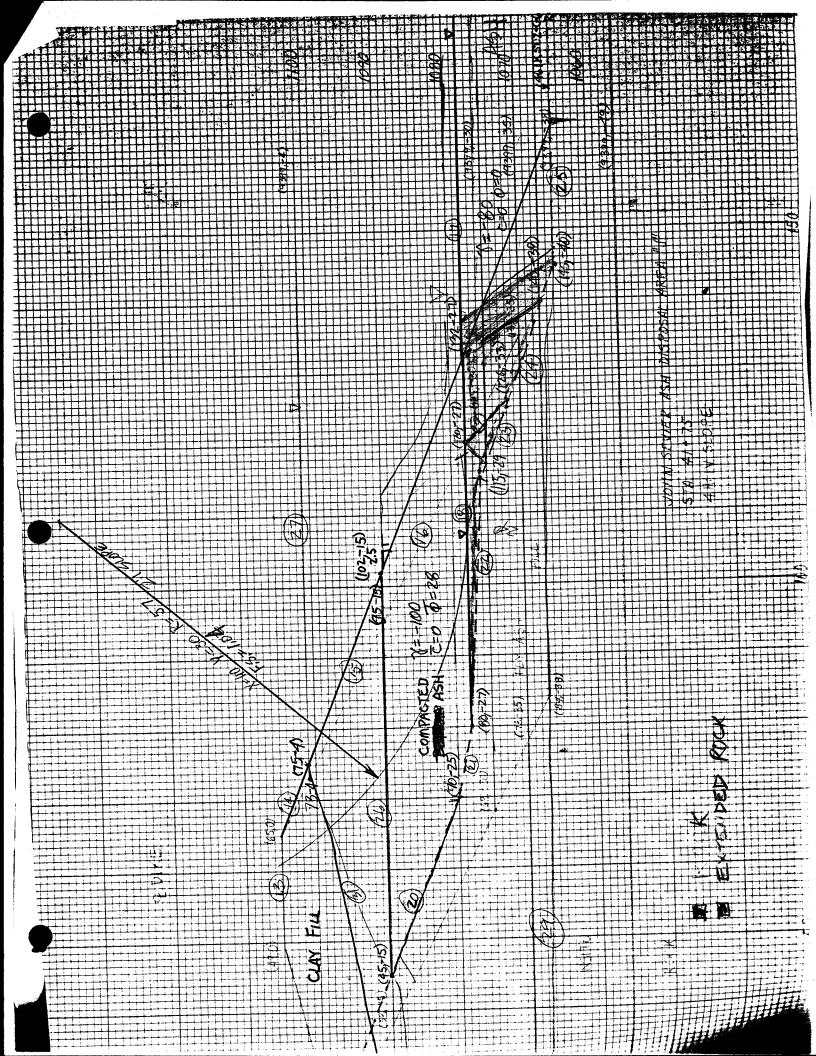
DSP December 14, 1984 J64349.4

A Principally prepared by C. L. Toney, extension 7134.

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Francisco 😽	
F M. H. MILLER	Det 25, 84
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Fold here for return	Knox Nor.
NAME /	EXTENSION
R ADDRESS ADDRESS	
O ADDRESS	Chatta M. S. Knox Nor.
UNCHECKED RESULTS:	
ROCK TOE NEEDED	
Z:1 SLOPE	
$\frac{\text{COMPACTED ASI} \Phi = 28^{\circ} FS = 1.}{1.5}$	04
$-\frac{11}{4} = 30^{\circ} = 10^{\circ}$	09
2.5:/ SLOPE	
COMPACTED ASH $\phi = 28^{\circ}$ FS	= 1.24
$\phi = 30^{\circ} F_{5}$	= 1.31
RECOMMEND 2.5:1:3	SLOPE
ON INSIDE OF DIKE.	
JOHN SEVIER S.P A	SH POND "J"
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TVA 45D (OS-9-80) INTEROFFICE MAILING SLIP



JOHN SEVIER ASH DISPOSAL AREA "J" STA. 41 + 75 (DODSON CREEK)

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John Sevier S.P. Ash Pand J. Dodson Creek

Summary. Bottom Ash Properties -

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Compacted Bottom Ash.	- 1 " - 1 " - 1 1 1	120 pcf		1200 958 0.615f	20	0	33
							8
Dumped Bottom Ash.		Hopef	48 pcf	600 PSF 0-3+sf	15	0	28
				100 ^{PSF}			
Consolidate Fly ash	85	95	33	0.05	15°	0	240.
V. LOOSE FLY ASH	65	70_	8	0	0	0	0

SHEET	1	OF	

COMPUTED	DATE	

CHECKED ______DA

FACTOR OF SAFETY AT STA. 41+75 (DODSON CREEK) WITH NORMAL PHREATIC SURFACE

DESCRIPTION OF REPAIR	FACT	OR OF SAFE	ſΥ
	R	R	
RIPRAP @ EL. 1076	0.94	0.96	
RIPRAP @ EL. 1080 9. FAILURE AT TOP OF RIPRAP	1.04	1.06	
b. FAILURE AT BOTTON OF RIPRAP	m 1.06		
RIPRAP@ EL. 1080; WITH 10'BERM @ EL.	1065		
a. FAILURE AT TOP OF RIPRAP	1.14	1.12	
b Failure at Bottom OF RIPRAP	1.15	1.27	
C. FAILURE ABOVE JRIPRAP	<u>-</u>	1.04	
RIPRAP@EL.1080; WITH 10' BERM@EL.10	0 70		
G. FAILURE AT TOP	1.17	1.12	
120,000 B. FAILURE AT BOTTOM OF RIPRAP	1.21	1.31	
+ 20% 144,000 C. FAILURE ABOVE RIPRAP		1.04	

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1- Cohesionless fine silty sand. 2. Unique type of behavior in triaxial testing.

Saturated sarplessiquified during the triaxial R test (very low shear strugther values) 3. Appears to be a dispersive material.

4. High potential for slongling; erosion and dispersion 5 in Recommend to provide a protective cover e.g, 3 tide compacted day cover, decilbonage BW-6051 (Small) roller to compact the clay, 1 (24 wide) BW-35 (15" wide) Justifications for placing earth cover on face of ash fill per S.B. Ahmed. 1/85
PAP

O. P. Thornton, Project Manager, Fossil Design Projects, 102 SPT-K (2)

John A. Raulston, Chief Nuclear Engineer, W10C126 C-K

JOHN SEVIER STEAM PLANT - ASH POND J - SOILS INVESTIGATION ON ASH MATERIAL - EN DES SOILS SCHEDULE 6.3

Testing of bag samples taken from the ash disposal areas as directed by Fossil Engineering Project (FEP) personnel has been completed. In addition to the requirements outlined in your memorandum of October 30, 1984, to W. H. Childres, saturated R and direct shear tests were performed as requested by the Geology and Geotechnical Engineering Group (GGEG) staff.

Index tests (ASTM D 4318), particle-size analyses (ASTM D 422), standard compaction tests (ASTM D 638), and saturated triaxial R tests with pore pressure measurements were performed on bag samples of three different types of ash. Only two of the three samples were chosen for direct shear tests by the CGEC staff. Specimens for triaxial R and direct shear tests were remolded at 95 percent maximum dry density and at 3 percent below optimum water content. Test results are shown in the attachments. The apparent triaxial shear strength parameters varied from c = 0 tsf and $\phi = 11.4^{\circ}$ to c = 0.08 tsf and $\phi = 20.5^{\circ}$. The effective shear strength parameters ranged from c = 0.03 tsf and $\phi = 17.3^{\circ}$ to c = 0.28 tsf and $\phi = 28.6^{\circ}$. The direct shear strength parameters are very similar on the two types of ash tested, being c = 0.13 tsf and $\phi = 31.2^{\circ}$ for pond J ash and c = 0.07 tsf and $\phi = 31.9^{\circ}$ for ash from the southeast bank.

It should be noted that during triaxial shearing on the remolded ash specimens from pond J and the southeast bank, the deviator stress reached its peak very early and then dropped constantly as the developed pore pressure increased continuously to a value equal to the applied confining pressure. It was apparent that an initial liquefaction occurred and the ash exhibited no resistance to deformation at the final stages of static loading. In view of these critical phenomena developed on the ashes of pond J and the southeast bank, the shear strength parameters based on the

SUBJECT ASH DISPOSAL AREA J REPAIR PROJECT JSF

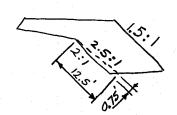
MUANTITY ESTIMATE

MUN DATE 10/29/84 CHECKED BY POP COMPUTED BY MAN

DATE 10/29/84

RIPRAP

$$0.15$$
 3.39
 3.24
 3.225
 $=$
 322.5
 $5F$
 6.60
 3.21



0.75 (12.5)/2 = 4.6875 SF

$$(322.5 - 4.6875)(30/2 + 330 + 40/2) = 116,001.6$$
 CF

$$116,001.6 / 27 = 4,296.35 CY$$

$$4296.35(1.8) = 7,733.4$$
 TONS & 7730
INSIDE AONA TONS & 7730
7730 + 36,200 = 43,930

A 44,000 TONS (TOTAL)

CRUSHED STONE SURFACING
$$(46(0.5))(365) = 8,395 \text{ CF}$$

1000 TONS 2

SUBJECT ASH DISPOSAL AREA "J" REPAIR PROJECT JSF

QUANTITY ESTIMATE

COMPUTED BY MAH DATE 10/29/84 CHECKED BY ROA DATE 10/19/84

COMPACTED ASH FILL

715 (600) = 429,000 CF

429,000 ÷ 27 = 15,888.9 CY-

15,888.9 ÷ 0.75 = 21,185 CY

21,200 CY

JOHN					. 4:							
ASH DIS	ROSAL	- ARE	EA "J"	REAL	YIRS					•		
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JOHN SEVIER STEAM PLANT

ASH DISPOSAL AREA "J"

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TVA 44 (08-4-46)

UNITED STATES GOVERNMENT

Memorandum

TENNESSEE VALLEY AUTHORITY

: C. C. Schonhoff, Director of Fossil and Hydro Power, 720 EB-C

FROM : Charles Bonine, Jr., Hanager of Construction, 12-108 SB-K

DATE : November 16, 1984

84111670293

SUBJECT: JOHN SEVIER STEAM PLANT - ASH POND "J"-SLOPE STABILIZATION MODIFICATIONS

R. G. Domer's September 12 memo to you (PEP 840912 002) outlines additional work to the ash pond dikes for slope stability improvements. These costs are to be charged to the original work order. A copy of Mr. Domer's memo is attached for your ready reference. Due to schedule delays, scope changes, and inclement weather the original work order is already significantly "overrun" and we thought it might be well to bring everyone up to date on this activity. Outlined in the following paragraphs is a brief chronology of this project.

Cost estimate number 82-19 Rl, dated March 2, 1982, authorized \$1,369,000 to construct ash pond J during calendar year 1982. The original scope indicated that the 486,000 cubic yards of fill material required for the dike would be available from a borrow area inside the dike and another borrow area outside the dike and across the Southern Railway railroad. Each area was to contain approximately 50 percent of the required material. Both of these areas required permits from agencies outside TVA in order to obtain the necessary material. The area inside the pond required a 404 permit before excavation could continue below elevation 1075. The area outside the dike required a permit from Southern Railway for a temporary crossing of the railroad.

Construction actually started on June 21, 1982, within a few days after project authorization. The 404 permit was received from the Corps of Engineers on October 7, 1982, and by November 25, 1982, all material inside the pond had been expended. A total of 200,000 cubic yards of fill had been placed for the dike. Production was slowed during this period due to delays in obtaining the 404 permit and 23 days of inclement weather.

All work was suspended on November 25, 1982, pending approval of the permit to cross the railroad. After the permit was secured, work was resumed on December 7, 1982. Earthwork was completed on September 30, 1983, with 516,267 cubic yards being placed. During this period, fill placement was suspended 70 days due to inclement weather.

Since only 200,000 cubic yards of fill were available inside the dike, approximately 316,267 cubic yards were hauled from the area across the railroad. This resulted in additional haul time and an expansion of this borrow area beyond the original limits. Additional material was also required for a cutoff trench to correct seepage underneath the dike. Following is a tabulation of the additional material handled:



Buy U.S. Savings Bonds Regularly on the Payroll Savings Plan

C. C. Schonhoff November 16, 1984

JOHN SEVIER STEAM PLANT - ASH POND "J"-SLOPE STABILIZATION MODIFICATIONS

	Original Estimate	Actual (CY)	Additional Material
Dike fill	486,000	516,267	30,267
*Topsoil Stripped and			
Stockpiled	16,133	63,000	46,867
Topsoil Removal	6,133	63,000	46,867
Fill for Seepage	0	50,000	50,000
Total			174,001 CY

*Double handling due to delay in railroad crossing permit.

Construction on work items not in the original scope was started in September 1983 and completed in January 1984. These items include: Polly's Branch relocation, a turnaround at the outfall pipes, a walkway to the out-fall pipe, and a floating skimmer. Mobilization was begun on March 27 for emergency repairs to ash pond J. This emergency work consisted of construction of an anti-seepage collar around one of the spillway discharge pipes, grouting of leaking joints in one discharge pipe, and replacement of riprap at the outfall of the discharge pipes. All of this work was completed on Hay 30, 1984.

Attached for your information is a summary of actual costs to date and the estimated additional costs for the stabilization work.

GF: HAO Attachment

cc: Frank Van Heter, 10-103 SB-K MEDS. WSB63 C-K

DH4307.H1



Paul Wade, Assistant Director of Fossil and Hydro Power (Fossil), 720 EB-C

Jack T. Thompson, Chief, Technical Services Branch, 705 EB-C

SEP 24 1984

JOHN SEVIER FOSSIL PLANT - ASH DISPOSAL PROGRAM

References: 1. My memorandum to C. C. Schonhoff dated June 3, 1984 with attachment on the above subject (M53 840530 912)

2. Letter from Leo H. Gerbus to the Land Branch dated August 23, 1984 regarding the sale of land near John Sevier (M47 840828 403)

33.

A meeting was held at John Sevier on August 14, 1984 to discuss plans for ash disposal addressing immediate and long-range needs. Those in attendance at the meeting represented the Divisions of Engineering Design (EN DES) and Fossil and Hydro Power (F&H PR).

To begin the meeting, representatives of EN DES presented total costs for additional repairs necessary to give the pond J dikes an acceptable factor of safety. To date, \$105,000 has been spent on repairs. In order to meet acceptable safety standards, an additional \$674,000 will have to be spent on repairs to pond J (\$509,000 for riprap of riverbank and \$165,000 for constructing a 4:1 slope on the dike at Dodson Creek). After considerable discussion of these repair figures, F&H PR agreed that this work is necessary; and that these repairs to pond J should be charged to the original work order.

At this point in the meeting, attention was directed toward immediate plans to support ash disposal needs. Presently, we have a usable ash capacity of 665,000 tons (400,000 tons in pond 2 and 265,000 tons in pond J). The final usable volume for pond J is 500,000 tons, which is 300,000 tons less than the original design volume. This reduced volume is negatively impacting the life of our overall ash disposal plan and forcing the necessity for a dry ash-handling system one year earlier than stated in the above-referenced memorandum. Between now and March 1986, we must dispose of 547,000 tons of ash. Since ash to be produced approximately equals the remaining storage capacity, it is essential that additional disposal capacity be provided by March 1986. The need for this early date has been a direct result of problems with pond J.

Paul Wade

JOHN SEVIER FOSSIL PLANT - ASH DISPOSAL PROGRAM

To meet our ash disposal requirements until the dry ash collection system is in operation, we recommend the following three actions be taken: (These actions are required to provide a water inventory in pond 2 to support the continued disposal of bottom ash and other plant wastewater streams.)

- 1. Reclaim and stack 400,000 tons of ash from the bathtub. This action is being implemented by the plant as equipment becomes available. However, bids will be solicited and will be awarded if proven to be economical. The estimated cost for this work is \$1,400,000.
- 2. Pond 2 will be full by spring 1986. Dredge 400,000 tons from pond 2 to the bathtub beginning in March 1986. The estimated cost for this is \$400,000.
- 3. Presently, a contract is in progress for removing 120,000 tons of dry bottom ash from pond 2 and reclaiming a portion of the earth borrow pit across the railroad tracks from pond 2. As soon as this contract is completed (late November 1984), set up a reclaim pond in pond 2 using tractor-scrapers (two CAT 637D's and one dozer, plus operators for two or three days per week). Dry stacking of this material will be at the abandoned section of Polly's Branch and on the abandoned ash ponds.

The conversion to dry fly ash handling is felt to be the most practical alternative to meet long-range ash disposal needs. However, the recent offer by Mr. Gerbus (reference 2) to sell land to TVA must be evaluated along with dry ash handling prior to making a final decision. Possibly, this land can be purchased and developed to support dry ash stacking for plant life. Independent of land considerations, the conversion to dry fly ash handling is expected to cost between \$8,000,000 and \$10,000,000.

In order to meet the additional ash-handling requirements mentioned in item 3 above, the plant will need two CAT 637D tractor-scrapers. These can be purchased with the money allocated for a dragline for fiscal year 1985, since a dragline will not be necessary for this operation. The cost of the two tractor-scrapers should be approximately \$565,000; \$555,000 is budgeted.

Paul Wade

JOHN SEVIER FOSSIL PLANT - ASH DISPOSAL PROGRAM

In view of the above, we will proceed immediately with a request for EN DES to prepare a cost estimate for dry fly ash handling. Also, we will prepare necessary work orders and project justification to begin construction in fiscal year 1985.

Jack T. Thompson

TWW: JWC: BLH: SRS

Attachment

cc: ARMS, 810 EB-C

B. B. Street, John Sevier

TVA 64 (05-9-65)

UNITED STATES GOVERNMENT

Memorandum

M. H. miller 333 SPT-K TENNESSEE VALLEY AUTHORITY

'840912 002 FFP

TO

: C. C. Schonhoff, Director of Fossil and Hydro Power, 716 EB-C

FROM

R. G. Domer, Director of Engineering Projects, W11A6 C-K

DATE

SEP 1 2 1984

SUBJECT: JOHN SEVIER STEAM PLANT - ASH POND J - SLOPE STABILIZATION MODIFICATIONS

Representatives from our respective staffs met with plant personnel in B. B. Street's office on August 14, 1984, to discuss the results of our recent slope stability analyses on the dikes for the subject project. The following areas were of primary concern:

- Area 1. The 600+ -foot-long section of riverbank dike adjacent to the spillway outfall.
- The 1000 foot-long section of riverbank dike between the abandoned bridge and the fisherman's access ramp.
- The 450+ -foot-long section of dike along Dodson Creek on the north end of ash pond J.

Our analyses indicate only area 2 is sufficiently stable to resist landslides without additional modifications. The safety factor against sliding is less than 1.0 fcr areas 1 and 3, and they will require additional modifications to obtain an acceptable safety factor for long-term operational reliability. Although these dike areas were originally designed to provide a 1.5 safety factor, our reanalysis has discovered the following discrepancies:

- The original dike design assumed a wide berm between the toe of the new ash pond dike and the existing riverbank. The dike was actually located (per design drawings) too close to the river. The riverbank - actually undercuts the dike foundation zone.
- 2. Original slope stability analyses were performed only for normal operating and construction conditions while our recent analysis for the long-term steady seepage yields lower, unacceptable, safety factors.
- 3. Our original design also called for granular material to be placed in the outside regions of the dike, but construction drawings made placement of granular material optional; therefore, sufficient granular material was not placed, thus reducing the calculated factor of safety.

In addition to our analysis we investigated various solutions to improve the safety factors for areas 1 and 3, but recommended that a safety factor of 1.5 is most desirable. To obtain this degree of safety would require placing an additional 39,000 tons of riprap at area 1 and moving the centerline of the dike toward the inside of the new pond, thereby creating a new outer dike slope of 4:1 for area 3. The construction costs for this effort would be on the order of magnitude of \$680,000.



C. C. Schonhoff SEP 1 2 1984

JOHN SEVIER STEAM PLANT - ASH POND J - SLOPE STABILIZATION MODIFICATIONS

Less costly modifications could be done but would not provide the recommended 1.5 safety factor. Construction in area 3 would also be delayed since placement of additional riprap on the outside slope of the dike would require an environmental review and approval process.

Therefore, we are proceeding with design and construction and will charge all costs to the original work order in accordance with the concurrence of your representatives at the August 14, 1983 plant meeting. Construction will begin by October 1, 1984, and be completed by December 31, 1984, with priority placed on completing the earthfill for area 3.

Since implementation of these modifications will decrease the ash disposal area of pond J, the long-term ash disposal plans (conversion to dry stacking) will need to be reevaluated and in all probability accelerated by approximately one year. The Office of Engineering will prepare a cost estimate for providing the dry ash handling facilities upon receipt of your scope of work document, but will also require separate funding for this engineering effort since it is not associated with the original work order for ash pond J. We can provide you with an estimate of our anticipated engineering costs for this cost estimate after receipt of your scope-of-work document.

Original Signed By John E Holladay

R. G. Domer

OPT: JEB: FLC

cc: R. O. Barnett, W9D224 C-K

C. Bonine, E7B24 C-K

C. A. Chandley, W7C126 C-K

MEDS, W5B63 C-K

R. A. Painter, W5D181 C-K

O. P. Thornton, 102 SPT-K

F. Van Meter, 500 SPT-K (3)

Principally Prepared By: J. E. Branch, Extension 3174, and M. H. Miller, Extension 2956

\$64248.04

5 July Sullivan 8-29-84
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O ADDRESS 333 SPT Counts X Inc. I
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If A Requirements are not required, is CFR Part 21 notice required	17 Yes⊔ No⊔				
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TVA 488 (EN DES-3-77)

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TVA 488 (EN DES-3-77)

CSB Estimates Section

Project John Sevier Steam Plant
Feature Ash Pond "J" Dike Relocation
Cost Code

ESTIMATE FORM

Sheet 1 of 1

Prepared J.D.J.Date 8-13-84
Checked Date

TOTAL Unit Amount	\$ 5,000	1,110	49,450	301.6CT	4,110	\$128,080	5,330 \$133,410 8,000	23,590	\$165,000
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JOHN SEVIER S.A.			
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TVA 64 (05-9-65) UNITED STATES GOVERNMENT Memorandum

TENNESSEE VALLEY AUTHORITY

H. S. Fox, Director of Fossil and Hydro Power, 716 EB-C 0329 : R. W. Cantrell, Manager of Engineering Design (Acting), WIIA9 C-K

DATE: MAR 2 9 1984

SUBJECT: JOHN SEVIER STEAM PLANT - ASH POND J REPAIRS

This is to confirm the agreement made by our respective staff representatives during the March 16, 1984, meeting at John Sevier Steam Plant regarding the subject repairs.

EN DES and CSB will proceed immediately with design and construction to repair the actual and potential riverbank slide areas which were identified during the March 8, 1984, inspection of the subject plant's ash disposal

The scope of work for these repairs is as follows:

- Stabilize approximately 600 feet of riverbank in the vicinity of the existing pond discharge pipes.
- Construct a permanent access road at the base of the dike around the western end of pond J (approximately 1500 feet).
- 3. Regrade the roadway surface on top of the dike to slope toward the pond in accordance with original design drawings.
- 4. Repair the washout of the interior slope of the dike at the eastern end of the pond.
- Seal off leakage around the existing pond discharge pipes.

These work areas are identified on the attached marked-up print of drawing 10W286-1 R2.

EN DES and CSB's order-of-magnitude costs for completing these repairs are \$22,000 and \$350,000 respectively. Due to the urgency for completing this work, we will charge all costs to work order number 51063-20656, account number 544-30-20656 per your staff's verbal request at the March 16, 1984, meeting. CSB mobilized their forces on March 26, 1984, and anticipates completing these repairs in September 1984. We expect pond J could be returned to service by late April 1984. Modifications to the existing 404



Land to the second second

H. S. Fox MAR 2 9 1984

JOHN SEVIER STEAM PLANT - ASH POND J REPAIRS

permit will be performed concurrently with the physical construction repairs per our verbal coordination with the Corps of Engineers and is included in our estimated costs.

EN DES is initiating an authorization level cost estimate for the purpose of revising the work order (account 544-30-20656) and authorizing the additional funds necessary for EN DES and CSB to perform this work which is outside the scope of the original work order.

> Orginal Sirred By John E. Holladay

R. W. Cantrell

RE

JEB : JAG : MHM : JEB : JAG

Attachment

cc: R. O. Barnett, W9D224 C-K - w/attachment - Please provide the necessary support documents

for the 404 permit modifications.---RWC

C. Bonine, E7B24 C-K

C. A. Chandley, W7C126 C-K - w/attachment - Please handle 404 permit

modification. Civils will provide support document .--- RWC

MEDS, W5B63 C-K

C. W. Kilgore, W12C74 C-K

R. A. Painter, W5D181 C-K

O. P. Thornton, 102 SPT-K

F. Van Meter, 500 SPT-K (3) - w/attachment - Note CSB's responsibilities.---RWC

Principally Prepared By: J. E. Branch, Extension 3174 and M. H. Miller, Extension 2956

BC/PM: for OPI

Memorandum

TENNESSEE VALLEY AUTHORITY

FDP '84 0328 007

TO : Fossil Design Projects Files

FROM : Marvin H. Miller, Senior Civil Engineer, 333 SPT-K

DATE : MAR 2 8 1984

SUBJECT: JOHN SEVIER STEAM PLANT - ASH POND J - REPORT OF RIVERBANK SLIDE AND

PROPOSED REPAIRS

On March 8, 1984, while participating in the spring inspection of John Sevier's ash disposal areas, Ronnie Powell (FDP) and Robert Spencer (CEB) discovered a slide at the riverbank at the base of Pond J's dike. The 65-foot long slide extended from the toe of the dike into the Holston River. This slide had eroded the foundation support for the dike creating a serious hazard to the dike itself. See Attachments A and B. FDP immediately notified F&H PR of the slide and the need for repairing it before the river level rises significantly. F&H PR requested EN DES to provide recommendations for the repair work to be done.

John Hillier Stivers, Syed Ahmed, and I visited the site on March 12, 1984. After the inspection of Pond J, we recommended additional work along the riverbank adjacent to the slide. This additional 600 ± feet of nearly vertical riverbank could slip at any time. Because the toe of the dike is so close to this bank, the dike is also susceptible to failure. FDP informed F&H PR the cost to repair the slide and stabilize the riverbank could be several hundred thousand dollars. F&H PR requested all cost be charged to the work order for Pond J. FDP requested CSB to mobilize for the slide repair.

On March 14th, Ronnie Powell returned to the site with CSB estimator Jimmy Jenkins and CSB's Bobby Elliott. While they were inspecting the work site, F&H PR personnel removed a spillway wier in preparation for raising the pond level. The resulting surge of water thru the discharge pipe washed away the riprap at the outfall, exposing the vertical riverbank at the toe of the dike. The plant immediately took Pond J out of operation. This new failure occurred within the 600 ± additional feet of riverbank EN DES recognized as a potential slide area.

On March 16th, O. P. Thornton, R. E. Harris, and John Hillier Stivers and CSB's Jim Sullivan, Bob Bruer, Bobby Elliott, and Jimmy Jenkins met Jack Thompson of F&H PR at Buford Street's office at the plant site. EN DES presented details for the proposed repairs. All parties agreed the entire 600 ± feet of riverbank should be stabilized immediately. A permanent access road will be constructed at the base of the dike around the western end of Pond J. The roadway surface on top of the dike will be graded to slope to the inside in accordance with the original design drawings. A washout of the interior slope of the dike at the eastern end of the pond will also be repaired. Leakage around the pond discharge pipes will be stopped.

CSB will perform all construction. EN DES will provide design drawings for the dike stabilization.

Fossil Design Projects Files MAR 28 1984

JOHN SEVIER STEAM PLANT - ASH POND J - REPORT OF RIVERBANK SLIDE AND PROPOSED REPAIRS

The Corps of Engineers gave TVA verbal approval to proceed. EN DES will prepare an amendment to the 404 permit.

Holston Electric Company will relocate or deenergize power lines as required.

Marvin H. Miller

red

MHM: EFS

Attachments

cc: 0. P. Thornton, 102 SPT-K

OF

OPT: EFS - MAR 2 8 1984

cc: R. O. Barnett, W9D224 C-K

C. A. Chandley, W7C126 C-K

J. E. Holladay, W2D224 C-K

MEDS, W5B63 C-K

F. Van Meter, 500 SPT-K (3)

R. W. Cantrell, W11A9 C-K

Principally Prepared By: Marvin H. Miller, Extension 2956

Executive Order 998 Water Residence - Roger Milsterd

Project JOHN SEVIETS STREAM PLANT

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REPAIR

DIRE

Feature ASH Cost Code

Archabaish need look enterbank (for significant withfacks) Sheet / or ESTIMATE FORM Spillway work entrophed prepared J.D. Date 3/2/89 no EA or EIS required acry cleared for MEPA act

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TOTAL FIELD CONGSTANGTIONS

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OEDC Estimates Section

Ro (superceded ESTIMATE FORM 1199

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way

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5,000 4,000 Amount 21,300 19,100 32,950 180,850 21,800 300,000 259,200 15,000 TOTAL Prepared J.D.J. Date 3/15/84 Price Unit Date Furnish & Contracts Install Checked 3,700 8,000 Eqpt Usage/ 4,000 11,000 \$47,800 Other 21,100 \$ 1,000 2,300 8,100 \$26,100 3,700 11,000 Amount \$/MH Man-Hours 160 009 240 720 1,720 R1 MH/ Unit 5 \$ 15,300 21,250 148,750 \$185,300 SMO Amount 3000 FIELD CONSTRUCTION Price 8.50 Unit (1.000 TNS Ribrap at \$8.50/TN) Q (1,000 TNS 10B2 at \$6,75/TN) Repair At Ash Pbnd Discharge Un John Sevier Steam Plant Construction Facilities Qty Mobilize & Demobilize Field General Ekpense (17,500 TNS Riprap) Access Road & Riprap (2,500 INS Riprap) SUBTOTAL Slide Area Repair TOTAL Ash Dike Repair Description Dike Repair Contingency (6 Loads) Clearing Cost Code 4004 ob tarmed Feature **0** Account No.

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Advance Copy

TVA 450 (OS-9-80) INTEROFFICE MAILING SLIP

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Fold here for return	
F R.J. Hunt	EXTENSION 6903
R ADDRESS 179 LB-K	Chatta M. S. Knox Nor.
RE: John Sevier S.P. Ash Pond J	dike - Stope faile
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57A. 50+ Loading conditions and factors, pl. refer Civil Design	Guide DG-
Section 5.4.5	
If you have any quests	in, pl.
contact byed Ahmed (ex: 6905	
Attachment	

John Sevier S.P. Ash Pond J

Dike stability Analysis. STA. 44 + to STA. 50+

COMPUTED SBA

DATE 3-21-84

Recommended Soil Properties for Stability Analysis to STA 50+ STA. 44± Pends dike Ash

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OEDC Estimates Section

Project JOHN SEVILE STEMM RANT Feature ASH POND "T"

Cost Code

ESTIMATE FORM

Prepared J.D. J. Date 8-13-89 Date Sheet / of Checked _

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V Un Price			\$7	1 1 1	2 7 7	\$ 7 7 7 7	27777	\$ 7 7 7 7 8 PK	2777787	2777787	2777787	2777787	2777787	2777787	277777	2777787	2777787	2777787	2777787	1	277787	2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
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Descri	MOBILIZATION	12 MOBILI ZATION	AMI ROMD M	HAWL ROOM M. BOTTOM MEH. D	AMI ROM M. KoTOM MSH-T	HAUL ROAD MODIFUATED BOTTOM ASH - DUMPED -(CAMPETED EARTH EXC - FILL	HAUL ROAD MODIFUR BOTTOM ASH - DUINPE - COMPET SPOIL DISTORAL	AMI ROM MAH IN CONTROL AND MANAGE AND MANAGE AND	AMI ROMD MOD SOTTOM MASH - DW CARTH EXC - I SPOIL DISTESS CRUSHED STOWE CELLSHED STOWE CELLSHED STOWE CELLSHED STOWE	AMI ROM MAHLT OTTOM MAHLT CREATHER STORES CREASHED STORES CREA	AUL ROMD MODIFHERD OFFICED OFFICE THE EXC. + FILL SPOIL DISTISSAN SUB TETH DIR (EUS)	AMI ROPA MA OTTOM MAH - T OTTOM MAH - T OTTOM MAH - T SPOIL DISTA SPOIL DISTA	AMI ROM MAHLI POTTER LA DISTA SPOIL DISTA STORY THEX STORY SWAR TETH DIN TONES TETH	AMI ROPE MOSTER STREETH EXC CO. STREETH EXC C	AMI ROM MAHLT OFFILE DISTS STORIL DIRTS STOR	AND ROMD MODING OF THE EAST A LEWAR STELL THE	AMI ROPA MA AMI ROPA MA BOTTHEXC - C SPOIL DISTA STORY THEN STORY STORY THEN STORY STORY THEN STORY STORY THEN STORY CONTINUES STORY CONTINUES	AMI ROM MAHLT BOTTOM MAHLT SPOIL DISTA STORIL DISTA SMB TETM DIM COMTIMOEN COMTIMOEN COMTIMOEN	HAMI ROPD MODIFIED BOTTOM ASH-DUME EARTHEX + FILL SFOIL DISTOSAN CRUSHED STONE SETT + MULCH SUB. TETH DIR (B CONST. FALLIT TOTH DIR (B CONTINGENCY CHATIMOGENCY	AMI ROM MAHLE OFFICE LEWSHED STEEL CENTIMEEN CENTIMEEN CENTIMEEN CENTIMEEN CENTIMEEN	AMI ROM M. ROM M. BOTTOM METHER STORY - TO S	AMI ROM MAHLINGEN CELLSHED STORY LOWER STO

OEDC Estimate Section

Cost Code Code Toke Resembly PRELIMINARY Project JOHN SEVILTE STEMA PLANT

ESTIMATE FORM

Prepared J.D.J. Date 8-13-8% Sheet / of Checked

		MA	MATERIAL.			LABOR		Dant	Trees de la		
Account		That) igy				E G P C	בחדוודמנו מ		18101
No. Description	Qty Un		Amount	Unit	Man-Hours	\$/MH	Amount	Other	Contracts	Unit Price	Amount
Moderization 4											
The Marie 2 27702								5.000			5,000
HAWL ROAD MODIFICATION	57 1 7				16		280	830			0111
BoTTOM ASH - DUMPLD	20.00 CY				340		12,156	37,300			49 450
-Compers	4,2co cx		1		0/12		3,600	11,506			15,100
EARTH EXC. + FILL.	14.400 CY				049		16.400	31,000			41.400
SPOIL DISTIBLE	2,100 CV		~ 1 ⁄		40		960	3,150			4.110
CRUSHED STOWE	205 TNS	1	1435		16		3281	3950			6,770
Sear + Mucch	15, Seo 51	٠ اه	1550		233		2630	0201			5.200
SUB TITH DIR (ENS			5862		2109	14.86	31.345	93.750			128,080
Const. Frenches					251		3730	1,600			5330
TOME DIE CONST			2985		23/06		35,075	95350			133 410
FIRST GEN. EXPLISE	36				2		400	7,600			8.00
CONTINGENCY											23.5%
	1001	F162	200	SIRU	STRUCTION						165.000
BASED	20 a	Constra	124c7/10	7 7	y Med						

FACTOR OF SAFETY AT STA. 41+75 (DODSON CREEK) WITH NORMAL PHREATIC SURFACE

DESCRIPTION OF	REPAIR	FACTOR	OF SAFETY
		Ŕ.	R
RIPRAP @ EL. 107	6	0.94	0.96
RIPRAP @ EL. 1082	O 9. FAILURE AT TOP OF RIPRAP	1.04	1.06
	b. FAILURE AT BOTTOM OF RIPRAP	1.06	
RIPRAP@ EL. 1080;	WITH 10'BERM @ EL. IL	%5	
	a. FAILURE AT TOP	1.14	1.12
	L'FAILURE AT BOTTOM OF RIPRAP	1.15	1.27
	C. FAILURE ABOVE RIPRAP		1.04
RIPRAP @ EL. 1080: 1	NITH 10' BERM @ EL. 10	70	
	9. FAILURE AT TOP	1.17	1.12
00 Ton x 10 2	b. FAILURE AT BOTTOM OF RIPRAP	1.21	1,31
144,000	C. FAILURE ABOVE		1.04

COMPUTED JMH DATE 8-9-84

CHECKE

NO ADDITIONAL RIPRAP AND NO SLUTE CHANGE

DROP WATER TABLE EL. 1073 IN POND FOR DRY STACKINS

R: OUTSIDE SLOPE F.S. = 1.08

INSIDE SLOPE F. 5. = 1.03

R: OUTSIDE SLOPE F.S= 1.16
INSIDE SLOPE F.S.= 1.12

SLOPE CHANGE TO 4": IV AND NO ADDITIONAL RIPRAP
POND WATER EL. 1101

R: DUTSIDE SLOPE F.S. = 1.47

INSIDE SLOPE F.S. = 1.29

R: OUTSIDE SLOPE F.S. = 1.73

INSIDE SLOPE F.S. = 1.87

SLOPE CHANGE TO 3": 1" AND NO ADDITIONAL RIPRAP

R: OUTSIDE SLOPE F.S. = 1.03

FACTOR OF SAFETY

	SHEET	OF
JOHN SEVIER ASH DISPOSAL AREA "J"		
STA 41+75 DODSON CREEK		
	COMPUTED	9MM DATE OCT. 26,84

PROBLEM! THE REPAIR OF JOHN SEVIER ASH POND "J"

CALLED FOR BOTTOM ASH IN THE DESIGN. DURING

CONSTRUCTION FLY ASH WAS DUMPED INSTEAD OF

BOTTOM ASH.

DESCRIPTION: CHANGE IN DESIGN WAS NEEDED WHEN THE BOTTOM ASH SUPPLY WAS FOUND TO BE VERY LIMITED AND THERE WAS NOT ENOUGH BOTTOM ASH FOR THE DESIGN. TWO CHANGES TO THE DESIGN WERE PROPOSED. THE FIRST WAS TO REMOVE DUMPED FLY ASH AND REPLACE WITH COMPACTED FLY ASH. WITH. A 3:1 SLOPE, THE FIRST PROPOSAL WAS FOUND TO HAVE A SAFETY FACTOR OF LESS THAN 1.2, THERE FORE WAS UNSATISFACTORY. THE SECOND PROPOSAL WAS TO REMOVE THE DUMPED FLY ASH PLACE A ROCK FILL BELOW THE WATER LEVEL AND THE TOP OF THE ROCK FILL BE PLACED SUCH THAT COMPACTED FLY ASH COUD BE PLACED ON TOP OF THE ROCK FILL, (SEE FIGURE 1)

11100	(-85,-30) ROCK FILL 3=4135	Q INITIAL DIKE CLAY 7-127	$(43,0) \qquad (65,0) \qquad ($
1070	φ=3.5° (-86,-3'7)	INSITU SOIL 8=-128; =0;	$ \bar{\Phi} = 25^{\circ} $ INSITU 1060
, -140 -130 -100		-30 -20 -70 0 10 2	0 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 JOHN SEVIER ASH DISPOSAL AREA "J" STA 41+75 DODSON CREEK
			FIGURE 1

3-21-84

John Sevier S.P. Ash Pond J Dike stability Analysis. STA. 44 + Recommended Soil Properties for Stability Analysis

STA. 441 to STA SOF

Pouds dike

Ash

do

				T	CHECKED	DATE	
	REMARKS		Properties same as evaluated	Proberties evaluated from test results on samples from Us. borings 12 8,15 only	* Assumed - No test data available stone weight. 150-450 F	sts of (In situ) cohesive Allyvium rock, Ignore any meace of consequentive analysis.	
	102	100	27	52	3 K	consists of sock, or a conse	
STH		1 C (18F)	0	0	*0	compacted earthfull adults of indicated on indicated shall adult the a	
STRENGTH	R	Ø.	1	=	* ທ ຕ	soil dute ala f	
SHEAR S	1	C (TSF)	0 - 0 S	9 0 E	* 0	e the insitu soil or ucted earthfull andustro or uncathened shale thr	
SHS	Ø	© &		0	* w	compacted earthfill vial or weathered s	
		Sub (TSE)	6.0	4.0	* 0	e the	
£1644T		Sub	n	65	***	, ,	
1	(PCF)	% **	121	12.8	* W	sis of the or Allu	
13	· .	~ moist	123	12.5	* SO 1	and Hou annul	
	Soil Toentification		Bonow Earthfull (tompacted)	In situ Cohesive Alluvium	Rockfill (wan packed)	Note: For stability andlesis assubetween the bottom of the complete insite grammillar Allevial	

TVA 11030 (WM-7-75)

				SHEET	OF
JOHN SEVIER S.P ASH	POND	<u>"J" </u>			
STA 41+75 - DODSON					
INSIDE SLOPE WITH COMP	ACTED	A5H_		COMPUTED JIH	DATE 027, 29, 84
ASH PROPERTIES				CHECKED	DATE
ENGINEERING PROPE ASSUMED PROPE		OF A	<i>5</i> Н	D	<u> </u>
	×	%	Y	- K	RORS
				с ф	c o
COMPACTED BOTTOM ASH	117pcf	120pcf	58pcf	1200psf 20°	0 33°
DUMPED BOTTOM ASH (IN WATER)	-	110 pcf	48Rf	600psf 15°	0 28°
CONSOLIDATED FLY ASH	85 pcf	95pcf	33 pcf	100psf 15°	0 24°
V. LOOSE FLY ASH	65pcf	Macf	8pcf	0 0	0 0
ASSUMED PROPERTIES	OF CO	MPACTED	ASH	* R	RORS
COMPACTED FLY ASH	V MAIST	1/sat -100pcf	8 SUB	Cd	E 7 0 28° AND 30°
			· · · · · · · · · · · · · · · · · · ·		
COMPACTED ASH				C φ 0 11.4	R C Ø O 18.8

1100	$2\sqrt{(-67,-29)}$	Compacted Clay $ \hat{\sigma} = 123, \hat{c} = 0; \hat{\phi} = 27^{\circ} $ $ \hat{\sigma} = 127, \hat{c} = 0; \hat{\phi} = 27^{\circ} $ Compacted $ \hat{\sigma} = -127, \hat{c} = 0; \hat{\phi} = 27^{\circ} $ $ \hat{\sigma} = -127, \hat{c} = 0; \hat{\phi} = 27^{\circ} $ $ \hat{\sigma} = -127; \hat{c} = 0; \hat{\phi} = 27^{\circ} $ $ \hat{\sigma} = -127; \hat{c} = 0; \hat{\phi} = 27^{\circ} $ (80,-27)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
1060 (-9399,-46.5) (-105-46.5) (-9399,-49) (-112,-49) 1050 -130 -120 -100	-70 -60 -50 -40 -30 -20	70 0 70 20 30 40 50 60 70 80 90	1050 100 110 120 130 140 150 160 170 180 1 D. AHMED THINKS \$= 200 FOR ASH BENEATH COMPACTED ASH TOO HIGH FOR DESIGN THERE FORE ROCK TOE MUST BE USED.

THESE ARE THE INPUT DATA LINES

X1	Y1	X5	Y2.	W	F2	Fi	C2	Ci
399. 0	-49.0	-112.0	_49.0	-1000.0	0.0	+00.0		0000 0
-112.0	-49.0	9399.0		-1000.0		100.0 100.0	0.0	9999.0
-9399.0	-46.5	-110.0		-62.4			0.0	9999.0
	-49.0		-46.5			0.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5		0.0		0.0	0.0
-105.5	-41.5		-39.5			25.0	0.0	0.0
1.5	-39.5		-37.0			25.0	0.0	0.0
-86.0	-37.0		-34.0	-128.0	35.0	25.0	0.0	0.0
-79.0	-34.0	-67.0		-127.0	35.0	27.0	0.0	0.0
-100.0	-39.5		-29.0	123.0	35.0	27.0	0.0	0.0
-100.0 -85.0		-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
	-30.0	- 6 7.0	-29.0	135.0	0.0	35.0	0.0	0.0
- 6 7.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
	0.0	77.0	-4.0	123.0	0.0	27.0	0.0	0.0
	-4.0	110.0	-15.0	-127.0	0.0	27.0	0.0	0.0
110.0	-15.0	146.0	-27.0	-100.0	0.0		0.0	0.0
	-27.0	150.0	-40.0	-90.0	10.0	20.0	0.0	0.0
	-26.0	185.0	-40.0	-85.0	0.0	10.0	0.0	0.0
80.0	-27.0	146.0	-27.0	-90.0	24.0	20.0	0.0	0.0
	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
X	-15.0	70.0	-25.0	-127.0	24.0	27.0	0.0	0.0
	-25.0	80.0	-27.0	-127.0	24.0	27.0	0.0	0.0
	-27.0	105.0	-29.0	-127.0	20.0	27.0	0.0	0.0
	-29.0	145.0	-40.0	-127.0	20.0	27.0	0.0	0.0
145.0	-40. 0	150.0	-40.0	-128.0	20.0	25.0	0.0	0.0
150.0	-40.0	185.0	-40.0	-128.0	10.0	25.0	0.0	0.0
185.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
	-15.0	10.0	-15.0	-100.0	27.0	24.0	0.0	0.0
	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-7 9. 0	-34.0	77.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT = 146.0 YT = -28.0 XB = 150.0 YB = -40.0

GRIDX= 90.0 GRIDY= 10.0 XMAX= 190.0 YMAX= 200.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

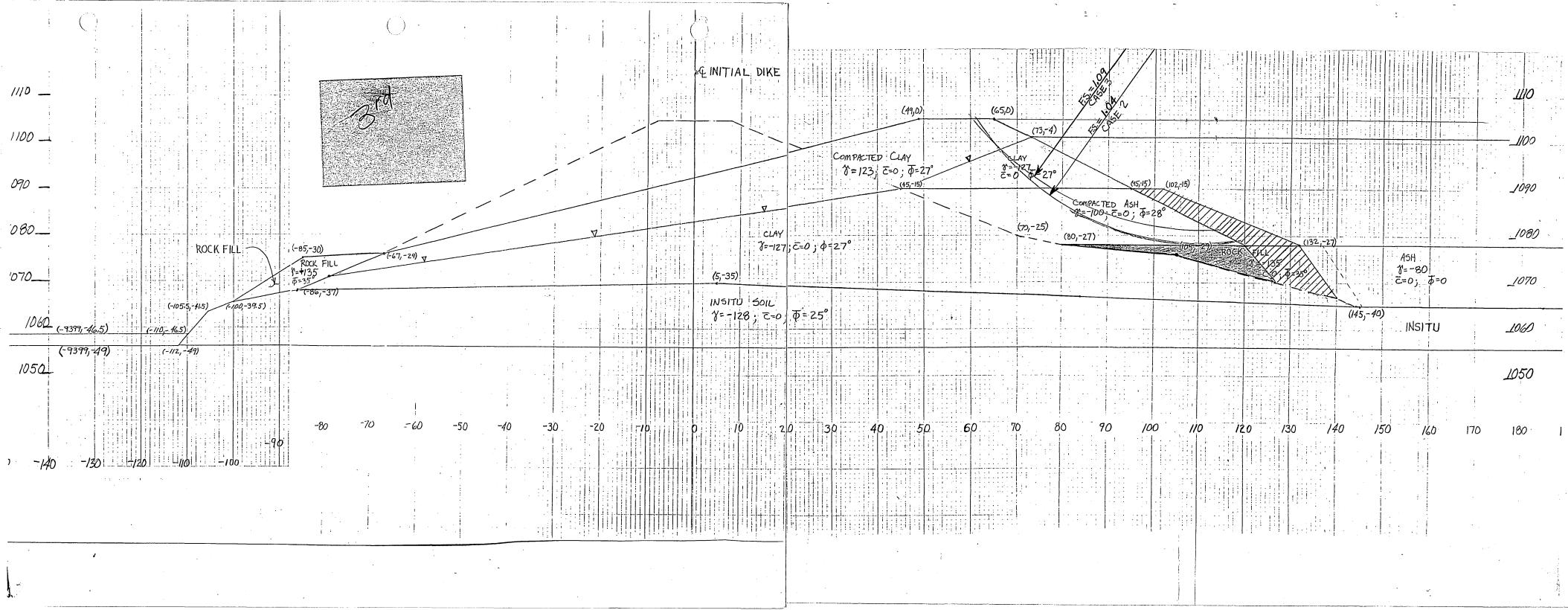
CASEI

THE MIN. FS= 1.02 EFS= .69 H(X)= 150.00 G(Y)= 50.00 R= 88.11

THE MIN. EFS= .17 FS= 3.51 H(X) = 190.00 G(Y) = 100.00 R= 135.36

SBU 185.006 UNTS.

-RUN COMPLETE



00110 SHALLOW CIRCLE,JSF,R-EFF,BUTSIDE=4:1,INSIDE=2:1,COMPACTED ASH,ROCK (ERQF= . 05 DEPTH OF ROCK= 49.0 FT)

CASE Z

THESE ARE THE INPUT DATA LINES

the state of the s								
×1	Y1	XS	Y2	W	F2	F1	ca	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	0.0	27.0	0.0	0.0
95.0	-15.0	120.0	-27.0	-100.0	0.0	28.0	0.0	0.0
	-27.0	126.0	-33.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	120.0	-27.0	-135.0	28.0	35.0	0.0	0.0
	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	28.0	27.0	0.0	0.0
	-25.0	80.0	-27.0	-127.0	28.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	126.0	-33.0	-127.0	35.0	27.0	0.0	0.0
	-33.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0		0.0	0.0
	-4.0	9399.0		-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0	27.0	0.0	0.0
45.0	-15.0	73.0	-4.0	-127.0	27.0	27.0	0.0	0.0
		and the second second	化氯化甲酚 化氯化甲基甲酚				医甲基二氏 医二二苯二酚 医皮肤	

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 (GRIDY= 30.0) XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

DOES NOT CONTROL DESIGN USE ZUE: 1 SLOPE

TEST POINTS

CASE Z

THE MIN. FS= 1.04 EFS= .82 H(X)= 110.00 (G(T)= 30.00) R= 57.02

THE MIN. EFS= .78 FS= 1.12 H(X) = 150.00 G(Y) = 100.00 R= 135.10

SBU 76.261 UNTS.

RUN COMPLETE

00110 PHI=30,SHALLOW CIRCLE,JSF,R-EFF,OUTSIDE=4:1,INSIDE=2:1,COMPACTED A
(ERQF= .05 DEPTH OF ROCK= 49.0 FT)

CASE 3 THESE ARE THE INPUT DATA LINES

● ×1	Y1	xe	Y2	W	F2	F1	C2	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0		-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4		0.0	0.0	0.0
-112.0	-49.0	-110.0		-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0		0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	00	27.0	0.0	0.0
		120.0	-27.0	-100.0	0.0	30.0	0.0	0.0
120.0	-27.0	126.0	-33.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	120.0	-27.0	-135.0	30.0	35.0	0.0	0.0
	-27.0	9399.0	-27.0		0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	30.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	30.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	126.0	-33.0	-127.0	35.0	27.0	0.0	0.0
126.0	-33.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	30.0	0.0	0.0
73.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0	27.0	0.0	0.0
45.0	-15.0	73.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

CASE 3

THE MIN. FS= 1.09 EFS= .88 H(X)= 110.00 G(Y)= 40.00 R= 63.65

THE MIN. EFS= .80 FS= 1.15 H(X) = 150.00 G(Y) = 100.00 R= 135.10

SBU 78.541 UNTS.

11;0 _ 1100 _ '070 _ '070_	\$\frac{1}{5} \\ \frac{1}{5} \\ \frac	K FILL		Compacted Clay $ \begin{array}{c} (49,0) \\ \uparrow = 123, \overline{c} = 0; \overline{\phi} = 27^{\circ} \end{array} $ $ \begin{array}{c} (45,-15) \\ \hline (45,-35) \end{array} $	(65,0) $(73,-4)$ $(65,0)$ $(73,-4)$ $(73,-4)$ $(73,-4)$ $(73,-4)$ $(73,-4)$ $(73,-4)$ $(73,-4)$ $(73,-4)$ $(73,-4)$ $(73,-25)$ $(80,-27)$ $(80,-27)$	$\frac{1}{2}$ Rock Fill $\frac{1}{2}$ A5H $\frac{1}{2}$ -80 $\frac{1}{2}$ -0; $\frac{1}{2}$ =0; $\frac{1}{2}$ =0	
1050	9399,-46.5) (-110,-46.5) -9399,-49) (-112,-49) -130 -100	-80 -70 -60 -50	-40 -30 -20 -70	$V = -128$; $C = 0$; $V = 25^{\circ}$	60 70 80 90 100 110	(145,-40) INSITU	1060 1050 170 180 1

CASE 4

84/10/25. 09.03.03. PROGRAM SLOPE2

00110 JSF ASH POND "J", R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMPACTED ASH,ROC (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

CASE 4

THESE ARE THE INPUT DATA LINES

×1	Y1	X2	Y2	W	F2	F1	62	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0		-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0		
-112.0	-49.0	-110.0	-46.5		0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0 0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0 0.0
-100.0	-39.5	-86.0	-37.0		35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0. U
65.0	0.0	75.0	-4.0	123.0	0.0	27.0	0.0	0.0
75.0	-4.0	102.0	-15.0	-127.0	0.0	27.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	28.0	0.0	0.0
132.0	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	132.0	-27.0	-135.0	28.0	35.0	0.0	0.0
132.0	-27.0	9399.0.,	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	28.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	28.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	102.0	-15.0	-100.0	27.0	<u> 28.0</u>	0.0	0.0
75.0	-4.0	9399.0		-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0	27.0	0.0	0.0
45.0	-15.0	75.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT = 65.0 YT = -5.0 XB = 150.0 YB = -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

CASE 4

THE MIN. FS= 1.24 EFS= .97 H(X) = 110.00 G(Y) = 40.00 R= 63.65

.93 FS= 1.32 H(X) = 150.00 G(Y) = 90.00 R= 127.49

00110 JSF ASH POND "J", R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMPACTED ASH,ROC (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

CASE 5

THESE ARE THE INPUT DATA LINES

	10 E. S. C. S.	**						
● X1	Y1	X2	72	W ₁	F2	F1	cs	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
100.0	-39.5		-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0		-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
्र: - 79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
~ -85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	75.0	-4.0	123.0	0.0	27.0	0.0	0.0
75.0	-4.0	102.0	-15.0	-127.0	0.0	27.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	30.0	0.0	0.0
132.0	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	132.0	- 27.0	-135.0	30.0	35.0	0.0	0.0
132.0	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	30.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	30.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	102.0	-15.0	-100.0	27.0	30.0	0.0	0.0
75.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
_5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0	27.0	0.0	0.0
45.0	-15.0	75.0	-4.0	-127.0	27.0	27.0	0.0	0.0
						e jiliyare je		

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

CASE 5

THE MIN. FS= 1.31 EFS= 1.02 H(X) = 110.00 G(Y) = 40.00 R= 63.65

THE MIN. EFS= .95 FS= 1.35 H(X)= 150.00 G(Y)= 90.00 R= 127.49

SBU 80.862 UNTS.

RUN COMPLETE

```
- ROP 11/2/84
    CASE
                 THESE ARE THE INPUT DATA LINES
                                                               02
     X1
                                                      F1
                                                                       C1
            Y1
                      X2
                              Y2
                                       bt:
                                               F2
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                                   -127.0
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                            -4.0
                                   -127.0
- XT≃ 65.0
              YT=
                       -5.0
                            XB= 150.0
                                              YB=
                                                     -45.0
                    GRIDY=
                             30.02 XMAX= 150.0 YMAX= 130.0
 GRIDX= 90.0
 INCX= 10 INCY= 10
                            INCR= 10
                                                     - expand test window
  THE MAXIMUM F.S. TO BE PRINTED IS
                                        0.00
  THE MAXIMUM E.F.S. TO BE PRINTED IS
                                        0.00
               TEST POINTS
   THE MIN. FS=
                                  . 95
                                        H(X) = 100.00 G(Y) =
                  1.20
                         EFS=
                                                               30.00<sup>)</sup>
   THE MIN. EFS=
                 . 94
                         FS= 1.37 H(X) = 150.00
                                                       G(Y) =
                                                               90.00
                                                                       R = 127.49
```

DEPTH OF ROCK= 49.0 FT)

(ERQF=

. 05

SBU 83.470 UNTS.

MRUM COMPLETE CA

THESE ARE THE INPUT DATA LINES .											
×1.	Yı	(A)		Office.	ħ.			194			
) / X2	. Y2	· · · · · · · · · · · · · · · · · · ·	. F2 :	`F1	: ce	CI,			
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₩.[3-112.0 3	5-49.0°	9399.n	-49.0 -		0.0` 0.0`	-100.0 \$100.0 2	0.0	9999.0			
~ -9399.0	2-46.5	-110.0	-46.5				0.0 0.0	9999.0 3 :0. 0			
. 3-112.0 °	5-49.O	-110.0	46.5	-128. 0	. 20.0°	25.0	O.O	-3.0.0			
110.0		-105.5	}-41.5 .			25.0 "	0.0	0.0			
NS E105.5	7-41.5	j=100.0	%-39.5	-128.0							
100.0	L - 39.5	%-86.0%		-128.O	235.n i		0.0	0.0			
885-86.0	3 - 37.0		· 经工程的证据 · · · · · · · · · · · · · · · · · · ·	ਜੁ127.0 ੀ	%¥35.0 %	2/27.0%	0.0:	720.0			
79.0	-34.0	;;-67.0		¥123.0 ≥	27 The second of	PROMOTER SECTION AND AN ARREST ASSESSMENT OF A SECTION OF		- 			
100.0	, , 39,5,	-85.0	-30.0 _A					2 4 00.01			
. 0,=85.0 -67.0		%-67.0	-29.0		≠ 0.0 °		0.0	0.0			
		\$7.49.0 65.0	440.0 P		**0.0 î			egge O.O			
		~, 63.0 ∴ 73.0	*0.0		**************************************		***0.0	ાં કે વેકળ કે છે. જે કે			
	-4.n	95.0		/123.0 -127.0	(0.0 ·)		%÷0.0;	0.0			
	.=15.0°	102.0		-100.0	*0.0 *0.0	.,27.0	0.0	**D.O			
2 0 2102.0 3		/ 132.D		=100.0	0.0	28.0 *28.0 %	0.0	0.0			
132.0 ×	-27.0	140.0		-135.0	0.0		*** 0.0 %				
		132.0°		-135.0	28.0	35.0 ⁴	0.0				
The state of the s	27.e	9399.n	-27.0	/-80.0	0.0	0.0	0.0	O.O			
- 1 - 機関を担じて終われない。		*¥70.0°	~25.0	-127.0	28.0	27.0	0.0	0.0			
	/ -25. 0	* 80.0	-27.0	-127.0	28.O	27.0 W	0.0	0.0			
	-27.0	115.0		-127.0	35.0	4 27.0 T	0.0	0.0			
	-29.0 -38.0		38.0	-127.0	ം 35.0	e~27.0 🥯	0.0	0.0			
	-40.0		-40.0	7127.Q		- 27.0 %	0.0	0.0			
- 100 2012年 (2012年 - 1912年 -		9399.0 95.0		-128.0		~ 25.0	0.0	0.0 %			
6-14-14-00	-4.0			-100.0	27.0	, 28.0	0.0	0.03			
	-37.0	5.0		%-62.4 -128.0	A STANDARD AND A STANDARD A STANDARD AND A STANDARD A STANDARD A STANDARD AND A STANDARD AND A STANDARD AND A STANDARD A STANDARD AND A STAND		(0.0	0.0			
	-35.0	145.0	\$2.00 per 100 uzula 2044.	-128.0	27.0	25.0	. 0.0	-0.0			
	-34.0	45.0	(1) (1) 1일 (1)	-127.0	27.0 / 27.0 /	25.0	0.0	0.0			
A CASE N	_15.0	73.0		-127.0	[4]名作业 主义 。 · 《礼程》	्र27.0 % ≨ 27.0 %	10.0 S	0.0			
				e de la companya de l		C U	0.0	0.0			
Market Commence		ica in second	1.00	÷775		- the Park	4.4				
XI = 65.0	·	[= - _5. 0	×B=	.150.0	.°'YB=	-45.0 ·2					
GRIDX= 9	iu. U isia. Sita n ama	GRIDY=	30.0	=×AMAX, دري	150.0	wakaymax.=	-100.0				
-,IMCX= 10					The Control of the Control						
				reins c							
THE MAXIMUM F.S. TO BE PRINTED IS 0.00											
THE MAXIMU	MFFS	TO DE	DOTNICH	10			- 4				
		·. 14 DC 1	K.111 1E.U	roka zu. U. I	/U	And the second	1				

CASE 6
TEST POINTS

THE MIN. FS= 1.17 EFS= .93 H(X)= 100.00 G(Y)= 30.00 R= 49.51

THE MIN. EFS= .93 FS= 1.17 H(X)= 100.00 5(γ)= 30.00 R= 49.5

SBŪ, ∲ 58.122 UMTS.

RUN COMPLETE.

: ' : : : G	ASE 6	HESE ARE	THE INF	PUT DATA	LINES.			
(1× ± 44	Y1		LLOW	. LEGICAL	*#F2 *	Fi :	r ca :	i.ci
. -9 399.0	49.0	-112.0	:::- 4 9.∩	=1000.0	0.0	.100.0	0.0	
5-112.0	7-49.0	9399.0	49.0	−1ពិព្រ. ្ព		100.0	는 함께 중심하는 하는 하는 소리를 받아 있다.	9999.0
- 9399.0	46.5	11 n n	-d£ 5	*-62.4	0.0			9999.0
112.0	∑'-49 . 0	-110.03	46.5	-128.0	# 0.0	4.25.0		
-110.0	./:−46 . 5	~=105.5	∛-41 . 5	.4128.0	0.0	2×25.0		
3-105.5°	%-41.5	2=100.0	39.5	-128.0	. O. O	725.0	2666A6226735年3147年38466	0.00
=100.0	39.5	%:586.0°	∰-37.0	-129.O	3935.0	: 25.0 ;	7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	2550.0
86. 0	37.0	% -79.0%	% <u>-</u> 34.0	ja7.0		≨\$ 27.0°		0.0
79.0	34.0	是一67.0	%-29.0	∡¥23.0	35.0	ae 27.0		0.0
	-# - 39.5		\$.~30.0	3135.0		35.0	and the second second	0.0
-85.0	∰-30.0-		<u></u> -29.0	- 135.0	~~.o.o	}}-35.0 ⁷		0.0
36 7.0			· ? 0.0	123.0	***O.O	°″27.0	The second second second	0.0
49.0	. O.O.	65.0 -		123.O	1.0000.00	#27 . 0∴5	8 5 0-0.0 %	avojo.nz
65.0	50 · 0.0	73.0		- 423. 0		%;27.0 ³	0.0	0.0
	4.0		₹ -15. 0	-127.0	0.0	%(27.0°)	ី 0.០ 🕏	0.0
	-15.0	102.0	% ≂15. 0	-100.0	J. 🚧 0.0	≨√28.0 K	. o.o s	Ø. 0.0°
\$\$102.0	-15.0	132.0	-27.0	-100.0	. 3- 0.0.	<u>,29.0</u>		. O. O.
**132.0	27.0		%-38.O	-135.0	- 0.0°	ু <u>35.</u> 0 :	CONTRACTOR OF THE PROPERTY OF	0.0
	-27.0		%-27 . 0	-135.0	<u>28.0</u>	i35.0	~ 0.0	0.0
%∻132.0 ∵¥445.0	% -27. 0		-27.0	-80.0	0.0	0.0	0.0	
234J.U 25.70.0	:=15.0		2725.0	-127.0	28.0	27.0	0.0	
90.0 80.0	70 -25.0	/ 80.0	[-27.0	-127.0	39.0	≈ 27.O	0.0	\$ 80.0
115.0	-27.0	115.0	J-29.0	-127.0	35.0	, 27.0	0.0	%% O.O
140.0	-29.0 9-38.0	140.0	38.0	-127.0	35.0	27.0	'0.0 ·s	370. 0
145.0	;-38.U :-40.O	145.0	-40.0	-127.0	0.0	27.n.,	0.0	z. 0.0 .
45.0	40.0 15.0	9399.0	-40.0	-128.0	0.0	25.0	ag 0.0 %	//.O.O.
the state of the s		* 95.0	⇒15.0	-100.0	÷27.0	ં∗ <u>28.0</u> ્≉	330.0 S	# # 0.0°
	;-4.0 -37.0	9399.0	-4.0	-62.4	0.0		48°0.0	* ,.0.0 °
5.0	7737.U √735.U	5.0	35.0	-128.0	27.0	≥ 25.0 /s		√0.0°
2.0 2.79.0	-34.0	145.0	-40.0	-128.0		a. 25.0 g	289 866 800 Day 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	The second of th
45.0	ີ-15.0 ີ-15.0	45.0 73.0	-15.0	-127.0		±:27.0 %		s#\`0.0 =
106/AL		ra.u	, -4.0	-127.0	27.0	27.0 °	0.0	0.0

. XT= 65.0 : YT= -5.0 : XB= ω150.0 ·ν YB= ω-45.0 · · ·

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 50.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS 6 SHALLOW

THE MIN. FS= 1.15 EFS= .94 H(X)= 90.00 G(Y)= 20.00

THE MIN. EFS= .93 FS= 1.16 H(x)= 90.00 G(y)= 10.00 TR= 29.16

BU ...66.603 UNTS.

00110 JSF,R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMP. ASH,ROCK;CLAY@2:1,PHI=30 (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

CASE 7

V ROP 11/2/84

THESE ARE THE]	INPUT	DATA	LINES
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X1	Y1	xa	Y2	W	F2	F1	ca	C1
-9399.0	-49.n	-112.0	_4Q_0	-1000.0				
-112.0	-49.0			-1000.0	0.0 25.0		0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	100.0	0.0	9999.0/
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	0.0 25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0 25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0		35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0 35.0	27.0	0.0	0.0/ 0.0/
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0		0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0 0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	-0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	0.0	27.0	0.0	0.0
95.0	-15.0	102.0	-15.0	-100.0	0.0	30.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	30.0	0.0	0.0
132.0	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	132.0	-27.0	-135.0	30.0	35.0	0.0	0.0
132.0	-27.0	9399.0	-27.0	-80.0	T.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	30.0	27.0	0.0	0.0
70.0	-25.0	80.0 ĭ	-27.0	-127.0	30.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	30.0	0.0	0.0
737570	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0	27.0	0.0	0.0
45.0	-15.0	ুকু: 0	-4.0	-127.0	27.0	27.0	0.0	0.0
		73			한가 뭐 되었다.			
Company of the Compan			er for the contract of the con			and the second of the second of the second of	THE STATE OF THE STATE OF	[48] 异类的强型体系设置中的发展。 (2.1)

XT = 65.0 YT = -5.0 XB = 150.0 YB = -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

CASE 7

THE MIN. FS= 1.24 EFS= 1.02 H(X) = 100.00 G(Y) = 50.00 R= 65.20

THE MIN. EFS= $\frac{1.40}{40}$ H(X)= 150.00 $\frac{1.49}{100}$ G(Y)= $\frac{1.49}{100}$

	LASE	Time.				1.50		-	
A Park		THESE ARE	THE INP	UT DATA L	IMES 点				*
No.	v.	X2							
	主持			. 2	F2	35 (F1 · ·	C2 44		
99.		;-112.O	- 49. 0	=1000.a	0.0	%100.0	0.07	3000 m	
112.	D 3.349.0·	.9399.O	#-49 n ?	- ។ គណៈគេ។	25.0	100.0		9999,"0"	
-9399.1		-,-110.0	-46,5		e. 20.0 ·	4,45 0. 0		isolo:	
-112. -110.1	The state of the s	-110.0	, -45.5 ₄				~ -0.03	$\mathbf{a} = 0 \in 0$	
105.		-105.5 -100.0	341.58	7-128.03	0.0	£5.0		0.0	
2 100)	in selection	39.5 39.0	-128.0 % -128.0 %	0.0			- 05 ibs	
-86.1)	79.0*	34 N	150.0 8-197 n 2	35. ii 3 385. ii 3	2-25.0 227.0		7. 1940. 1940.	1
# - 79. ()	567-67-11°8	-29.0.	123.0°	35.0.2	27.0		0.07	
#100.) ////-39.5	<85.0 \	2530.0€		× (40.0 ×	35.0	0.0	0.0	
. ÷85. () > > 30.0°	,67.0	½-29.0°	135.0	: 0.0 Z	35.0°°	0.0	2.0.0	
¥67. (1397-29.0	49.0		123.0	o.dec	* 27.0° €	. 0.0 🎎	ένμ, υ τ	
49.0 65.0		3 ∌/65.0 73.0	0.0 -4.0	123.0数	0.0/	(%,27.0 <i>)</i>	4 0.0		
73.0		***95.0	-7.0 (215:07)	.123.0) -127.0 %	0.0 j	27.0	0.0	0.0	
95.(15.0		Control of the Contro	-100.0		/%27.0 ¥ %30.0 ∗	350.0% 350.0%	* 0.07	
(102.)	13:515.0		1 CONTROL OF THE PARTY OF THE P			- 	A THE RESERVE OF THE PARTY OF T	20.0.	
132.0	12,-27.0	140.0	%-38.0°	-135.0		35.0		**************************************	
80.0			%-27.0	-135.0				ນຂໍດ.ດີ	
(2)132.((1)/45.(~~27.0	9399.0		-80.Q.Z	\$ * 0.0	-0.0	0.0	0.0	
*** 7 0.0		70.0 80.0		-127.0%		27.0°	:0.0 🕄	0.0	
80.0		, 115.0	-27.0 -29 n	-127.0°% -127.0°	30.0 35.0	°27.0	0.0	0.0.	
×115.0				-127:0	1967	27.0 27.0	0.0 %;	≈ 0.0 * 0.0	
_140.0			-40.0	-127.0%	. 0.0	27.0	0.0	* 0.0 *0.0	A-4
45,0		9399.0	-40.0	j–128.o	AND THE RESERVE TO A STATE OF THE RESERVE	.25.0 ·	0.0	0.0	341.1
.45.0				≥100.0°	S27.0 /	(30.D) :	:00.0 kg	×0.0	2
73.0				2-62.4	0.0	0.0	0.0 %	.0.0	
-86:0 5.0		5.0	-35.0	≟i28.0		25.0	0.0	- 0.0°	202
-79.0	-34.0		-40.0 -15.0	-128.0 /		(125.0 d	0.0		+ U-
45.0		73.0	4.0		27.0 27.0	627.0 227.0	0.0	0.0	
	Zine.							0.03	
								- 7	
XT= 36	5.0 × Y	T=5.0	:	. 150.O	ΥB=	45.0.4	43.3		
	ed reduction	7.00 120 120 120 120 120 120 120 120 120 1	A. A.			A SHOW AND A SHOW			1

DEPTH OF ROCK=

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 🛷 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

CASE 7,

(ドスペー

TEST POINTS

THE MIH. FS= 1.20 EFS= .99 H(X)= 90.00 G(Y)= 30.00 (R= H(X)= 150.00 G(Y)= 90.00 SR= 127.49

.1.INSIDE=2.5:1.COMP. ASH.ROCK:CLAY@2:1.PHI=30 uEPTH OF ROCK= 49.0 FT) : 사용하다

.1.	χές Υ1 .	28. Est		, Ы :	F2	. F1 . ∤	÷ic2	C1
_ ::=3\£#::::		444		44.5				4
-9399.OJ]-49.0	-112.0	%-49.0	-1000.0	* 0.0.	100.0	0.0	9999.0
-112.0 <u>.</u>	% - 49.0	9399.0	The second second second second	-1000.0	25.0	100.0	%;₹ 0. 0	9999.N
-9399.D	報義於於於於 이 도로되어 없	1-110.0	9-46.5	87-62.4	O.O.	- 63:0. 0 (7 ; 0.0.	
	-49. 0	£110.0	46.5	"-128.0°	0.0	25.0	7.0.0	7.j; 0.0
	2 46.5	9-105.5	* #41.5	}≒128.0	0.0	25.0	``.O.O	₩0. 0 ;
	₩-41.5	%−,100.0%	約439.5	128.0	394x0.0.	演员25.0	(0,0)	0.0
	v;_39.5	_%,56.0	The state of the s	} - 129.0	35.0	¥25.0	7.7- O.O,	
££86.0	-37.0	%-79 . 0	-34.0	-127.0	35.0	27.0	* 0.0	-,50.0
<i>#</i> 4-79.0 °	*-34.0	-67.0	<i>:</i> 2=29.0	123.0	35.0	27.0	::€0.0	- 3 -4,0.0
<u>7-100.0</u>	∍ , 39.5	%-85.0	\$30.0	135.0	0.0	35.0	* \$0.0	0.0
s:-85.0	30.0	∴-67.0	## 29. 0	135.0	0.0	35.0		~~~ o. o . ·
767.0	7-29.0	249.0	0.0	123.0	0.0	78.27.0	0.0	7-17 0.0
49.0	* ;-0.0	%≈ 65. 0	. A. O. O	123.0		*** 27. 0	7. O.O	
65.0		73.0		123.0	- 0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	σ.ο	27.0	0.0	*0.0
	-15.0	102.0	-15.0	-100.0	0.0	<u>30.0</u>	0.0	***********
102.0	-15.0	132.0	-27.0	-100.Q	0.0	<u>30.0</u>	0.0	0.0
-4132.0	7-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	**** 0. 0
%80.0	-27.0	132.0	- 27.0	-135.0	30.0	35.0	0.0	0.0
(_132.0	×-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	<u>30.0</u>	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	$\frac{30.0}{50}$	27.0	0.0	0.0
80.0	27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	70.0 90.0
115.0	~29.0	140.0	+38.0	-127.0	35.0	27.0	0.0	7.0.0 1.0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	0.0	20.0
145.0	-40.0	9399.0	-40.0	128.0	0.0	25.0	. O.O	200.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	30.0 		20.0
73.0	∴-4.0	9399.0	-4.0	-62.4	0.0	~ 25.0	35 ,0.0	50.0°
-86.0	-37.0	5.0	-35.0	-128.0	27.0	- 2J.U -∷25.0		5.560.0
##5.0 ••••••••••••••••••••••••••••••••••••	*-35.0	145.0	-40.0 15 3	-128.0	27.0			0.0
3-79.0	.4-34.0	∞.45.0 72.0	-15.0	-127.0	27.0 27.0	%27.0 3 27.0 ≉		0.04
45.0	-15.0	73.0	-4.0	-127.0	Cí.U	⊆ 0 .:		
		自然的编辑 化二氯酚银矿 化氯化二氢硫酸矿	化二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十	erano del Sono eschel establich	(1977年),我们们不知的人,还能够成为了	CONTRACTOR OF THE PROPERTY OF	"在大学生"在一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个	

KT= 3065.0 YT= -5.0 XB= 150.0 % YB= -45.0 %

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

CASE 7 SHALLOW

TEST POINTS

THE MIN. FS= \$1.16 EFS= .95 H(x)= 90.00 3 G(Y)= 20.00 3 R=

				±	· · · · · · · · · · · · · · · · · · ·	
147						
			& INITIAL DIKE		Sir Son Williams	
///0				(49,0) (65,0)	12 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	<u> </u>
1100				COMPACTED CLAY 2 CLAY	13,-4)	
090 _			V	$\delta = 123$, $\overline{c} = 0$; $\overline{\phi} = 27^{\circ}$ $\overline{c} = 0^{\circ}$ $\overline{\phi} = 0^{\circ}$	= 27° Compacted Ash $3^{\circ}=-100$; $\overline{c}=0$; $\overline{\phi}=28^{\circ}$	1090
080_	ROCK FILL (-85,-30)		CLAY 8=-127; c	$\bar{c}=0$; $\phi=2.7^{\circ}$	25) (80,-27)	_(132,-27)
070	ROCK FILL 1=+135 \$=35 \$=35		(5,-35)		7 = -135 7 = -135	A5H 1=-80 =0; J=0
1060_(-9.	(-105.5,-41.5) 7-100,-39.5)		INSITU SOIL 8=-128; C=0; 7	Φ=25°		(145,-40) INSITU 1060
(-0	(-9399,-49) (-1/2,-49)					
1050					" "	1050
	-80	-70 -60 -50 -40 -30 -20	Γ/ ρ			140 150 160 170 180
, -140	-/30 -/20 110 -100					
		A STATE OF THE STA		と 自per in [] 自ltalle little little 		

 3HEE1	Ur	
JOHN	SEVIER	
DISPOSA	AREA	11/11
		Ост. 26,84
CHECKED	DATE	

RESULTS FROM SLOPEZ PROGRAM

/.	PROFILE INSIDE SLOPE 3:1 COMPACTED ASH ON DEPOSITED ASH	F. S. 1.02	
2,	INSIDE SLOPE 2:1 COMPACTED ASH ON ROCK TOE COMPACTED ASH $\phi = 28^{\circ}$	1.04	
3,	INSIDE SLOPE 2:1 COMPACTED ASH ON ROCK TOE COMPACTED ASH $\phi = 30^{\circ}$	1.09	
4.	INSIDE SLOPE 2.5:1 COMPACTED ASH ON ROCK TOE COMPACTED ASH $\phi = 28^{\circ}$	1.24	
5.	INSIDE SLOPE 2,5:1 COMPACTED ASH ON ROCK TOE COMPACTED ASH Ф=30°	1.31	
6.	INSIDE SLOPE: CLAY @ 2:1 COMPACTED ASH @ 2.5:1 ROCK TOE; COMPACTED ASH \$=28°	1.17	SHALLOW 1.15
7.	INSIDE SLOPE: CLAY @ 2:1 COMPACTED ASH @ 2.5:1 ROCK TOE; COMPACTED ASH \$\P=30^\circ\$	1.20	SHALLOW 1.16

 	SHEET OF
	JOHN SEVIER
	DISPOSAL AREA "J"
	COMPUTED 2000 DATE OCT. 29,84
	CHECKED DATE

RECOMMENDATION:

USE INSIDE SLOPE W'TH CLAY FILL @ 2:/ SLOPE, COMPACTED ASH FILL @ 2:5: | SLOPE, AND ROCK FILL AT THE TOE OF THE SLOPE AS SHOWN IN FIGURE 1.

THE SLOPE WILL BE REANALYZED WITH THE LABORATORY TESTING RESULTS OF R TRIAXIAL SHEAR TESTS, WHEN THE RESULTS ARE AVAILABLE.

-1	S)			: 4.		15-		Ā	TE	71 <u>0</u> E-57	•													•				
===	MPUTE	:O 1	3Y /	R. K	1. /	00,	VE.	<u></u>	DAT	€ .	×	×	×	×	×c	HEC	(ED	BY			- 42 - 44 - 44 - 44 - 44 - 44 - 44 - 44	7	• :	DATI	E .			
				1	N	W.	1	7	U	1	B	g	Ó	7	4	2	¥	ß	'n	1	4	6	8	à	2	3	R	-
Andreas and a pure of the control of	COMESIC		7 %	8886	6666	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Ö		0	0	
	COHESION		ر ا ا	0	0	0	0	0	0	0	0	0	0	0	0	0	O	0	C	0	0	0	9	0	Ċ.	0	0	
	M MELOW	L	シートなり	001	00/	0	25	2.5	25	25	27	35	38	27	27	27	27	27	25	25	27	0	25	. 25	2.5	25	23	
	7. ABOVE	3 A O C C	3.5.2 (Ny	0	25	0	0	0	0	35	35	0	0	0.	0	0	0	0	22	23	0	0	27	27	27.	25	27	
		P.OIST	3, W (N) W.	- 1000	-1000	-62.4	-128	125	125	125	123	135	(36	123	123	123	123	-127	-120	-128	-127	-62.4	125	- 128	-128	١	-127	
(3)			", (N) Z/ 12, "	8	- 49	-46.5	-46.5	-41.5		-37	-29	-30	-29	-26	o	0	+-	-35	-38	-38	-35	•	-35.5-37	-35	-35	-35.5-37		
101100			1, X2 (N) 2, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	-//2	9399	011-	0//-	-105.5		-86	-67	- 85	-67	-60	8	B	.9/	28	64	9399	9399	9389	-20-62		26	-20-62	/6	
7101 - 1			X (N	61-	- 49	-46.5	64-	- 16.5	-41.5	-39.5	- 37	-39.5	-30	-29	-26	0	0	1	-35	-38	-35	-4	-37	-35,5-37	- 35	-46.5	- 35.5	
Ī			(N) 1×	-9399	-112	19399	-//2	0//-	2/08.5	00/-	- 56	1 .	2.4.5	-67	.60	ď	•	/6	10	63	26	/6	78-	-20-62	V	-110	-20-02-	
いこののと・	L	기		130	1	150	4	2/	281	130		200			ــــــــــــــــــــــــــــــــــ			220	280	290	300	3/0	320	330	340	350	360	
	15.				1 ह	V / `	Ź.					(L1)	MIT		o L	INE	s) .		뒣냋						1, 11 A,	•		

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PROJECT - JOHN SEVIER

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SLOPE STABILITY ANALYSIS OLD, SLOPE 2

JSF ASH POND "J" R-EFF TEST@STA 41+75, 3:1 SLOPE

COMPUTED BY

DATE

-													-											DA		 .		
48	COHESION	BELOW		6666	6666	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	COHESION	ABOVE	, C2 (N)		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7.7	2	BELOW	(Z) LA: (Z)		001	0	25	25	25	27	35	35	27	22	27	27	3	24	20	31	22	12	27	25	25	27	27	20
DESCRIPTION		ABOVE	35 35 (N) 2		25	0	0	0	35	35	0	0	0	0	0	0	0	Q	0	27	12	24	20	27	127	20	0	44
ALPHAMERIC DE	UNIT WT. (PCF)	40187	(N) W ₆₂₈₅	8	-1000	-62.4	- 128	-128	1-128	-127	135	135	123	123	123	-127	-//5	50/-	-95	-115	127	127	-/27	921-	-128	121-	-127	-95
(Z) ALPY			22 (N)	-49	-49	-46.5	-41.5	-39.5	-37	-29	- 30	-29	0	0	7-	0/-	-15	07-	- 35	0/-	-15	02-	- 35	-38	- 38	-35	-35	20
0 UTP UT			14 15 X2 (N) 21	711-	9399	0//-	-105,5	00/-	-86	-67	-85	19-	20	R	44	56	99	76	91	56	38	48	78	84	9399	3/	9399	2/2
2 1 - FULL 0		Z	$_{\rm s}$ $\times_{\rm l}$ (N)	-49	-49	-46,5	-46.5	-41.5	-39,5	-37	-39.5	-30	62-	0	0	-4	-10	-15	-20	Q-	01-	-/5	-20	-35	- 38	-35	-35	-20
EI= C		ال ا ا ا	, (N) <u>,</u>	-9399	-112	-9399	011-	-105,5	-100	-86	00/-	-85	-67	92	36	44	56	99	76	28	28	38	48	78	84	78	16	48
KODEI		보	LINE		7	8	4	5	9	/	00	6	0/	1	12	13	14	N	16	17	8	19	22	17	22	23	74	25

O - LIMITED OUTPUT

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(LIMIT 50 LINES

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ONE CARD FOR EACH FAILURE ARC CONSIDERED

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50 LINES)

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(COMPUTER OUTRUT) COMPACTED ASH.
SLOPE STABILITY
(INSIDE SLOPE)

CASE

84/10/24.11.03.58. PROGRAM SLOPE2

بنعتب

00110 JSF ASH POND "J", R-EFF,OUTSIDE=4:1,INSIDE=3:1,COMPACTED ASH (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

-9399.0	×1	Y1	X2 ⁻	Y2	hJ	F2	F1	C2	Ci
-112.0	-9399.n	-49. ft	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						25.0	100.0	0.0	9999.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				-46.5	-62.4	0.0	0.0	0.0	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						0.0	25.0	0.0	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				-41.5	-128.0	0.0	25.0	0.0	0.0
-100.0 -39.5 -86.0 -37.0 -128.0 35.0 25.0 0.0 0.0 -86.0 -37.0 -79.0 -34.0 -127.0 35.0 27.0 0.0 0.0 -79.0 -34.0 -67.0 -29.0 123.0 35.0 27.0 0.0 0.0 0.0 -79.0 -34.0 -67.0 -29.0 123.0 35.0 27.0 0.0 0.0 0.0 -100.0 -39.5 -85.0 -30.0 135.0 0.0 35.0 0.0 0.0 0.0 -85.0 -30.0 -67.0 -29.0 135.0 0.0 35.0 0.0 0.0 0.0 -67.0 -29.0 49.0 0.0 123.0 0.0 27.0 0.0 0.0 0.0 49.0 0.0 65.0 0.0 123.0 0.0 27.0 0.0 0.0 65.0 0.0 77.0 -4.0 123.0 0.0 27.0 0.0 0.0 0.0 77.0 -4.0 110.0 -15.0 -127.0 0.0 27.0 0.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 146.0 -26.0 185.0 -40.0 -85.0 0.0 10.0 20.0 0.0 0.0 146.0 -27.0 9399.0 -27.0 -80.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0					-128.0	0.0	25.0	0.0	
-86.0 -37.0 -79.0 -34.0 -127.0 35.0 27.0 0.0 0.0 -79.0 -34.0 -67.0 -29.0 123.0 35.0 27.0 0.0 0.0 -79.0 -34.0 -67.0 -29.0 123.0 35.0 27.0 0.0 0.0 0.0 -100.0 -39.5 -85.0 -30.0 135.0 0.0 35.0 0.0 0.0 -85.0 -30.0 -67.0 -29.0 135.0 0.0 35.0 0.0 0.0 0.0 -67.0 -29.0 49.0 0.0 123.0 0.0 27.0 0.0 0.0 49.0 0.0 65.0 0.0 123.0 0.0 27.0 0.0 0.0 65.0 0.0 77.0 -4.0 123.0 0.0 27.0 0.0 0.0 0.0 77.0 -4.0 110.0 -15.0 -127.0 0.0 27.0 0.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -85.0 0.0 10.0 0.0 0.0 0.0 146.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 0.0 146.0 -27.0 9399.0 -27.0 -80.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0					-128.0	35.0	25.0	0.0	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					-127.0	35.0	27.0	0.0	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					123.0	35.0	27.0	0.0	0.0
-85.0 -30.0 -67.0 -29.0 135.0 0.0 35.0 0.0 0.0 -67.0 -29.0 49.0 0.0 123.0 0.0 27.0 0.0 0.0 49.0 0.0 65.0 0.0 123.0 0.0 27.0 0.0 0.0 65.0 0.0 77.0 -4.0 123.0 0.0 27.0 0.0 0.0 77.0 -4.0 110.0 -15.0 -127.0 0.0 27.0 0.0 0.0 110.0 -15.0 146.0 -27.0 -100.0 0.0 24.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 146.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 146.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 146.0 -27.0 9399.0 -27.0 -80.0 0.0 0.0 0.0 0.0 0.0 0.0 146.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 0.0 146.0 -27.0 9399.0 -27.0 -80.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0						0.0	35.0	0.0	0.0
-67.0 -29.0 49.0 0.0 123.0 0.0 27.0 0.0 0.0 49.0 0.0 65.0 0.0 123.0 0.0 27.0 0.0 0.0 65.0 0.0 77.0 -4.0 110.0 -15.0 -127.0 0.0 27.0 0.0 0.0 77.0 -4.0 110.0 -15.0 -127.0 0.0 27.0 0.0 0.0 110.0 -15.0 146.0 -27.0 -100.0 0.0 24.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -85.0 0.0 10.0 0.0 0.0 80.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 45.0 -15.0 70.0 -25.0 -127.0 24.0 27.0 0.0 0.0 80.0 -27.0 105.0 -29.0 -127.0 24.0 27.0 0.0 0.0					135.0	0.0	35.0		
49.0 0.0 65.0 0.0 123.0 0.0 27.0 0.0 0.0 65.0 0.0 77.0 -4.0 123.0 0.0 27.0 0.0 0.0 77.0 -4.0 110.0 -15.0 -127.0 0.0 27.0 0.0 0.0 110.0 -15.0 146.0 -27.0 -100.0 0.0 24.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 80.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 146.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 146.0 -27.0 9399.0 -27.0 -80.0 0.0 0.0 0.0 0.0 45.0 -15.0 70.0 -25.0 -127.0 24.0 27.0 0.0 0.0 105.0							27.0		0.0
65.0				0.0	123.0	0.0	27.0		0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				-4.0	123.0	0.0			
110.0 -15.0 146.0 -27.0 -100.0 0.0 24.0 0.0 0.0 146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 146.0 -26.0 185.0 -40.0 -85.0 0.0 10.0 0.0 0.0 0.0 80.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 146.0 -27.0 9399.0 -27.0 -80.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0			110.0	-15.0	-127.0	0.0			0.0
146.0 -27.0 150.0 -40.0 -90.0 10.0 20.0 0.0 0.0 146.0 -26.0 185.0 -40.0 -85.0 0.0 10.0 0.0 0.0 80.0 -27.0 146.0 -27.0 -90.0 24.0 20.0 0.0 0.0 146.0 -27.0 9399.0 -27.0 -80.0 0.0 0.0 0.0 0.0 45.0 -15.0 70.0 -25.0 -127.0 24.0 27.0 0.0 0.0 70.0 -25.0 80.0 -27.0 -127.0 24.0 27.0 0.0 0.0 80.0 -27.0 105.0 -29.0 -127.0 24.0 27.0 0.0 0.0 80.0 -27.0 105.0 -29.0 -127.0 20.0 27.0 0.0 0.0 105.0 -29.0 145.0 -40.0 -128.0 20.0 25.0 0.0 0.0 145.0 -40.0 150.0 -128.0 20.0 25.0 0.0 0.0 185.0 <t< td=""><td></td><td></td><td></td><td>-27.0</td><td>-100.0</td><td>0.0</td><td></td><td></td><td></td></t<>				-27.0	-100.0	0.0			
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146.0 -27.0 9399.0 -27.0 -80.0 0.0			146.0	-27.0	-90.0°	24.0			0.0
45.0 -15.0 70.0 -25.0 -127.0 24.0 27.0 0.0 0.0 70.0 -25.0 80.0 -27.0 -127.0 24.0 27.0 0.0 0.0 80.0 -27.0 105.0 -29.0 -127.0 20.0 27.0 0.0 0.0 105.0 -29.0 145.0 -40.0 -127.0 20.0 27.0 0.0 0.0 145.0 -40.0 150.0 -40.0 -128.0 20.0 25.0 0.0 0.0 150.0 -40.0 185.0 -40.0 -128.0 10.0 25.0 0.0 0.0 185.0 -40.0 9399.0 -40.0 -128.0 0.0 25.0 0.0 0.0 45.0 -15.0 10.0 -15.0 -100.0 27.0 24.0 0.0 0.0 77.0 -4.0 9399.0 -4.0 -62.4 0.0 0.0 0.0 -86.0 -37.0 5.0 -35.0 -128.0 27.0 25.0 0.0 5.0 -35.0 <		-27.0	9399.0	-27.0	-80.0	0.0			0.0
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105.0 -29.0 145.0 -40.0 -127.0 20.0 27.0 0.0 0 145.0 -40.0 150.0 -40.0 -128.0 20.0 25.0 0.0 0 150.0 -40.0 185.0 -40.0 -128.0 10.0 25.0 0.0 0 185.0 -40.0 9399.0 -40.0 -128.0 0.0 25.0 0.0 0 45.0 -15.0 10.0 -15.0 -100.0 27.0 24.0 0.0 0 77.0 -4.0 9399.0 -4.0 -62.4 0.0 0.0 0.0 0 -86.0 -37.0 5.0 -35.0 -128.0 27.0 25.0 0.0 0 5.0 -35.0 145.0 -40.0 -128.0 27.0 25.0 0.0 0			105.0	-29.0	-127.0	20.0			0.0
145.0 -40.0 150.0 -40.0 -128.0 20.0 25.0 0.0 0 150.0 -40.0 185.0 -40.0 -128.0 10.0 25.0 0.0 0 185.0 -40.0 9399.0 -40.0 -128.0 0.0 25.0 0.0 0 45.0 -15.0 10.0 -15.0 -100.0 27.0 24.0 0.0 0 77.0 -4.0 9399.0 -4.0 -62.4 0.0 0.0 0.0 0 -86.0 -37.0 5.0 -35.0 -128.0 27.0 25.0 0.0 0 5.0 -35.0 145.0 -40.0 -128.0 27.0 25.0 0.0 0		-29.0	145.0	-40.0	-127.0	20.0			0,0
150.0 -40.0 185.0 -40.0 126.0 10.0 25.0 0.0 0 185.0 -40.0 9399.0 -40.0 -128.0 0.0 25.0 0.0 0 45.0 -15.0 10.0 -15.0 -100.0 27.0 24.0 0.0 0 77.0 -4.0 9399.0 -4.0 -62.4 0.0 0.0 0.0 0 -86.0 -37.0 5.0 -35.0 -128.0 27.0 25.0 0.0 0 5.0 -35.0 145.0 -40.0 -128.0 27.0 25.0 0.0 0	145.0	-40.0	150.0	-40.0	-128.0				0.0
185.0 -40.0 9399.0 -40.0 -128.0 0.0 25.0 0.0 0 45.0 -15.0 10.0 -15.0 -100.0 27.0 24.0 0.0 0 77.0 -4.0 9399.0 -4.0 -62.4 0.0 0.0 0.0 0 -86.0 -37.0 5.0 -35.0 -128.0 27.0 25.0 0.0 0 5.0 -35.0 145.0 -40.0 -128.0 27.0 25.0 0.0 0	150.0	-40.0	185.0	-40.0		10.0			0.0
77.0 -4.0 9399.0 -4.0 -62.4 0.0 0.0 0.0 0 -86.0 -37.0 5.0 -35.0 -128.0 27.0 25.0 0.0 0 5.0 -35.0 145.0 -40.0 -128.0 27.0 25.0 0.0 0		-40.0	939 9 .0	-4.0.0	-128.0				0.0
-86.0 -37.0 5.0 -35.0 -128.0 27.0 25.0 0.0 0 5.0 -35.0 145.0 -40.0 -128.0 27.0 25.0 0.0 0	45.0	-15.0	10.0	-15.0	-100.0				0.0
5.0 -35.0 145.0 -40.0 -128.0 27.0 25.0 0.0 0	77.0	-4.0	9399.0	-4.0					0.0
5.0 -35.0 145.0 -40.0 120.0 27.0 07.0 0	-86.0	-37.0	5.0						
-79.0 -34.0 77.0 -4.0 -127.0 27.0 27.0 0.0 U	5.0	-35.0	145.0						0.0
	-79.0	-34.0	77.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT = 146.0 YT = -28.0 XB = 150.0 YB = -40.0

GRIBX= 90.0 GRIBY= 10.0 XMAX= 190.0 YMAX= 200.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.02 EFS= .69 H(X)= 150.00 G(Y)= 50.00 R= 88.11 THE MIN. EFS= .17 FS= 3.51 H(X)= 190.00 G(Y)= 100.00 R= 135.36 SBU 185.006 UNTS.

RUN COMPLETE.

O.828 UNTS.

READY.

DLD,SLOPE2

READY.

GET,TAPE5=JMH46

READY.

RUN

84/10/26. 13.03.17. PROGRAM SLOPE2

CASE 2

00110 SHALLOW CIRCLE, JSF, R-EFF, DUTSIDE=4:1, INSIDE=2:1, COMPACTED ASH, ROCK (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1 °.	Y1 -	XS	Y2	tel -	F2	F1	C2	C 1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0,0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	O, O.
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	0.0	27.0	0.0	0.0
95.0	-15.0	120.0	-27.0	-100.0	0.0	28.0	0.0	0.0
120.0	-27.0	126.0	-33.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	120.0	-27.0	-135.0	28.0	35.0	0.0	0.0
120.0	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	28.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0		28.0	27.0	0.0	0.0
80.0		115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	126.0	-33.0	-127.0	35.0	27.0		0.0
126.0	-33.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	28.0	0.0	0.0
73.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0		27.0		0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0			
45.0	-15.0	73.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.04 EFS= .82 H(X)= 110.00 G(Y)= 30.00 R= 57.02 THE MIN. EFS= .78 FS= 1.12 H(X)= 150.00 G(Y)= 100.00 R= 135.10

RUN COMPLETE.

SBU 76.261 UNTS.

CU:CLOPE2 READY. GET,TAPE5=JMH47 READY. RUN

CASE 3

84/10/25. 09.41.21. PROGRAM SLOPE2

00110 PHI=30,SHALLOW CIRCLE,JSF,R-EFF,OUTSIDE=4:1,INSIDE=2:1,COMPACTED A
(ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE IMPUT DATA LINES

×1	Y1	×2	Y2 ₁	W	F2	F1	CZ	C 1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0		-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5		0.0	0.0	0.0	0 - 0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0°	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	$0 \downarrow 0$	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
	-4.0	95.0	-15.0	-127.0	0.0	27.0	0.0	0.0
95.0	-15.0	120.0	-27.0	-100.0	0.0	30.0	0.0	0.0
120.0	-27.0	126.0	-33.0	-135.0	0.0	35.0		0.0
80.0	-27.0	120.0	-27.0	-135.0	30.0	35.0	0.0	0.0
120.0	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25:0	-127.0	30.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	30.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	126.0	-33.0	-127.0	35.0	27.0	0.0	0.0
126.0	-33.0	145.0	-40.0	127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	30.0	0.0	0.0
73.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0%	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0		0.0	0.0
45.0	-15.0	73.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.09 EFS= .88 H(X) = 110.00 G(Y) = 40.00 R= 63.65 THE MIN. EFS= .80 FS= 1.15 H(X) = 150.00 G(Y) = 100.00 R= 135.10 SBU 78.541 UNTS.

READY.

84/10/25. 09.03.03. PROGRAM SLOPE2 CASE 4

00110 JSF ASH POND "J", R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMPACTED ASH,ROC (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

X1	Y1	X2	Y2	. td	F2	F1	C5	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0.	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0.	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	Ü.U
65.0	-0.0	75.0	-4.0	123.0	0.0	27.0	0.0	0.0
75.0	-4.0	102.0	-15.0	-127.0	0.0	27.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	28.0	0.0	0.0
132.0	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0°	0.0
80.0	-27.0	132.0	-27.0	-135.0	28.0	35.0	0.0	0.0
132.0	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	28.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	28.0	27.0	0 * 0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40:0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	102.0	-15.0	-100.0	27.0	28.0	0.0	0.0
75.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0		0.0	0.0
45.0	-15.0	75.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.24 EFS= .97 H(X) = 110.00G(Y) =40.00 R= 63.65 THE MIN. EFS= .93 90.00 R= 127.49 FS= 1.32 H(X) = 150.00G(Y) =SBU 80.145 UNTS.

RUN COMPLETE

84/10/25. 09.15.04. PROGRAM SLOPE2

CASE 5

00110 JSF ASH POND "J", R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMPACTED ASH,RDC (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y1	X2	Y2	W	F2	F1	cs	C 1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0.	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0.
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	-0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	00
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0.	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0		-4.0	123.0	0.0	27.0	0.0	0.0
75.0	-4.0	102.0	-15.0	-127.0	0.0	27.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	30.0	0.0	0.0
132.0	-27.0	140.0	-38:0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	132.0	-27.0	-135.0	30.0	35.0	0.0	0.0
132.0	-27.0	9399.0	-27.0	-80.0	00	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	30.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	30.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	.0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	0.0	Ü., Ü.
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	102.0	-15.0	-100.0	27.0	30.0	00	0.0
75.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86:0	-37.0	5.0		-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	$-1.5 \cdot 0$	-127.0	27.0	27.0	0.0	
45.0	-15.0	75.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT = 65.0 YT = -5.0 XB = 150.0 YB = -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.31 EFS= 1.02 H(X) = 110.00 G(Y) = 40.00 R= 63.65

THE MIN. EFS= .95 FS= 1.35 H(X) = 150.00 G(Y) = 90.00 R= 127.49

SBU 80.862 UNTS.

RUN COMPLETE.

READY. GET, TAPE5=JMH49 READY.

RUN

84/10/25. 14.09.43. PROGRAM SLOPE2

CASE 6

00110 JSF, R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMPACTED ASH,ROCK;CLAY@2:1 (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y1	X2	Y2	W	F2	F1	C2	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0		-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0 0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	
-105.5	-41.5	-100.0	-39.5	-128.0	Õ.Õ	25.0	0.0	0.0
-100.0	-39,5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0 0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0°	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	0.0	27.0	0.0	0.0
95.0	-15.0	102.0	-15.0	-100.0	0.0	28.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	28.0	0.0	0.0
132.0	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	132.0	-27.0	-135.0	28.0	35.0	0.0	0.0
132.0	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	28.0	27.0	0.8	0.0
70.0	-25.0	80.0	-27.0	-127.0	28.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.O	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	28.0	0.0	0.0
75.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-127.0	27.0	27.0	0.0	0.0 0.0
45.0	-15.0	75.0	-4.0	-127.0	27.0	27.0	0.0	0.0
							THE ME THE	O a O

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0 GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.20 EFS= .95 H(X) = 100.00 G(Y) = 30.00 R = 49.51 THE MIN. EFS= .94 FS= 1.37 H(X) = 150.00 G(Y) = 90.00 R = 127.49 SBU 83.470 UNTS.

RUN COMPLETE. OLD,JMH48 READY. OLD SLOPE2 READY. GET, TAPE5=JMH53 READY. RUN

84/10/25. 14.21.03. PROGRAM SLOPE2

CASE 7

00110 JSF,R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMP. ASH,ROCK;CLAY@2:1,PHI=30 (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y1	X2	Y2	\ul	F2	F 1	ca	/ C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	-0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39:5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86:0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	00	35.0	0.0	0 = 0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	0.0	27.0	0.0	0.0
95.0	-15.0	102.0	-15.0	-100.0	0.0	30.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	30.0	0.0	0.0.
132.0	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	0.0
80.0	-27.0	132.0	-27.0	-135.0	30.0	35.0	0.0	0.0
132.0	-27.0	9399.0	-27.0	-80.0	0.0	0.0	្រុំ ប៉ុ	0.0
45.0	-15.0	70.0	-25.0	-127.0	30.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	30.0	27.0	Ü, Ü	Ü. Ü
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	Ŭ"Ũ	0.0
115.0	-29.0	140.0	-38"0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	/ 0 . 0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	30.0	0.0	0.0
75.0	-4.0	9399.0	-4.Ü	-62.4	0.0	0.0	O.O	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0.	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0		45.0	-15.0	-127.0	27.0	27.0	0.0	0.0
45.0	-15.0	75.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE BRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.24 EFS= 1.02 H(X) = 100.00 5(Y) = 50.00 R= 65.20 THE MIN. EFS= .96 FS= 1.40 H(X) = 150.00 5(Y) = 90.00 R= 127.49 SBU 83.935 UNTS.

RUM COMPLETE.

REHIM -GET:TAPE5=JMH53 REAL . 모니네

84/11/27. 13.15.29. PROSRAM SLOPEZ

CASE 7

00110 USF.R-EFF.OUTSIDE=4:1.INSIDE=2.5:1.COMP. 95H.ROCK:CLAY@2:1.PHI=30 .05 DEPTH OF ROCK= 49.0 FT) (EROF=

THESE ARE THE INPUT DATA LINES

	TH	FRE HET 1	1 1 Laure - 1	•				
		×2	Y2	₩	F2	F1	02	C,1
71 -939.0 -112.0 -9399.0 -110.0 -105.5 -100.0 -105.	-35. -34.	-112.0 939.0 -110.0 -105.5 -100.0 -105.0 -10	-49.0 -49.0 -46.5 -46.5 -37.0 -39.0 -39.0 -29.0 -4.0 -27	123.0 123.0 123.0 -127.0 -100.0 -100.0 -135.0 -135.0 -137.0 -127.0 -127.0 -127.0 0 -127.0 0 -128.0 0 -128.0 0 -128.0 0 -127.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	25.0 25.0 27.0	0. 0. 0.	
	<u> </u>		. O	$\times B = 150.$	· **			

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0 -γMAX= 100.0 GRIDK= 90.0 GRIDY= 10.0 KMAK= 150.0 INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS

TEST POINTS

35.37 H(x) = -90.00 - G(x) = -20.00F' =THE MIN. FS= 1.16 EFS= .95 R= 35.3 6(7) = -20.00H(X) = 90.00THE MIN. EFS= .95 FS= 1.16 SBU AN, 995 WHTS.

RUM LO METE.

OLD,SLOPE2 READY. GET,TAPE5=JMH54 READY. RUN

84/11/27. 13.33.34. PROGRAM SLOPE2 (

CASE 6

00110 JSF,R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMP. ASH,ROCK;CLAY92:1,PHI=28 (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y1	×a	ŶΞ	ul	F8	F1	CE	01
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0,0	9999.0
-112.0	-49.0	9399.0		-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-63.4	0.0	0.0	ប៉ុ.ប៉េ	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	.00	25.0	0.0	0.0,
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	Sale in the	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0		0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	ប. ប	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	ា ព្រ	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	Ú. Ú	27.0		0.0
65.0	0.0	73.0	-4.0	123.0	, O,O	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	0.0	27.0	Û. Ü	0.0
95. n	-15.0	102.0	-15.0	-100.0	0.0	E,8.0	0.0	0.0
163.	-15.0	132.0	-27.0	-100.0	0.0	39.0	0.0	0.0
	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	0.0
A Light	-87.0	132.0	-27.0	-135.0	28.0	35.0	0.07	0.0
132.0	-27.0	9399.0	-27.0	-80.0	0.0	0. 0	0.0	0.0
45.0	-15.0	70.0	-25.0	-127.0	28.0	27.0	0.0	0.0
70.0	-25.0	80.0	-27.0	-127.0	28.0	27.0	0.0	0.0
30.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0. ប	25.0	Ü,Ü	0.0
45.0	-15.0	95.0	-15.0		27 . 0	29.0	0.0	0.0
73.0	-4.0	9399.0	-4.0	-62,4	្រួម៉	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0		27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0		27.0	25.0	0.0	
-79.0	-34.0	45.0	-15.0		27.0	27.0	0.0	0.0
45.0	-15.0	.73.0	-4.0	-187.O	27.0	27.0	0.0	0,0

XT = 65.0 YT = -5.0 XB = 150.0 YB = -45.0

GRIDX= 90.0 GRIDY= 10.0 XMAX= 150.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAKIMUM F.S. TO BE PRINTED IS . 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIM. F3= 1.15 EFS= .94 H(X)= 90.00 5(Y)= <math>20.00 R= 35.37 THE MIM. EF3= .93 FS= 1.16 H(X)= 90.00 6(Y)= <math>10.00 R= 29.16 SBU 66.603 UNTS.

RUN COMPLETE.

READY. GET,TAPE5=JMH54 READY. RUN

~ 11727. 15.53.10. PROGRAM SLOPE2

CASE 6

00110 USF.R-EFF, DUTSIDE=4:1.INSIDE=2.5:1,CDMP. ASH, RDCK; CLAY@8:1,PHI=28 (SRQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	¥1	XB	Y2	!.!	F2	Fi	ÇΖ	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0		-1000.0	25.0	100.0	u. A	9999.0
-999a,0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	:	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39,5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	ប៉ុ. ប៉ុ	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	Ů. Ú
73.0	-4.0	95.0	-15.0	-127.O	0.0	27.0	0.0	0.0
95.0	-15.0	102.0	-15.0	-100.0	0.0	28.0	0.0	0.0
103.0	-15.0	132.0	-27.0	-100.0	0.0	28.0	0.0	0.1
132.0	-27.0	140.0	-38.0	-135,0	0.0	35.0	0.0	0.0
30.0	-27.0	132.0	-27.0	-135.0	28.0	35.0	0.0	0.0
132.0	-27.0	9399.0	-27.0	-80.0	0.0	0.0	0.0	0.0
45.0	-15.0	70.0	-25.O	-127.0	28.0	27.0	0.0	0.0
70.0	-25.0	8:0.0	-27.0	-127.0	28.0	27.0	0.0	0.0
80.0	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29,0	140.0	-39.0	-127.0	35.0	27.0	0.0	0.0
140.0	-39.0	145.0	-4 0.0	-127.0	0.0	27.0	0.0	0.0
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	28.0	o. o	0.0
73.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	ລີ. ປ	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-129.0	27.0	25.0	0.0	ů. ů
-79.0	-34.0	45.Ü	-15.0	-127.0°	27.0	27.0	0.0	0.0
45.0	-15.0	73.0	-4.0	-187.0	27.0	27.0	0.0	0.0

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0

GRIDX= 90.0 GRIDY= 30.0 XMAX= 150.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.17 EFS= .93 H(X)= 100.00 G(Y)= 30.00 R= 49.51 THE MIN. EFS= .93 FS= 1.17 H(X)= 100.00 G(Y)= 30.00 R= 49.51 SBU 58.122 UNTS.

RUM COMPLETE.

. REPOY. 364.7APE5=JMH53 3640Y. RJM

84 11727. 13.09.06. 289 --- SLOPE2

CASE 7

UNITED USF,R-EFF,OUTSIDE=4:1,INSIDE=2.5:1,COMP. ASH,ROCK;CLAY@2:1,PHI=30 CEROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	¥1	X2	, Y2	ig	FE	F1	C2	F- 1
				.,	-		U.C.	C 1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
-112.0	-49.0.	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
- () () . 0	-45.5	-105.5	-41.5	-128.O	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0,0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0,0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39,5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.O	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	27.0	0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65. 0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
73.0	-4.0	95.0	-15.0	-127.0	0.0	27.0	0.0	0.0
95.0	-15.0	108.0	-15.0	-100.0	0.0	30.0	0.0	0.0
102.0	-15.0	132.0	-27.0	-100.0	0.0	30.0	0.0	0.0
132.0	-27.0	140.0	-38.0	-135.0	0.0	35.0	0.0	0.0
30.0	-27.0	132.0	-27.0	-135.0	30,0	35.0	0.0	. 0.0
133.0	-27.0	9399.0	-27 . 0	-80.0	0.0	0.0	0.0	0.0
45. 0	-15.0	70.0	-25.0	-127.0	30.0	27.0	0.0	0.0
70.0	-25.0	80.O	-27.0	-127.0	30.0	27.0	0.0	0.0
80.O	-27.0	115.0	-29.0	-127.0	35.0	27.0	0.0	0.0
115.0	-29.0	140.0	-38.0	-127.0	35.0	27.0	0.0	0.0
140.0	-38.0	145.0	-40.0	-127.0	Ü, Ü	27.0	0.0	ô.o
145.0	-40.0	9399.0	-40.0	-128.0	0.0	25.0	0.0	0.0
45.0	-15.0	95.0	-15.0	-100.0	27.0	30.0	0.0	0.0
73.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-129.0	27.0	25.0	0.0	0.0
5.0	-35.0	145.0	-40.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	45.0	-15.0	-187.0	27.0	27.0	0.0	0.0
45.0	-15.0	73.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 65.0 YT= -5.0 XB= 150.0 YB= -45.0 SRIDX= 90.0 SRIDY= 30.0 XMAX= 150.0 YMAX= 130.0 INCX= 10 INCY= 10 INCR= 10

THE MAKIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POTHT

THE MIN. 655 1.20 EFS= H(X)= 90.00 , 99 G(Y) =R= 43.02 30.00 THE mim. EFS= .95 FS= 1.39 H(X) = 150.00(5 (Y) = 90.00 R= 127.49 82.772 UMTS. SEU

RUM COMPLET-OLD:JMH53 READY. JOHN DEVIER HEH DISPOSAL "J".

SLOPE STABILITY

OUTSIDE SLOPE CHANGED FROM Z:1 TO 4:1

(COMPUTER OUTPUT)

JMH39 IS A LOCAL FILE SBU 0.312 UNTS. READY. OLD, SLOPE2 READY. FTN READY. GET, TAPE5=JMH39 READY. RUN 84/08/13. 08.03.12. PROGRAM SLOPE2 110 USF ASH POND "J", R-EFF,@STA.41+75,3.5:1 SLOPE,R BAR (EROF= . 05 DEPTH OF ROCK= 49.0 FT) THESE ARE THE INPUT DATA LINES $\times 1$ Y1 X2 72 l,l F2 F1 02 C1-9399.0 -49.0-112.0 -49.0 -1000.0 0.09999.0 100.0 0.0-112.0-49.09399.0 -49.0 -1000.025.0 100.0 0.09999.0 -9399.0 -46.5-110.0-46.5-62.4 0.00.00.00.0-112.0 -49.0-110.0 -46.5-128.0 0.025.0 0.00.0-110.0-46.5 -105.5-128.0 -41.50.025.0 0.00.0-105.5-41.5-39.5 -100.0-128.0 0.025.0 0.00.0-100.0-39.5 -86.0-37.0 -128.0 35.0 25.0 0.00.0-86.0 -37.0 -75.0-32.5 -127.035.0 27.0 0.0 0.0-75.0-32.5 -67.0-29.0123.0 35.0 27.0 0.00.0-100.00-39.5-85.0 -30.0 135.0 0.035.0 0.0 0.0-85.0 -30.0 -67.0-29.0135.0 0.035.0 0.00.0 -29.0 -67.034.5 0.0123.0 0.027.0 0.00.0 34.5 50.5 0.00.0123.0 0.027.0 0.00.050.5 -4.0 0.058.5 123.0 0.027.0 0.00.058.5 -4.070.5 -10.0-127.00.027.0 0.00.070.5 -10.080.5 -15.0-120.00.033.0 0.00.080.5 -15.0110.5 -30.0 -110.00.029.0 0.00.0110.5 -30.0 115.5 -35.0 -95.00.0 24.0 0.00.028.0 -10.035.0 -13.5123.0 33.0 27.0 0.00.035.0 -13.538.0 -15.0-127.033.0 27.0 0.00.038.0 -15.068.0 -30.0 -127.028.0 27.0 0.00.068.0 -30.0 78.0 -35.0 -127.024.0 27.0 0.00.078.0 -35.0 84.0 -38.0 -128.027.0 25.0 0.00.084.0 -38.0 9399.0 -38.0 -128.0 27.0 25.0 0.00.078.0 -35.0 115.5-35.0-127.024.0 27.0 0.00.0115.5 -35.0 9399.0 -35.0 -127.00.027.0 0.00.068.0-30.0 110.5 -30.0 -95.028.0 24.0 0.0 0.0 110.5 -30.0 9399.0 -30.0 -70.00.00.00.00.038.0 -15.080.5 -15.0-110.033.0 28.0 0.0 0.028.0 -10.043.0 -10.0117.0 27.0 33.0 0.00.043.0 -10.070.5 -10.0-120.027.0 33.0 0.00.058.5 9399.0 -4.Ù -4.0-62.40.00.00.00.0-86.0 -37.0 5.0-35.0 -128.027.0 25.0 0.00.05.0 -35.078.0 -35.0 -128.027.0 25.0 0.00.0-75.0-32.5 35.0 -127.0 -13.527.0 27.0 0.00.035.0 -13.543.0 -120.0 -10.033.0 33.0 0.00.043.0 -10.0-127.0 58.5 -4.027.0 27.0 0.0 0.0

XT = 34.5 YT = -5.0 XB = 34.5 YB = -45.0

GRIDX= 70.0 GRIDY= 20.0 XMAX= 170.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

REPLACED

77 Q,,RL JMH39 ||

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.28 EFS= .99 H(X) = 100.00 G(Y) = 50.00 R= 85.54 THE MIN. EFS= .99 FS= 1.28 H(X) = 100.00 G(Y) = 50.00 R= 85.54

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

×1	ΥΊ	X2	Y2	W	F2	F1	ca	Ci
9399.0	-49.0	112.0	-49.0	-1000.0	0.0	100 A		
112.0	-49.0	- 9 399.0		-1000.0	25.0	100.0	0.0	9999.0
9399.0	-46.5	110.0	-46.5	-62.4	0.0	100.0	0.0	9999.0
112.0	-49.0	110.0	-46.5	-128.0	0.0	0.0 25.0	0.0	0.0
110.0	-46.5	105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
105.5	-41.5	100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
100.0	-39.5	86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
86.0	-37.0	75.0	-32.5	-127.0	35.0	27.0	0.0	0.0
75.0	-32.5	67.0	-29.0	123.0	35.0	27.0	0.0	0.0
100.0	-39.5	85.0	-30.0	135.0	0.0	35.0	0.0	0.0
85.0	-30.0	67.0	-29.0	135.0	0.0	35.0	0.0	0.0
67.0	-29.0	-34.5	0.0	123.0	0.0	27.0	0.0	0.0
-34.5	0.0	-50.5	0.0	123.0	0.0	27.0	0.0 0.0	0.0
-50.5	0.0	-58.5	-4.0	123.0	0.0	27.0	v.v 0.0	0.0
-58.5	-4.0	-70.5	-10.0	-127.0	0.0	27.0	0.0 0.0	0.0
-70.5	-10.0	-80.5	-15.0	-120.0	0.0	33.0	0.0 0.0	0.0
-80.5	-15.0	-110.5	-30.0	-110.0	0.0	28.0	0.0 0.0	0.0
-110.5	-30.0	-115.5	-35.0	-95.0	0.0	24.0	0.0	0.0
-28.0	-10.0	-35.0	-13.5	123.0	33.0	27.0	0.0	0.0
-35.0	-13.5	-38.0	-15.0	-127.0	33.0	27.0	0.0	0.0
-38,0	-15.0	-68.0	-30.0	-127.0	28.0	27.0	0.0	0.0 0.0
-68.0	-30.0	-78.0	-35.0	-127.0	24.0	27.0	0.0	0.0
-78.0	-35.0	-84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
-84.0		-9399.0	-38.0	-128.0	27.0	25.0	0.0	0.0
-78.0	-35.0	-115.5	-35.0	-127.0	24.0	27.0	0.0	0.0
-115.5		-9399.0	-35.0	-127.0	0.0	27.0	0.0	0.0
-68.0	-30.0	-110.5	-30.0	-95.0	28.0	24.0	0.0	0.0
-110.5		-9399.0	-30.0	-70.0	0.0	0.0	0.0	0.0
-38.0	-15.0	-80.5	-15.0	-110.0	33.0	28.0	0.0	0.0
-28.0	-10.0	-43.0	-10.0	117.0	27.0	33.0	0.0	0.0
-43.0	-10.0	-70.5	-10.0	-120.0	27.0	33.0	0.0	0.0
-58.5		- 9 399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
86.0	-37.0	-5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
-5.0	-35.0	-78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
75.0	-32.5	-35.0	-13.5	-127.0	27.0	27.0	0.0	0.0
-35.0	-13.5	- 4 3.0	-10.0	-120.0	33.0	33.0	0.0	0.0
-43.0	-10.0	-58.5	-4.Û	-127.0	27.0	27.0	0.0	0.0
								था चार्च ।

 XT = -34.5
 YT = -5.0
 XB = -34.5
 YB = -45.0

 GRIDX = 10.0
 GRIDY = 150.0
 XMAX = 140.0
 YMAX = 250.0

 INCX = 10
 INCY = 10
 INCR = 10

 THE MAXIMUM F.S. TO BE PRINTED IS
 0.00

 THE MAXIMUM F.S. TO BE PRINTED IS
 0.00

TEST POINTS

THE MIN. FS= 1.18 EFS= .98 H(X)= 100.00 G(Y)= 180.00 R= 228.74THE MIN. EFS= .98 FS= 1.18 H(X)= 100.00 G(Y)= 180.00 R= 228.74SBU 137.618 UNTS.

RUN COMPLETE.

?? Q,,RL UMH35 REPLACED が知る IS A LOCAL FILE

SBU 0.329 UNTS.
READY.
OLD,SLOPE2
READY.
FIN
READY.
GET,TAPE5=JMH35

USE 4:1 SLOPE JMA 11-20-84

84/08/06. 13.49.54. PROGRAM SLOPE2

READY. RUN

110 JSF ASH POND "J", R-EFF,@STA.41+75,4:1 SLOPE,R BAR (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y1	X2	Y2	W	F2	F1	62	01
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0		0.0	9999.0
-9399.0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
-79.0	-34.0	-67.0	-29.0	123.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0		0.0	0.0
49.0	0.0	65.0	0.0	123.0	0.0	27.0	0.0	0.0
65.0	0.0	73.0	-4.0	123.0	0.0	27.0	0.0	0.0
73.0	-4.0	87.0	-11, 0	-127.0	0.0	27.0	0.0	0.0
87.0	-11.0	95.0	-15.0	-120.0	0.0	33.0	0.0	0.0
95.0	-15.0	125.0	-30.0	-110.0	0.0	28.0	0.0	0.0
125.0	-30.0	130.0	-35.0	-95.0	0.0	24.0	0.0	0.0
30.0	-11.0	37.0	-14.5	123.0	33.0	27.0	0.0	0.0
37.0	-14.5	38.0	-15.0	-127.0	33.0	27.0	0.0	0.0
38.0	-15.0	68.0	-30.0	-127.0	28.0	27.0	0.0	0.0
68.0	-30.0	78.0	-35.0	-127.0	24.0	27.0	0.0	0.0
78.0	-35.0	84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
84.0	-38.0	9399.0	-38.0	-128.0	27.0	25.0	0.0	0.0
78.0	-35.0	130.0	-35.0	-127.0	24.0	27.0	0.0	0.0
130.0	-35.0	9399.0	-35.0	-127.0	0.0	27.0	0.0	0.0
68.0		125.0	-30.0	-95.0	28.0	24.0	0.0	0.0
125.0	-30.0	9399.0	-30.0	-70.0	0.0	0.0	0.0	0.0
38.0	-15.0	95.0	-15.0	-110.0	33.0	28.0	0.0	0.0
30.0	-11.0	57.0	-11.0	117.0	27.0	33.0	0.0	0.0
57.0	-11.0	87.0	-11.0	-120.0	27.0	33.0	0.0	0.0
73.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
	-35.0	78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
-79.0	-34.0	37.0	-14.5	-127.0	27.0	27.0	0.0	0.0
37.0	-14.5	57.0	-11.0	-120.0	33.0	33.0	0.0	0.0
57.0	-11.0	73.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT = 49.0 YT = -5.0 XB = 49.0 YB = -45.0

GRIDX= 70.0 GRIDY= 20.0 XMAX= 170.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.29 EFS= 1.00 H(X) = 110.00 G(Y) = 40.00 R= 75.81 THE MIN. EFS= 1.00 FS= 1.29 H(X) = 120.00 G(Y) = 60.00 R= 96.27

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

×i	Y 1	X2	Y2	W.	F2	F1	ca	C1
9399.0	-49.0	112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
112.0	-49.0	-9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
9399.0	-46.5	110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
112.0	-49.0	110.0	-46.5	-128.0	0.0	25.0	0.0	0.0
110.0	-46.5	105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
105.5	-41.5	100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
100.0	-39.5	86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
86.0	-37.0	79.0	-34.0	-127.0	35.0	27.0	0.0	0.0
79.0	-34.0	67.0	-29.0	123.0	35.0	27.0	0.0	0.0
100.0	-39.5	85.0	-30.0	135.0	0.0	35.0	0.0	0.0
85.0	-30.0	67.0	-29.0	135.0	0.0	35.0	0.0	0.0
67.0	-29.0	-49.0	0.0	123.0	0.0	27.0	0.0	0.0
-49.0	0.0	-65.0	0.0	123.0	0.0	27.0	0.0	0.0
-65.0	0.0	-73.0	-4.0	123.0	0.0.	27.0	0.0	0.0
-73.0.	-4.0	-87.0	-11.0	-127.0	0.0	27.0	0.0	0.0
-87.0	-11.0	-95.0	-15.0	-120.0	0.0	33.0	0.0	0.01
-95.0	-15.0	-125.0	-30.0	-110.0	0.0	28.0	0.0	0.0
-125.0	-30.0	-130.0	-35.0	-95.0	0.0	24.0	0.0	0.0
-30.0	-11.0	-37.0	-14.5	123.0	33.0	27.0	0.0	0.0
-37.0	-14.5	-38.0	-15.0	-127.0	33.0	27.0	0.0	0.0
-38.0	-15.0	-68.0	-30.0	-127.0	28.0	27.0	0.0	0.0
-68.0	-30.0	-78.0	-35.0	-127.0	24.0	27.0	0.0	0.0
-78.0	-35,0	-84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
-84.0	-38.0	-9399.0	-38.0	-128.0	27.0	25.0	0.0	0.0
-78.0	-35.0	-130.0	-35.0	-127.0	24.0	27.0	0.0	0.0
-130.0	-35.0	-9399.0	-35.0	-127.0	0.0	27.0	0.0	0.0
-68.0	-30.0	-125.0	-30.0	-95.0	28.0	24.0	0.0	0.0
-125.0	-30.0	-93 99. 0	-30.0	-70.0	0.0	0.0	0.0	0.0
-38.0	-15.0	- 9 5.0	-15.0	-110.0	33.0	28.0	0.0	0.0
-30.0	-11.0	-57.0	-11.0	117.0	27.0	33.0	0.0	0.0
-57.0	-11.0	-87.0	-11.0	-120.0	27.0	33.0	0.0	0.0
-73.0	-4.0	-9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
86.0	-37.0	-5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
-5 0	-35.0	-78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
79.0	-34.0	-37.0	-14.5	-127.0	27.0	27.0	0.0	0.0
-37.0	-14.5	-57.0	-11.0	-120.0	33.0	33.0	0.0	0.0
-57.0	-11.0	-73.0	-4.0	-127.0	27.0	27.0	0.0	0.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.47 EFS= 1.18 H(X)= 50.00 G(Y)= 90.00 R= 137.22 THE MIN. EFS= 1.18 FS= 1.47 H(X)= 50.00 G(Y)= 90.00 R= 137 SBU 104.962 UNTS.

GET,TAPE5=JMH36 READY. kSd

84/08/07. 08.34.56. PROGRAM SLOPE2

110 JSF ASH POND "J", R-APP,@STA.41+75,4:1 SLOPE,R LOW POOL (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	, Y1	XS	Y2	W	F2	F1	cs	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49 * 0	9399.0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
-9399.0	-48.0	-111.0	-48.0	-62.4	0.0	0.0	0.0	0.0
-112.0	-49.0	-111.0	-48.0	-128.0	0.0	11.0	0.0	600.0
-1111.0	-48.0	-105.5	-41.5	-128.0	0.0	11.0	0.0	600.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	11.0	0.0	600.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	11.0	0.0	600.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	16.0	0.0	200.0
-79.0	-34.0	-74.0	-32.0	123.0	35.0	16.0	0.0	200.0
-74.0	-32.0	-67.0	-29.0	123.0	35.0	16.0	0.0	200.0
-100.0	-39.5	-88.0	-32.0	135.0	0.0	35.0	0.0	0.0
-88.0	-32.0	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	16.0	0.0	200.0
49.0	0.0	65.0	0.0	123.0	0.0	16.0	0.0	200.0
65.0	0.0	73.0	-4.0	123.0	0.0	16.0	0.0	200.0
73.0	-4.0	87.0	-11.0	-127.0	0.0	16.0	0.0	200.0
87.0	-11.0	95.0	-15.0	-120.0	0.0	20.0	0.0	1200.0
95.0	-15.0	125.0	-30.0	-110.0	0.0	15.0	0.0	600.0
125.0	-30.0	130.0	-35.0	-95.0	0.0	15.0	0.0	100.0
30.0	-11.0	37.0	-14.5	123.0	20.0	16.0	1200.0	200.0
37.0	-14.5	38.0	-15.0	-127.0	20.0	16.0	1200.0	200.0
38.0	-15.0	68.0	-30.0	-127.0	15.0	16.0	600.0	200.0
68.0	-30.0	78.0	-35.0	-127.0	15.0	16.0	100.0	200.0
78.0	-35.0	84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
84.0	-38.0	9399.0	-38.0	-128.0	16.0	11.0	200.0	600.0
78.0	-35.0	130.0	-35.0	-127.0	15.0	16.0	100.0	200.0
130.0	-35.0	9399.0	-35.0	-127.0	0.0	16.0	0.0	200.0
68.0	-30.0	125.0	-30.0	-95.0		15.0	600.0	100.0
125.0	-30.0	9399.0	-30.0	-70.0	0.0	0.0	0.0	0.0
38.0	-15.0	95.0	-15.0	-110.0	20.0	15.0	1200.0	600.0
30.0	-11.0	57.0	-11.0	117.0	16.0	20.0	200.0	1200.0
57.0	-11.0	87.0	-11.0	-120.0	16.0	20.0	200.0	1200.0
73.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
5.0	-35.0	78.0	-35.0	-128.0	36 *aa* B *a*	11.0	200.0	600.0
-79.0	-34.0	37.0	-14.5	-127.0	16.0	16.0	200.0	200.0
37.0	-14.5	57.0	-11.0	-120.0	20.0	20.0	1200.0	1200.0
57.0	-11.0	73.0	-4.0	-127.0	16.0	16.0	200.0	200.0

XT= 49.0 YT= -5.0 XB= 49.0 YB= -45.0

GRIDX= 70.0 GRIDY= 20.0 XMAX= 170.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.87 EFS= 1.47 H(X)= 100.00 G(Y)= 20.00 R= 56.81 THE MIN. EFS= 1.47 FS= 1.87 H(X)= 100.00 G(Y)= 20.00 R= 56.81

THESE ARE THE INPUT DATA LINES

X1	Y1	X2	Y2	W	F2	F1	C2	C1
				1000	0.0	100.0	0.0	9999.0
9399.0	-49.0	112.0			0.0 11.0	100.0	•	9999.0
112.0		-93 99. 0				0.0	0.0	
9399.0	-48.0	111.0		-62.4	0.0 0.0	11.0	0.0	600.0
112.0	-49.0	111.0		-128.0		11.0	0.0	600.0
111.0	-48.0	105.5	-41.5	-128.0	0.0 0.0	11.0	0.0	600.0
105.5	-41.5	100.0	-39.5			11.0	0.0	600.0
100.0	-39.5	86.0	-37.0		35.0 35.0		0.0	200.0
86.0	-37.0	7 9 .0	-34.0	-127.0		16.0	0.0	200.0
79.0	-34.0	74.0	-32.0	123.0	35.0	16.0	0.0	
74.0	-32.0	67.0	-29.0					0.0
100.0	-39.5	88.0	-32.0		0.0	35.0 35.0		0.0
88.0	-32.0	85.0	-30.0		0.0			0.0
85.0	-30.0	67.0	-29.0		0.0	35.0	0.0	200.0
67.0	-29.0	-49.0	0.0			16.0		200.0
-49.0	0.0	-65.0	0.0	123.0	0.0	16.0		
-65.0	0.0			123.0	0.0	16.0		200.0
-73.0	-4.0	-87.0	-11.0			16.0	0.0	1200.0
-87.0	-11.0	-95.0			0.0	20.0	0.0	600.0
-95.0	-15.0	-125.0	-30.0			15.0	0.0	100.0
-125.0	-30.0	· ·	-35.0		0.0	15.0	1200.0	200.0
-30.0	-11.0		-14.5		20.0	16.0	1200.0	200.0
-37.0	-14.5		-15.0		20.0			200.0
-38.0	-15.0		-30.0		15.0		600.0	200.0
-68.0	-30.0		-35.0					600.0
-78.0	-35.0	•••	-38.0		16.0	11.0	200.0	600.0
-84.0	-39.0	- 9 399.0	-38.0		16.0	11.0	200.0	200.0
-78.0	-35.0		-35.0		15.0		100.0	200.0
-130.0	-35.0	-9399.0	-35.0		0.0	16.0	0.0	100.0
-68.0	-30.0		-30.0		15.0	15.0	600.0 0.0	0.0
-125.0	-30.0	-939 9. 0	-30.0		0.0	0.0	1200.0	600.0
-38.0	-15.0			-110.0	20.0	15.0		1200.0
-30.0	-11.0	-57.0	-11.0		16.0		200.0	1200.0
	-11.0		-11.0				200.0	0.0
-73.0	-4.0	-9399. 0	-4.0		0.0		0.0	600.0
86.0	-37.0	-5.0		-128.0		11.0		600.0
-5.0	-35.0	-78.0		-128.0	16.0	11.0	200.0	
79.0	-34.0			-127.0	16.0	16.0	200.0	200.0
-37.0				-120.0	20.0	20.0		1200.0
	-11.0		-4.0	-127.0	16.0	16.0	200.0	200.0
						س سور		
$\forall T = -49$	ű ·	YT = -5.0) Х	B = -49.0	YB=	-45.0		

XT= -49.0 YT= -5.0 XB= -49.0 YB= -45.0

GRIDX= 10.0 GRIDY= 10.0 XMAX= 140.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.73 EFS= 1.40 H(X)= 20.00 G(Y)= 60.00 R= 94.80 THE MIN. EFS= 1.39 FS= 1.75 H(X)= 20.00 G(Y)= 50.00 R= 98.25 SBU 109.433 UNTS.

OLD, SLOPES
READY.
FIN
READY.
GET, TAPES=JMH37
READY.
RUN

84/08/07. 10.04.51. PROGRAM SLOPE2

110 JSF ASH POND "J", R-APP,@STA.41+75,4:1 SLOPE,R HIGH POOL (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y1	XS	Y2	l _e i	F2	F1	cs	C1
-9399.0	-49.0	-112.0	-49. n	-1000.0	0.0	100.0		0000 0
-112.0	-49.0	9399.0		-1000.0	11.0	100.0	0.0 600.0	9999.0
-9399.0	-32.0	-88.0	-32.0	-62.4	0.0	0.0	0.0	9999.0
-112.0	-49.0	-111.0	-48.0	-128.0	0.0	11.0	0.0	0.0 600.0
-111.0	-48.0	-105.5	-41.5	-128.0		11.0	0.0	600.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	11.0	0.0	600.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	11.0	0.0	600.0
-86.0	-37.0	-79.0	-34.0	-127.0	35.0	16.0	0.0	200.0
-79.0	-34.0	-74.0	-32.0	123.0	35.0	16.0	0.0	200.0
-74.0	-32.0	-67.0	-29.0	123.0	35.0	16.0	0.0	200.0
-100.0	-39.5	-88.0	-32.0	-135.0	0.0	35.0	0.0	0.0
-88.0	-32.0	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-67.0	-29.0	49.0	0.0	123.0	0.0	16.0	0.0	200.0
49.0	0.0	65.0	0.0	123.0	0.0	16.0	0.0	200.0
65.0	0.0	73.0		123.0	0.0	16.0	0.0	200.0
73.0	-4.0	87.0	-11.0	-127.0	0.0	16.0	0.0	200.0
87.0	-11.0	95.0	-15.0	-120.0	0.0	20.0	0.0	1200.0
95.0	-15.0	125.0	-30.0	-110.0	0.0	15.0	0.0	600.0
125.0	-30.0	130.0	-35.0	-95.0	0.0	15.0	0.0	100.0
30.0	-11.0	37.0	-14.5	123.0	20.0	16.0	1200.0	200.0
37.0	-14.5	38.0	-15.0	-127.0	20.0	16.0	1200.0	200.0
38.0	-15.0	68.0	-30.0	-127.0	15.0	16.0	600.0	200.0
68.0	-30.0	78.0	-35.0	-127.0	15.0	16.0	100.0	200.0
78.0	-35.0	84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
84.0	-38.0	93 99 .0	-38.0	-128.0	16.0	11.0	200.0	600.0
78.0	-35.0	130.0	-35.0	-127.0	15.0	16.0	100.0	200.0
130.0	-35.0	9399.0	-35.0	-127.0	0.0	16.0	0.0	200.0
68.0	-30.0		-30.0	-95.0	15.0	15.0	600.0	100.0
125.0	-30.0	9399.0	-30.0	-70.0	0.0	0.0	0.0	0.0
38.0	-15.0	95.0	-15.0	-110.0	20.0	15.0	1200.0	600.0
30.0	-11.0	57.0	-11.0	117.0	16.0	20.0	200.0	1200.0
57.0	-11.0	87.0	-11.0	-120.0	16.0	20.0	200.0	1200.0
73.0	-4.0	9399.0	-4.0	-62.4		0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
5.0	-35.0	78.0	-35.0	-128.0	16.0	11.0	200.0	600.0
-79.0	-34.0	-6 7.0	-32.0	-127.0	16.0	16.0	200.0	200.0
-67.0	-32.0	37.0	-14.5	-127.0	16.0	16.0	200.0	200.0
37.0	-14.5	57.0	-11.0	-120.0	20.0	20.0	1200.0	1200.0
57.0	-11.0	73.0	-4.0	-127.0	16.0	16.0	200.0	200.0
-88.0	-32.0	-74.0	-32.0	-135.0	35.0	35.0	0.0	0.0

XT= 49.0 YT= -5.0 XB= 49.0 YB= -45.0

GRIDX= 70.0 GRIDY= 20.0 XMAX= 170.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.87 EFS= 1.47 H(X)= 100.00 G(Y)= 20.00 R= 56.81 THE MIN. EFS= 1.47 FS= 1.87 H(X)= 100.00 G(Y)= 20.00 R= 56.81

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

6.7.4		1.17			,			
×1	Υ1	X2	. Y2	W	F2	F1	C2	C1
9399.0	-49.0	112.0	-49, 0	-1000.0	0.0	100.0	0.0	9999.0
112.0	-49.0	-93 99 .0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
9399.0	-32.0		-32.0	-62.4	0.0	0.0	0.0	0.0
112.0	-49.0		-48.0	-128.0	0.0	11.0	0.0	600.0
111.0	-48.0		-41.5	-128.0	0.0	11.0	0.0	600.0
105.5	-41.5		-39.5	-128.0	0.0	11.0	0.0	600.0
100.0	-39.5		-37.0	-128.0	35.0	11.0	0.0	600.0
86.0	-37.0	79.0	-34.0	-127.0	35.0	16.0	0.0	200.0
79.0	-34.0	74.0	-32.0	123.0		16.0	0.0	200.0
74.0	-32.0	67.0	-29.0	123.0	35.0	16.0	0.0	200.0
100.0	-39.5	88.0	-32.0	-135.0	0.0	35.0	0.0	0.0
88.0	-32.0	85.0	-30.0	135.0	0.0	35.0	0.0	0.0
85.0	-30.0	67.0	-29.0	135.0	0.0	35.0	0.0	0.0
67.0	-29.0	-49.0	0.0	123.0	0.0	16.0	0.0	200.0
-49.0	0.0	-65.0	.0.0	123.0	0.0	16.0	0.0	200.0
-65.0	0.0	-73.0	-4.0	123.0	0.0	16.0	0.0	200.0
-73.0	-4.0	-87.0	-11.0	-127.0	0.0	16.0	0.0	200.0
-87.0	-11.0	-95.0	-15.0	-120.0	0.0	20.0	0.0	1200.0
-95.0	-15.0	-125.0	-30.0	-110.0		15.0	0.0	600.0
-125.0	-30.0	-130.0	-35.0	-95.0	0.0	15.0	0.0	100.0
-30.0	-11.0	-37.0	-14.5	123.0	20.0	16.0	1200.0	200.0
-37.0	-14.5	-38.0	-15.0	-127.0	20.0	16.0	1200.0	200.0
-38.0	-15.0	-68.0	-30.0	-127.0	15.0	16.0	600.0	200.0
-68.0	-30.0	-78.0	-35.0	-127.0	15.0	16.0	100.0	200.0
-78.0	-35.0	-84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
-84.0	-38.0	-9399.0	-38.0	-128.0	16.0	11.0	200.0	600.0
-78.0	-35.0	-130.0	-35.0	-127.0	15.0	16.0	100.0	200.0
-130.0	-35.0	-9399.0	-35.0	-127.0	0.0	16.0	0.0	200.0
-68.0	-30.0		-30.0	-95.0	15.0	15.0	600.0	100.0
-125.0	-30.0	-9399.0	-30.0	-70.0	0.0	0.0	0.0	0.0
-38.0	-15.0	-95.0	-15.0	-110.0	20.0	15.0	1200.0	600.0
-30.0	-11.0	-57.0	-11.0	117.0	16.0	20.0	200.0	1200.0
-57.0	-11.0	-87.0	-11.0	-120.0	16.0	20.0	200.0	1200.0
-73.0	-4.0	-9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
86.0	-37.0	-5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
-5.0	-35.0	-78.0	-35.0	-128.0	16.0	11.0	200.0	600.0
79.0	-34.0	67.0	-32.0	-127.0	16.0	16.0	200.0	200.0
67.0	-32.0	-37.0	-14.5	-127.0	16.0	16.0	200.0	200.0
-37.0	-14.5	-57.0	-11.0	-120.0	20.0	20.0	1200.0	1200.0
-57.0	-11.0	-73.0	-4.0	-127.0	16.0	16.0	200.0	200.0
88.0	-32.0	74.0	-32.0	-135.0	35.0	35.0	0.0	0.0

TEST POINTS

THE MIN. FS= 1.73 EFS= 1.40 H(X)= 20.00 G(Y)= 60.00 R= 94.80 THE MIN. EFS= 1.39 FS= 1.75 H(X)= 20.00 G(Y)= 50.00 R= 98.25 SBU 112.286 UNTS.

OLD.SLOPE2
READY.
FIN
READY.
GET.TAPE5=JMH34
READY.
RUN

84/08/03.11.13.31. PROGRAM SLOPE2

110 JSF ASH POND "J", R-EFF,@STA.41+75,3:1 SLOPE (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

X1	Y1	X2	45	ld.	F2	F1	C2	C 1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0 9	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0 9	9999.0
-939 9. 0	-46.5	-110.0	-46.5	-62.4	0.0	0.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	-128.0	0.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	0.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-67.0		-127.0	35.0	27.0	0.0	0.0
-100.0	-39.5		-30.0		0, 0		0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0		0.0
-67.0	-29.0	20.0	0.0	123.0	0.0	27.0		0.0
20.0	0.0 0.0	36.U	u, u, u	123.0	0.0	27.0	0.0	0.0
36.0			-4.0	123.0	0.0	27.0	0.0	0.0
44.0	-4.0	56.0	-10.0		0.0	27.0	0.0	0.0
56.0	-10.0	66.0	-15.0		0.0	31.0	0.0	0.0
66.0	-15.0	96.0	-30.0	-105.0	0.0	24.0	[0.0]	0.0
96.0	-30.0	98.0	-35.0	-95.0	0.0	20.0	0.0	0.0
28.0	-10.0	56.0	-10.0	-115.0	27.0	31.0	0.0	0.0
28.0	-10.0	38.0	-15.0	-127.0	31.0	27.0	0.0	0.0
38.0	-15.0	68.0	-30.0	-127.0	24.0	27.0	0.0	0.0
68.0	-30.0	78.0	-35.0	-127.0	20.0	27.0	0.0	0.0
78.0	-35.0	84.0	-38.0	-128.0	27.0		0.0	0.0
84.0	-38.0	9399.0	-38.0	-128.0	27.0	25.0		0.0
78.0	-35.0	98.0	-35.0	-127.0	20.0	27.0	0.0	0.0
98.0	-35.0	9399.0	-35.0		0.0	27.0 20.0	0.0	0.0
68.0	-30.0	96.0		-95.0		1 N N N	~ * ~	
96.0	-30.0	9399.0				0.0	0.0	0.0
38.0		66.0	-15.0	-105.0	31.0	24.0	0.0	0.0
44.0				-62.4	0.0	0.0	W # W	0.0
-8 6. 0	-37.0	5.0	-35.0			25.0	0.0	0.0
5.0	-35.0	78.0	-35.0	-128.0		25.0	0.0	0.0
-67.0	-29.0	28.0	-10.0	-127.0	27.0	27.0		0.0
28.0	-10.0	44.0	-4.0	-127.0	27.0	27.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-127.0 -127.0 -128.0	0.0	25.0	0.0	0.0
XT= 30.	0 Y	T= -5.0	ΧE	e 30.0	YB=	-45.0		
GRIDX=	40.0	GRIDY=	20.0	XMAX=	140.0	YMAX=	100.0	
INCX= 10	INC	Y= 10	INCR=	10				

TEST POINTS

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

THE MIN. FS= 1.00 EFS= .79 H(X)= 90.00 G(Y)= 50.00 R= 81.40 THE MIN. EFS= .77 FS= 1.01 H(X)= 100.00 G(Y)= 60.00 R= 95.53

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

×ı	Y1	X2	A5.	l _t l	F2	F1	C2	C1
		***	_40.0.	-1000.0	0.0	100.0	0.0	9999.0
9399.0	-49.0	112.0		-1000.0	25.0	100.0	0.0	9 999 .0
112.0		-9 3 99 .0		-62.4	0.0	0.0	0.0	0.0
93 99 .0	-46.5	110.0	-41.5	-128.0	0.0	25.0	0.0	0.0
110.0	-46.5	105.5	-39 . 5		0.0	25.0	0.0	0.0
105.5	-41.5	100.0	-37.0	-128.0	35.0	25.0	0.0	0.0
100.0		86.0	-37.0 -29.0	-127.0	35.0	27.0	0.0	0.0
86.0	-37.0	67.0		135.0	0.0	35.0	0.0	0.0
100.0	-39 . 5	85.0	-30.0	135.0	0.0	35.0	0.0	0.0
85.0	-30.0	67.0	-29.0	123.0	0.0	27.0	0.0	0.0
67.0	-29.0	-20.0	0.0	123.0	0.0	27.0	0.0	0.0
-20.0	0.0	-36.0	0.0	123.0	0.0	27.0	0.0	0.0
-36.0	0.0	-44.0	-4.0	-127.0	0.0		0.0	0.0
-44.0	-4.0	-56.0	-10.0	-127.0 -115.0	0.0	31.0		0.0
-56.0	-10.0	-66.0	-15.0	-115.0	0.0	24.0	0.0	0.0
-66.0	-15.0	- 96 .0	-30.0	-105.0 -95.0	0.0	20.0	0.0	0.0
-96.0	-30.0	-98.0	-35.0	-75.0 -115.0	27.0	31.0	0.0	0.0
-28.0	-10.0	-56.0	-10.0	-113.0 -127.0	31.0	27.0	0.0	0.0
-28.0	-10.0	-38.0	-15.0	-127.0	24.0	27.0		0.0°
-38.0	-15.0	-68.0	-30.0		20.0	27.0	0.0	0.0
-68.0	-30.0	-78.0	-35.0	-127.0	27.0	25.0	0.0	0.0
-78.0	-35.0	-84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
-84.0	-38.0	-9399.0	-38.0	-128.0	20.0	27.0	0.0	0.0
-78.0	-35.0	- 9 8.0	-35.0	-127.0 -127.0	0.0	27.0	0.0	0.0
-98.0	-35.0		-35.0	-127.0 -95.0	24.0	20.0	0.0	0.0
-68.0	-30.0	- 96 .0	-30.0		0.0	0.0	0.0	0.0
-96.0	-30.0	- 9 3 99 .0	-30.0	-70.0	31.0	24.0	0.0	0.0
-38.0	-15.0	-66.0	-15.0	-105.0	0.0	0.0	0.0	0.0
-44.0		-93 99 .0	-4.0	-62.4	27.0	25.0	0.0	0.0
86.0	-37.0	-5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
-5.0	-35.0		-35.0	-128.0	27.0	27.0	0.0	0.0
67.0	-29.0		-10.0	-127.0	27.0 27.0	27.0	0.0	0.0
-28.0	-10.0		-4.0		27.0 0.0	25.0	0.0	0.0
112.0	-49.0	110.0	-46.5	-128.0	ម. ម.	c.J. 0	0.0	

XT = -20.0 YT = -5.0 XB = -20.0 YB = -45.0 GRIDX = 10.0 GRIDY = 10.0 XMAX = 140.0 YMAX = 100.0 INCX = 10 INCY = 10 INCR = 10 THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.03 EFS= .86 H(X)= 80.00 G(Y)= 90.00 R= 137.94 THE MIN. EFS= .86 FS= 1.03 H(X)= 80.00 G(Y)= 90.00 R= 137.94 SBU 121.738 UNTS.

110 JSF ASH POND "J",R-BAR,@STA.41+75,LOW W.T. WITH DRY STACKING,HIGH PO (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y 1	XS	Y2	l,d	F2	F1	C2	C1
-9399.0	-49.0	-112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-32.0	-88.0	-32.0	-62.4	0.0	0.0	0.0	0.0
-88.0	-32.0	-74.0	-32.0	-135.0	35.0	35.0	0.0	0.0
-112.0	-49.0	-105.5	-41.5	-128.0	35.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	-128.0	35.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	-128.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-74.0	-32.0	-127.0	35.0	27.0	0.0	0.0
-100.0	-39.5	-88.0	-32.0	-135.0	0.0	35.0	0.0	0.0
-88.0	-32.0	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
-74.0	-32.0	-67.0	-29.0	123.0	0.0	27.0	0.0	0.0
-67.0	-29.0	-8.0	0.0	123.0	0.0	27.0	0.0	0.0
-8.0	0.0	8.0	0.0	123.0	0.0	27.0	0.0	0.0
8.0	0.0	72.0	-32.0	123.0	0.0	27.0	0.0	0.0
72.0	-32.0	78.0	-35.0	-127.0	0.0	27.0	0.0	0.0
78.0	-35.0	84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
84.0	-38.0	939 9 .0	-38.0	-128.0	27.0	25.0	0.0	0.0
78.0	-35.0	9399.0	-35.0	-127.0	0.0	27.0	0.0	0.0
72.0	-32.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
-74.0	-32.0	72.0	-32.0	-127.0	27.0	27.0	0.0	0.0

XT = 8.0 YT = -5.0 XB = -40.0 YB = -35.0

GRIDX= 20.0 GRIDY= 20.0 XMAX= 100.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.03 EFS= .89 H(X)= 70.00 G(Y)= 30.00 R= 71.21 THE MIN. EFS= .89 FS= 1.03 H(X)= 70.00 G(Y)= 30.00 R= 71.21

FOR SIDE TWO

111								
X1	Y1.	XS	Y2	hJ	F2	F1	C2	Ci
9399.0	-49.0	112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
112.0	-49.0	-9 399.0		-1000.0	25.0	100.0	0.0	
9399.0	-32.0	88.0	-32.0	-62.4	0.0	0.0	0.0	9999.0
88.0	-32.0	74.0	-32.0	-135.0	35.0	35.0		0.0
112.0	-49.0	105.5	-41.5	-128.0	35.0	25.0	0.0	0.0
105.5	-41.5	100.0	-39.5	-128.0	35.0	25.0	Û.Û	0.0
100.0	-39.5	86.0	-37.0	-128.0	35.0		0.0	0.0
86.0	-37.0	74.0	-32.0	-127.0		25.0	0.0	0.0
100.0	-39.5	88.0	-32.0	-135.0	35.0	27.0	0.0	0.0
88.0	-32.0	85.0	-30.0	135.0	0.0	35.0	0.0	0.0
85.0	-30.0	67.0	-29.0		0.0	35.0	0.0	0.0
74.0	-32.0	67.0	-29.0	135.0	0.0	35.0	0.0	0.0
67.0	-29.0	9.0	0.0	123.0	0.0	27.0	0.0	0.0
8.0	0.0	-8.0		123.0	0.0	27.0	0.0	0.0
-8.0	0.0	-72.0	0.0 -33 o	123.0	0.0	27.0	0.0	0.0
-72.0	-32.0	-78.0	-32.0	123.0	0.0	27.0	0.0	0.0
-78.0	-35.0	-84.0	-35.0	-127.0	0.0	27.0	0.0	0.0
-84.0		-93 99 .0	-38.0	-128.0	27.0	25.0	0.0	0.0
-78.0			-38.0	-128.0	27.0	25.0	0.0	0.0
-72.0		-93 99 .0	-35.0	-127.0	0.0	27.0	0.0	0.0
86.0		-93 99 .0	-4.0	-62.4	0.0	0.0	0.0	0.0
-5.0		-5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
	-35.0	-78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
74.0	-32.0	-72.0	-32.0	-127.0	27.0	27.0	0.0	0.0
								0 8 0

XT= 8.0 YT= -5.0 XB= -70.0 YB= -45.0

GRIDX= 25.0 GRIDY= 5.0 XMAX= 120.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.08 EFS= .92 H(X)= 105.00 G(Y)= 85.00 R= 132.33 THE MIN. EFS= .92 FS= 1.08 H(X)= 105.00 G(Y)= 85.00 R= 132.33 SBU 61.178 UNTS.

RUN COMPLETE.

110 JSF ASH POND "J",R-APP,@STA.41+75,LOW W.T. WITH DRY STACKING,HIGH PO (ERQF= .05 DEPTH OF ROCK= .49.0 FT)

	X1	Y1	X2	Y2	W	F2	F1	C2	C1
	399.0	-49.0	-112.0	-49.0	-1000.0	.0.0	100.0	0.0	9999.0
	112.0	-49.0	9399.0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
-9	399.0	-32.0	-88.0	-32.0	-62.4	0.0	0.0	0.0	0.0
	-88.0	-32.0	-74.0	-32.0	-135.0	35.0	35.0	0.0	0.0
_	112.0	-49.0	-105.5	-41.5	-128.0	35.0	11.0	0.0	600.0
	105.5	-41.5	-100.0	-39.5	-128.0	35.0	11.0	0.0	600.0
	100.0	-39.5	-86.0	-37.0	-128.0	35.0	11.0	0.0	600.0
	-86.0	-37.0	-74.0	-32.0	-127.0	35.0	16.0	0.0	200.0
****	100.0	-39.5	-88.0	-32.0	-135.0	.0.0	35.0	0.0	0.0
	-88.0	-32.0	-85.0	-30.0	135.0	0.0	35.0	0.0	0.0
	-85.0	-30.0	-67.0	-29.0	135.0	0.0	35.0	0.0	0.0
	-74.0	-32.0	-67.0	-29.0	123.0	0.0	16.0	0.0	200.0
	-67.0	-29.0	-8.0	0.0	123.0	0.0	16.0	0.0	200.0
	-8.0	0.0	8.0	0.0	123.0	0.0	16.0	0.0	200.0
	8.0	0.0	72.0	-32.0	123.0	0.0	16.0	0.0	200.0
	72.0	-32.0	78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
	78.0	-35.0	84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
	84.0	-38.0	939 9 .0	-38.0	-128.0	16.0	11.0	200.0	600.0
	78.0	-35.0	93 99 .0	-35.0	-127.0	0.0	16.0	0.0	200.0
	72.0	-32.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
	-86.0	-37.0	5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
	5.0	-35.0	78.0	-35.0	-128.0	16.0	11.0	200.0	600.0
	-74.0	-32.0	72.0	-32.0	-127.0	16.0	16.0	200.0	200.0
						-			

XT= 8.0 YT= -5.0 XB= -40.0 YB= -35.0 GRIDX= 20.0 GRIDY= 20.0 XMAX= 100.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.12 EFS= .98 H(X)= 50.00 G(Y)= 30.00 R= 64.68 THE MIN. EFS= .98 FS= 1.12 H(X)= 50.00 G(Y)= 30.00 R= 64.68

FOR SIDE TWO

W.A	Q a	1, 3 200	1.100	`1.1	. 1000 400			
X1	Y1	X2	Y2	W	F2	F1	C2	·C1
9399.0	-49.0	112.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
112.0	-49.0	-9399.0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
9399.0	-32.0	88.0	-32.0	-62.4	0.0	0.0	0.0	0.0
88.0	-32.0	74.0	-32.0	-135.0	35.0	35.0	0.0	0.0
112.0	-49.0	105.5	-41.5	-128.0	35.0	11.0	0.0	600.0
105.5	-41.5	100.0	-39.5	-128.0	35.0	11.0	0.0	600.0
100.0	-39.5	86.0	-37.0	-128.0	35.0	11.0	0.0	600.0
86.0	-37.0	74.0	-32.0	-127.0	35.0	16.0	0.0	200.0
100.0	-39.5	88.0	-32.0	-135.0	0.0	35.0	0.0	0.0
88.0	-32.0	85.0	-30.0	135.0	0.0	35.0	0.0	0.0
85.0	-30.0	67.0	-29.0	135.0	0.0	35.0	0.0	0.0
74.0	-32.0	67.0	-29.0	123.0	0.0	16.0	0.0	200.0
67.0	-29.0	8.0	0.0	123.0	0.0	16.0	0.0	200.0
8.0	0.0	-8.0	0.0	123.0	0.0	16.0	0.0	200.0
-8.0	0.0	-72.0	-32.0	123.0	0.0	16.0	0.0	200.0
-72.0	-32.0	-78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
-78.0	-35.0	-84.0	-38.0	-128.0	16.0	11.0		600.0
-84.0		- 9 399.0	-38.0	-128.0	16.0	11.0	200.0	600.0
-78.0		- 9 399.0	-35.0	-127.0	0.0	16.0	0.0	200.0
-72.0		-9 399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
86.0		-5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
-5.0	-35.0	-78.0	-35.0	-128.0	16.0	11.0	200.0	600.0
74.0	-32.0	-72.0	-32.0	-127.0	16.0	16.0	200.0	200.0
								

XT= 8.0 YT= -5.0 XB= -70.0 YB= -45.0 GRIDX= 25.0 GRIDY= 5.0 XMAX= 120.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.16 EFS= 1.01 H(X)= 55.00 G(Y)= 15.00 R= 51.09 THE MIN. EFS= 1.01 FS= 1.16 H(X)= 55.00 G(Y)= 15.00 R= 51.09 SBU 60.848 UNTS.

PUN COMPLETE.

SBU 120.800 UNTS. RUM:COMPLETE: DLI:JMK90 READY. XED XEDIT 9.1.00 77 B DOUSON CREEK 430 0.0 ?? M-2 410 -50,-26,-50,-70 77 M NORMAL I WAR 410 -50,-26,-50,-70 410 50,-26,50,-70 Some Contraction The 77 Q.,RL JMH30 REPLACED
JMH30 IS A LOCAL FILE SBU 0.301 UNTS. READY. OLD, SLOPE2 READY. FTN READY. GET+TAPE5=JMH30 READY. RUN 84/07/31. 13.47.06. PROGRAM SLOPE2 110 JSF ASH POND "J", R TEST @STA.41+75.RIPRAP1080BERM10/@1065 (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Yt	xa	Y2	l _e l		F2	Fi	CS	C1
-93 99 .0	-49. 0	-132.0	-49.0	-1000.0		0.0	100.0	0.0	9999.0
-132.0	-49.0	-112.0	-49.0	-1000.0		35.0	100.0	0.0	9999.0
-112.0	-49.0	93 99. 0	-49. 0	-1000.0	- 16	11.0	100.0	600.0	9999.0
-9399.0	-46.5	-129.5	-46.5	-62.4		0.0°	0.0	0.0	0.0
-128.5	-46.5	-110.0	-46.5	-135.0	1	35.0	35.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0		35.0	11.0	0.0	600.0
-110.0	-46.5	-105.5	-41.5	125.0		35.0	11.0	0.0	600.0
-105.5	-41.5	-100.0	-39.5	125.0	1	35.0	11.0	0.0	600.0
-100.0	-39.5	-8 6. 0	-37.0	125.0		35.0	11.0	0.0	600.0
~86.0	-37.0	-60.0	-26.0	123.0	3	35.0	16.0	0.0	200.0
-132.0	-49.0	-128.5	-46.5	-135.0		θ . θ	35.0	0.0°	0.0
-128.5	-46.5	-117.0	-39.0	135.0		0.0	35.0	0.0	0.0
-117.0	-39.0	-107.0	-39.0	135.0	. 1	0.0	35.0	0.0	0.0
-107.0	-39.N	-86.0	-25.0	135.0		0.0	35.0	0.0	0.0
-86.0	-25.0	-58.0	-25.0	135.0		0.0	35.0	0.0	0.0
-60.0	-26.0	-59.0	-25.0	123.0		35.0	16.0	0.0	200.0
-58.0	-25.0	-8.0	0.0	123.0		0.0	16.0	0.0	200.0
-8.0	0.0	8.0	0.0	123.0	7	0.0	16.0	0.0	200.0
ล.ก	0.0	16.0	-4.0	123.0	Ì	0.0	16.0	0.0	200.0
16.0	-4.0	79.0	-35.0			0.0	16.0	0.0	200.0
78.0	-35.0	94.0	-98.0	-120.0		16.0	11.0	200.0	600.0
84.0	-38.0	9399.0	-38.0	-129.0	1-1	16.0	11.0	200.0	600.0
79.0	-35.0	9399.0	-35.0	-127.0		ŭ.ŭ	16.0	0.0	200.074
16.0%	::	9399.0	::- -4. (i	62. 4		0.0	0.0	0. 0.	0.0%
'' -86. A	9-4470 W	-82.0	-97:0	1250	243	16.0	11110	-200.0°	600/0
-AB.00	+37 C 160	garage,53 ibir	95.0			16.0	11.0	200.0	- 600. 0
5.0	-35.0	78.0	-35. U	-120.0		16.0	1120	700.O	600.0
-110.0	46.5	-82.0	. ⊬37.0	-128.0		11.0	11.0	600.0	600.0],
-92.0	497.0	16.0	-4.0	-127.0		15.0	16.02	200.C	k-200v0 u

XT= 8.0 YT= -10.0 XB= -40.0 YB= -3520

GRIDX= 50.0 GRIDY= 25.0 XMAX= 100.0 YMAX= 75.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

67.

THE MIN. FS= 1.45 EFS= 1.18 H(X)= 60.00 G(Y)= 35.00 R= 68.78 THE MIN. EFS= 1.18 FS= 1.45 H(X)= 60.00 G(Y)= 35.00 R= 68.78

FOR SIDE THE

	The state of the state of	· 通過 1 四十四十二十四
THE CORP. THE JAPAN SHIP		B. B. Barry, State

					FE	F1	e E2	TEE THE STATE
. 21 .	¥1.	ME	YE	interest of the second				ФФ4. И
9399.A			49.0 -1			00.0 60.0	A STATE OF STATE OF	999.6
13220		112.0 399.0	- 4 9.0:-1 - 4 9.0:-1	A STATE OF THE PARTY OF THE PAR		00.0		cicc it
the same of the sa		129.5	46.5	-62:4		O. P.	0.0 A.O	ing fi
128.5	-4615	110.0			95.0 95.0	25.0 11.0	. Ú. Ú	600.0
112.0		110.0 105.5	-46.5 - -41.5	125.0	35:0	11.0	0.0	后前位。[6] 1000 第
110.0 105.5		166.0	-39.5	425.0	35.0	11.0	. Q.Q. (Q. () *	600.0 600.0
100.0	-3915			125.0 123.0	35.0 35.0	16.0	Ü_B	200:00
. 86. U		60.6 128.5	-26:0 -46:5	-135.0	* 0. 0 ·	25.0	*0.0	in H. H.
138:0 188:5		117.0	-3920	135.0	. 0. 0 · · · · · · · · · · · · · · · · ·	35.0 35.0	一种。(i) 用_用	B. B.
117.0		107.00 · · · · · · · · · · · · · · · · · ·	—39.0 —25.0	135.0 135.0	U_U	35.0	D_B	· N.H.
107.0 86.0		59.0	-25.0	135.0	0.0 35.0	35.0 46.0	(日)。 (日) 日	200.0
60_0	-26.0	50 k 0 E 0	一之5。0 - 0、0	123.0 123.0	6.6	16.0	0.0	·尼爾斯。他 (2017) 古古诗 (1)
50 P 8 P		0≥0::	0.0	123.0	0.0	16.0 16.0	0.0 0.0	200.0 200.0
8.0	0.0		. — 4. ₪ —35. ₪	123.0 -127.0	0.0 6.0	16.0	FI20	ZOULD :
-16:0 -78:0	-4.0 -35.0	一点 は、 U 一 日本 :D	-38.0	-129.0	16.0	11.0	200.0 200.0	600.0 600.0
	-38, i -	4399_Ü			16-10	11.0 16.0		20020000
"一定各位的"。	- 골5. [1 ~] - 4. [1 ~]	27049.11 - 1015 1	-35,00 -4,00	62.4	0.0	0.0	. D. B.	9 0.0
,"自己"。 有品,他是		BE.0	-37.0	125.0	16.0	11_0 °	200.0 200.0	600.0 600.0
BELO.	3-37.0			-129.0 -126.0	16.0 16.0	11.0	200.0 -	600.0
-5.0 110-0	*-35_0 -46_5	- A220	-37.0	_129±0	11:0	11.0	600.0. 200.0	60020 200-0
	-97.0		- 4. 0	-12710	le.u	LD. U	EBB*C.	
	77.3				a life	7A A		
XT= -50:	jo ij	= -26.0	A.B°	= 50.0				Production of Production
GRIDH	10.0	EPIDY=	P ÚCE	以前代 集	30.0	学性自然		
	TME'r					The Supplement of the Control of the		
		the state of the state of the state of		<u>v</u>	The second secon			
THE MAXI	MUM E.F.3	TO VE	PRIMTED	ES III	MW,			

TEST POINTS

		11.20%	_ 4ñ ññ	547= 160f	in P= 42.	Ŧ,
THE MIM. FS=	1:04 EFS= "			August 1 State of the Control		
	and the second s			Processor Commence		
THE MIN. EFS=		+ na. +(*)	= 40.00	6(Y)= 10.1	in P= 422	3
THE MIN. Et 3-	_ GT	Part of the second of the seco				
. 380 74.949 Ū	METS.		and the second second second	gramma and the second state of the second		
. 2BU 4-343 U	Marian Gran			and the second s		
FIRE COMPLETE.						

FEOLY GETYKAPE5=JMH33 FEADY, RUN

84/08/01.09.25.14. PROGRAM SLOPE2

110 JSF ASH POND "J", R TEST @STA.41+75.RIPRAP 1080.28/WIDE (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

								1,74
X1	Y1	XS	Y2	W	F2	F1	C2	C1
-9399.0	-49.0	-122.0		-1000.0	0.0	100.0	0.0	9999.D
-122.0	-49.0	-112.0	-49. 0	-1000.0	35.0	100.0	0.0	9999.0
-112.0	-49.0	939 9 .0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
-9399.0	-46.5	-118.5	-46. 5	-62.4	0.0	0.0	0.0	0.0
-118.5	-46.5	-110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	35.0	11.0	0.0	600.0
-110.0	-4 6 .5	-105.5	-41.5	125.0	35.0	11.0	0.0	600.0
-105.5	-41.5	-100.0	-39.5	125.0	35.0	11.0	0.0	600.0
-100.0	-39.5	-86.0	-37.0	125.0	35.0	11.0	0.0	600.0
-86.0	-37.0	-6 0.0	-26.0	123.0	35.0	16.0	0.0	200.0
-122.0	-49. 0	-118.5	-46.5	-135.0	0.0	35.0	0.4	0.0
-118.5	-46.5	-96.0	-25.0	135.0	0.0	35.0	0.0	0.0
-86.0	-25.0	-58.0	-25.0	135.0	0.0	35.0	0.0	0.0
-60.0	-26.0	-58.0	-25.0	123.0	0.0	16.0	0.0	200.0
-58.0	-25.0	-8.0	0.0	123.0	0.0	16.0	0.0	200.0
-8.0	0.0	8.0	0.0	123.0	0.0	16.0	0.0	200.0
8.0	0.0	16.0	-4.0	123.0	0.0	16.0	0.0	200.0
16.0	-4.0	78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
78.0	-35.0	84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
84.0	-38.0	93 99 .0	-38.0	-128.0	16.0	11.0	200.0	600.0
78.0	-35.0	9399.0	-35.0	-127.0	0.0	16.0	0.0 -	200.0
16.0	-4.0	939 9 .0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	-82.0	-37.0	125.0	16.0	11.0	200.0	600.0
-82.0	-37.0	5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
5.0	-35.0	78.0	-35.0	-128.0	16.0	11.0	200.0	
-110.0	-46.5	-82.0	-37.0	-128.0	11.0	11.0	600.7	
-82.0	-37.0	16.0	-4.0	-127.0	16.0	16.0	200.0	200.0

XT = 8.0 YT = -5.0 XB = -40.0 YB = -35.0

GRIBX= 20.0 GRIBY= 20.0 XMAX= 100.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.42 FFS= 1.14 H(X)= 50.00 G(Y)= 30.00 P= 64.60

THE MIM. FES= 1.14 FS= 1.42 H(X)= 50.00 G(Y)= 30.00 R= 64.68

		A LIMES

×4		*2****	Y2	a like a	F2	-F1	C2 -	C1
to the transfer of the second section of	nanga indaga indi Amerikan in	150270000	in an anti-ann a 1990 a tha bhail agus an da agus a					
9399.0	-49. D	122.0	-49.0 -	-1000.0	0.0	100.0	inalita da Albaria (Despera	하루 시즌에 경찰 영화 연락하다
122.0	-49.0	112.0	-49.0 ·	-1000.0	35.0	100.0	0:0	9999.0
112.0	-49.0	-9399.0	-49.0 ·	-1000.0	11.0	100.0	600.0	9999.0
9399.0	-46.5	110.5	-46.5	-62.4	0.0	0.0	0.0	0.0
118.5	-46.5	110.0	-46.5	-135.0	35.0	95 . 0	0.0	0.0
112.0	-49_n	110.0	-46.5	-128.0	95.0	11.0	0.0	600.0
110.0	-46.5	1.05.5	-41.5	125.0	35.0	11.0	0.0	600.0
105.5	-41.5	166.6	_94 <u>.</u> 5	125.0	35.0	11.0	0.0	600.0
100.0	-39.5	그 이 생활하면 하다. 중요 그렇	-37.0	125.0	35.0	11.0	0.0	600.0
96.0	-37.0	60.0		123.0	35.0	16.0	0.0	200.0
122.0	-49-0	118.5	-46.5	-135.0	0.0	95 . 6	0.0	0.0
118.5	-46.5	소스 : 소시 교육 표정한 문화원 환경하다	-25.0	195.U	0.0	35.0	0.0	0.0
86.0	-25.0	58.0	-25.0	135.0	0.0	35.0	0.0	0.0
60.0	-26.0		-25.0	123.0	0.0	16.0	0.0	200.0
58.0		9.0	0.0	123.0	0.0	16.0	0.0	200.0
9.0 8.0	0.0		그런 회원으로 그 프로그램을 입니다.	129.0	0.0	16. Ú	0.0	200.0
-8.0	0.0	-16.0	-4.0	129.0	0.0	16.0	0.0	200.0
-16.0		-78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
-78.0	and the second s		num: - ninaut rimmangibliogelämmelet	-128:0	16.0	11.0	200.0	600.0
-84-0	\$100 miles 1990	-9399.0	-38.0	-128.0	16.0	11.0	200.0	600.0
-78.0	T 72 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-9399.0		-127.0	0.0	16.0	0.0	200.0
-16.0		-9399. N		-62.4	00	0.0	0.0	0.0
86.0	-37.0	82.0		4 94 CM + 4, 194	16. D-	11.0	200.0	600.0
20.0 82.0	-37.0	-5.0	-35.0	-128:0	16.0	11.0	200.0	600.0
-5.0	-35.0	-78.0		-129.0	16:0	11.0	200.0	600.0
110.0	-46.5	92.0		-129.0	11.0	11.0	600.0	600.0
82.0	-37.0	-16.0	***	-127.0	16.0	16.0	200.0	200.0
ac.v			F # 14		· . - · -			

XT= 8.0 YT= -5.0 XB= -70.0 YB= -45.0

GRIDX= 25.0 GRIDY= 5.0 XMAX= 120.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIM. FS= 1.06 EFS= .91 H(X)= 45.00 G(Y)= 25.00 R= 57.64

THE MIN. EFS= .91 FS= 1.07 H(X)= 35.00 G(Y)= 5.00 R= 38.80

SBU 78.976 UNTS.

RUN COMPLETE.

```
GET.TAPE5=JM432
READY.
RUN
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94 08/01. 08.52.20. PROGRAM SLOPE2

110 JSF ASH POND "J", R TEST @STA.41+75,RIPRAP 1076,25/WIDE (ERQF= .05 DEPTH DF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

×1	Y1	X5	Y2	l _u i	F2	F1	C2	C1
-939 9 .0	-49.0	-122.0	-49. 0	-1000.0	0.0	100.0		9999.0
-122.0	-49.0	-112.0	-49. 0	-1000.0	35.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
-9399.0	-46.5	-118.5	-46.5	-62.4	0.0	0.0		0.0
-118.5	-46.5	-110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	35.0	11.0	0.0	600.0
-110.0	-46.5	-105.5	-41.5	125.0	35.0	11.0	0.0	600.0
-105.5	-41.5	-100.0	-39.5	125.0	35.0	11.0	0.0	600.0
-100.0	-39.5	-86.0	-37.0	125.0	35.0	11.0	0.0	600.0
-86.0	-37.0	-67.0	-29.0	123.0	35.0	16.0	0.0	200.0
-122.0	-49.0	-118.5	-46.5	-135.0	0.0	35.0	0.0	0.0
-118.5	-46.5	-92.0	-2 9. 0	135.0	θ . θ	35.0	0.0	0.0
- 9 2.0	-29.0	-67.0	-29.0	135.0	0.0°	35.0	0.0	0.0
-67.0	-29.0	-60.0	-26.0	123.0	0.0	16.0	0.0	200.0
-60.0	-26.0	-8.0	0.0	123.0	0.0	16.0	0.0	200.0
-8.0	0.0	8.0	0.0	123.0	0.0	16.0	0.0	200.0
8.0	0.0	16.0	-4.0	123.0	0.0	16.0	0.0	200.0
16.0	-4.0	78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
78.0	-35.0	84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
84.0	-38.0	93 99 .0	-38.0	-128.0	16.0	11.0	200.0	600.0
78.0	-35.0	9399.0	-35.0	-127.0	0.0	16.0	0.0	200.0
16.0	-4.0	9399.0	-4. 0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	-82.0	-37.0	125.0	16.0	11.0	200.0	600.0
-82.0	-37.0	5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
5.0	-35.0	78.0	-35.0	-128.0	16.0	11.0	200.6	600.0
-110.0	-46.5	-82.0	-37.0	-128.0	11.0	11.0	600.0	the state of the first and a
-82.0	-37.0	16.0	-4.0	-127.0	16.0	16.0	200.0	200.0
Sec.								

XT= 8.0 YT= -5.0 XB= -40.0 YB= -35.0

GRIDX= 50.0 GRIDY= 25.0 XMAX= 100.0 YMAX= 75.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.44 EFS= 1.15 H(X)= 60.00 G(Y)= 55.00 R= 89.41

THE MIM. EFS=-1.15 FS=-1.44 H(X)=-60.00 G(Y)=-55.00 R=-69.41

FOR SIDE TWO

THESE ARE THE IMPUT DATA LINES

×1	Y1	**************************************	¥2	e de la company	F2	F1	ce	C1
9399.0	-49.0	122.0	- 4 9.0	-1000.0	ւն, մ	100.0	0.0	9999.0
122.0	-49.0	112.0	-49.0	-1000.0	35.0	100.0	0.0	9999.0
112.0	-49. Ù	-9399.0	- 49. 0	-1000.0	11.0	100.0	600.0	9999.01
9399.0	-46.5	118.5	-46.5	-62.4	0.0	0.0	0.0	0.0
118.5	-46.5	110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
112.0	-49.0	110.0	-46.5	-120.0	35.0	11.0	0.0	600.0
110.0	-46.5	105.5	-41.5	· 125.0	95.0	11.0	0.0	600.0
105.5	-41,5	100.0	-99.5	125.0	35.0	11.0	0.0	600.0
100.0	-39.5	86.0	-37.0	125.0	35.0	11.0	0.0	600.0
8 6. 0	-97.0	67.0	-29.0	123.0	95.0	16.0	0.0	200.0
122.0	-49. 0	119.5	- 46 .5	-135.0	0.0	35.0	0.0	0.0
118.5	-46.5	92.0	-29.0	135.0	0.0	35.0	0.0	0.0
92.0	-29.0	67.0	-29.0	135.0	0.0	95.0	0.0	0.0
67.0	-29.0	60.0	-26.0	123.0	0.0	16.0	0.0	200.0
60.0	-26.0	0.0	0.0	123.0	0.0	16.0	0.0	200.0
9.0	0.0	-8.0	O.O	123.0	0.0	16.0	0.0	200.0
-8 - 0	0.0	-16.0	-4.0	129.0	0.0	16.0	0.0	200.0
-16.0	-4.0	-78.0\	-35.0	-127.0	0.0	16.0	0.0	200.0
-78.0	-35.0	-84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
-84.0	-38.0	-9399. 0	38.0	-120.0	16. O	11.0	200.0	- 5 00.0
-78.0	-35.0	-9399.0	-35.0	· -127.0	0.00	16.0	0.0	200.0
-16.0	-4. D	-93 99. 0	-4.0	-62.4	0.0	ற். ந்	0.6	0.0
86.0	-37.0	92.0	TO SERVICE A CONTRACT OF THE PERSON OF THE P	125.0	16.0	11:0	200.0	600.0
82.0		_5.0	95.0	-128.0	7.07.4.7.6.7.4.4.6.	11.0		600.0
-5.0	-35.0	7 (77, 7)	-35.0	기업 아이 시민 교육 중요 아이들이 없었다.	16.0	11.0	200.0	600.0
110.0	-46.5	92.0		-128.0	11.0			600.0
82.0	-37.0	-16.0	-4.0	-127. Ū	16.0	16.0	200.0	200.0
			177					and the second s

XT = 8.0 YT = -5.0 XB = -70.0 YB = -45.0 GRIDX = 10.0 XMAX = 80.0 YMAX = 80.0 INCX = 10 INCX = 10 INCX = 5

THE MAXIMUM F.S. TO DE PRINTED IS -- 0.00-

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= .96 EFS= .83 H(X)= 50.00 G(Y)= 30.00 R= 64.68THE MIN. EFS= .83 FS= .97 H(X)= 40.00 G(Y)= 20.00 R= 55.62SBU 78.122 UNTS.

RUN COMPLETE.

347°7/31. 14.06.53. %ROGRAM SLOPE2

110 JSF ASH POND "J", R TEST @STA.41+75*RIPRAP1080*BERM10/@1070 (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE IMPUT DATA LINES

×1	Y1	1,37%	1.00					
V.1	1 1	X2	Y2	(J)	F2	F1	C2	Ch.
-9399.0	-49.0	-132.0	-49. ñ	-1000.0	0.0	100.0		
-132.0	-49. 0	-112.0		-1000.0				9999.0
-112.0	-49. 0	9399.0	-49.0	-1000.0	35.0	100.0		9999.0
- 9 39 9 .0	-46.5	-128.5	-46.5	-1000.0 -62.4	11.0	100.0		9 999 .0
-128.5	-46.5	-110.0	-46.5	-135.0	0.0	0.0		0.0
-112.0	-49.0	-110.0	-46.5	-128.0	35.0	35.0		0.0
-110.0	-46.5	-105.5	-41.5		35.0	11.0	0.0	4.50 (4
-105.5	-41.5			125.0	35.0	11.0		- 600 .a -
-100.0	-39.5	-100.0	-39.5	125.0	35.0	11.0		600.0
-86.0		-86.0	-37.0	125.0	35.0	11.0	0.0	600.0
	-37.0	-60.0	-26.0	123.0	35.0	16.0	0.0	200.0
-132.0	-49.0	-129.5	-46.5	-135.0	0.0	35.0	0.0	0.0
-128.5	-46.5	-111.0	-35.0	135.0	0.0	35.0	0.0	0.0
-111.0	-35.0	-101.0	-35.0	135.0	0.0	35.0	0.0	ű. ñ
-101.0	-35.0	-8 6. 0	-25.0	135.0	0.0	35.0	0.0	Õ.Õ
-8 6. 0	-25.0	-58.0	-25.0	135.0	0.0	35.0	0.0	Ö.Ö
-6 0.0	-2 6 .0	-58 .0	-25.0	123.0	35.0	16.0	0.0	FM 40.7
-58.0	-25.0	-8.0	0.0	123.0	0.0	16.0	0.0	200.0
-8.0	0.0	8.0	0.0	123.0	0.0	16.0	0.0	200.0
8.0	0.0	16.0	-4. 0	123.0	0.0	16.0	0.0	200.0
16.0	-4.0	78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
78.0	-35.0	84.0	-38.0	-128.0	16.0	11.0	200.0	
84.0	-38.0	9399.0	-38.0	-128.0	16.0	11.0	200.0	600.0
78.0	-35.0	9399.0	-35.0	-127.0	0.0	16.0	0.0	ST 10 TO 10
16.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	
-86.0	-37.0	-82.0	-37.0	125.0	16.0			0.0
-82.0	-37.0	5.0	-35.0	-128.0		11.0	200.0	600.0
5.0	-35.0	78.0	-35.0 -35.0	-128.0	16.0	11.0	200.0	600.0
-110.0	-46.5	-82.0	-37.0 -37.0		16.0	11.0	200.0	
-82.0	-37.0	16.0	-37.0 -4.0	-128.0	11.0	11.0	600.0	600.0-
Total Company (St. 1921)	er e u	10.0	-4. U	-127.0	16.0	16.0	200.0	200.0

XT = 8.0 YT = -10.0 XB = -40.0 YB = -35.0

GRIDX= 50.0 GRIDY= 25.0 XMAX= 100.0 YMAX= 75.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.45 EFS= 1.18 H(X)= 60.00 G(Y)= 35.00 P= 68.78

THE MIN. EFS= 1.18 FS= 1.45 H(X)= 60.00 G(7)= 35.00 P= 50.70

FOR SIDE TWO

THESE ARE THE INPUT DATA LIMES

		we.	42	in the second	F2	F1	C2	E İ
and the state of t	N. E.	erresta e madri e carrinte e pre-		and the second second		an and an installation	i.i	9999.0
9399.0 -4	9.0	132.0		-1000.0	0.0	100.0	0.0	9999.0
132.0 -4		112.0		-1000.0	35.0	100.0	600.0	9999.0
	ν 4 .0 -	-93 99. 0	-49.Ú	-1000.0	11.0	100.0	արդս.ս Ո.Ս	0.0
1 2 to 1 2	6.5	128.5	-46.5	-62.4	0.0	0.0		0.0
128.5		110.0	-46.5	-135.0 ··	35.0	35.0	0.0	그 그런 16호텔 등록 개월하다
the beautiful and the	19.0	110.0	-46.5	-129.0	95.U	11.0	0.0	
	16.5	105.5	-41.5	125.0	35.0	11.0	o. Ç	Table 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
105.5		100.0		125.0	35.0	11.0	0.0	
100.0	71.J	그림 이 그 그는 한국의 중 상략된 그림을 보였다.	-97.0	125.0	35.0	Space of a first and a first	0.0	600.0
96.0 -	97.0	60.0	-26.0	123.0	35.0	16.0	0.0	2.5
	49.0	128.5	-46.5	-135.0	0.0	35.0		0.0
2022	46.5	111.0	-95.0	135.0	0.0	35.Ū	0.0	
2 5 m m 8 m	35.0	10120	-35.0	135.0	0.0		0.0	
	35.0	86.0	-25.0	135.0	0.0	95.0		0.0
	25 A	59 . 0	-25.0	135.0	Û.Û	35.0		0.0
	26.0	58.0	-25.0	123.0	35.0	16.0	0.0	200.0
	25.0	8.0	0.0	129.0	0.0	16:0	0.0	200.0
Tank Tank W. W.	0.0	-0.0	0.O	123.0	0.0	16.0	0.0	200.0
₩ ■ ₩	0.0	-16.0	-4.0	129.0	0.0	16.0	0.0	200.0
~ .	-4.0	-78.0 ⁰⁰	-35. Ø	-127.0	0.0	16.0	0.0	The state of the s
·	-4.0 95.0	-8 4: 0	-39.0		16.0	11.0	200.0	600.0
		-93 99 .0	-38.0		i6:0-	11.0		
		-9399.0	-35.0		O.O.	16.0	0.0	200.0
		- 9399. 0	-4.0		Ũ.Ū	0.0		0.0
*		82.0	-37.0		16.0	11.0	200.0	600.0
		-5.0	-35.0		16.0	11.0		
	37.0 35.0	-78.0	_95.A	-129.0	16.0	11.0	200.0	
	AC 5	82.0	-37.0		11.0	110	and the second second	600.0
		-16.0	-4.0	-127.0	16.0	16.0	200.0	200.0
82.0 -	OF EVEN UP						**	
							2.0	

XT= 50.0 YT= -26.0 XB= 50.0 YB= -70.0

GRIDX= 10.0 GRIDY= 10.0 XMAX= 80.0 YMAX= 80.0

INCX= 10 INCY= 10 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS=
$$1.04$$
 EFS= $.89$ H(X)= 40.00 G(Y)= 10.00 R= 42.37 THE MIN. EFS= $.89$ FS= 1.04 H(X)= 40.00 G(Y)= 10.00 R= 42.37 SBU 74.300 UNTS.

RUM COMPLETE.

READY.

READY.

READY.

RUN

84/07/31. 08.57.26. PROGRAM SLOPE2

110 JSF ASH POND "J", R TEST @STA.41+75,RIPRAP1080BERM10/@1065 (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

FALURE THRU THE BERM

THESE ARE THE INPUT DATA LINES

									41 H 3 A A A A A A A A A A A A A A A A A A
	×1	Y1	XS	Y2	l _e l	F2	F1	C2	C1
_	-93 99 .0	-49.0	-132.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
	-132.0	-49.0	-112.0	-49.0	-1000.0	35.0	100.0	0.0	9999.0
	-112.0	-49.0	9399 .0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
-	-939 9 .0	-46.5	-128.5	- 46 .5	-62.4	0.0	0.0	0.0	0.0
	-128.5	-46.5	-110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
	-112.0	-49.0	-110.0	-46.5	-128.0	35.0	11.0	0.0	600.0
	-110.0	-46.5	-105.5	-41.5	125.0	35.0	11.0	0.0	600.0
	-105.5	-41.5	-100.0	-39.5	125.0	35.0	11.0	0.0	600.0
	-100.0	-39.5	-8 6 .0	-37.0	125.0	35.0	11.0	0.0	600.0
	-86.0	-37.0	-60.0	-26.0	123.0	35.0	16.0	0.0	200.0
	-132.0	-49.0	-128.5	-46. 5	-135.0	0.0	35.0	Đ, Ú	0.0
	-129.5	-46 .5	-117.0	-39.0	135.0	0.0	35.0		0.0
	-117.0		-107.0						
	-107.0		-86.0						
	-86.0	-25.0		-25.0			35.0	G. G. Carlotte	
	-60.0	-26.0	-59.0	-25.0	123.0		16.0	ST 1 25 10 10 10 10 10 10 10 10 10 10 10 10 10	一、大力工工工工工工工工工工工工工工工工工工工工工工工工工工工工工工工工工工工工
W	-58.0	-25.0	-8 .0	0.0	123.0		16.0	\$500 P P P P P P P P P P P P P P P P P P	
	-8.0	0.0	8.0	0.0	123.0		16.0		The state of the s
	8.0	0.0	16.0	-4.0	123.0	0.0		0.0	
	16.0	-4.0	78.0	-35.0	-127.0	0.0	5.0	0.00	 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
	78.0	-35.0	84.0	-38.0	-128.0	16.0		200.0	
	84.0	-38.0	9399.0	-38.0	-128.0	16.0	11.0		
	78.0	-35.0	9399.0	-35.0	-127.0	0.0		0.0	2. Y. V.
	16.0	-4.0	9399.0	-4.0	-62.4	0.0		energia (i. verte de Albago (Alba)).	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	-86.0	- 37.0	-82.0	-37.0	125.0	16.0		200.0	. 705.5566
	-82.0	-37.0	5.0	-35.0	-128.0	16.0		200.0	C
	5.0	-35.0	78.0	-35.0	-128.0	16.0	11.0		600.0
	-110.0	-46.5	-82 .0	-37.0	-128.0	11.0	11.0		- 151,840
	-82.0	-37.0	16.0	-4.0	-127.0	16.0	16.0	200.0	200.0

XT = 8.0 YT = -10.0 XB = -40.0 YB = -35.0

GRIDX= 50.0 GRIDY= 25.0 XMAX= 100.0 YMAX= 75.0

IMCX= 10 IMCY= 10 IMCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MORIMUM E E C IN DE DOINTEN TO A AA

TEST POINTS

X1	∵'1 */*	2005/W2	~~~ Y2 ~>	o-tracy W asses		Fi	C2	C1
9399.0	-49.0	132.0	46.6					
132.0	-49. 0	The state of the s			0.0	250, 442, 743, 741, 75	The second second	9999.0
112.0				-1000.0	30.U	100.0	0.0	The same of the sa
9399.A	-46.5	128.5				100.0		
128.5	-46.5			-62.4		0.0	0.0	
112.0	-49.0			-135.0		35.0		0.0
110.0	-46.5			-129.0		11.0		
105.5	-41.5			125.0		11.0		
100.0				125.0		11.0		
86.0	-39.5			125.0		11.0		7. 2.4.4
	-37.0		-26.0		35.0		3	200.0
132.0	10.0	129.5			. 0.0		0.0	-
128.5	-46.5				0.0	35.0		0.0
117.0		107.0				95.0		0.0
107.0		36.0			0.0	35.0	0.0	0.0
96. 0	20 to 20 20 20 to 30 20 20 20 20 20 20 20 20 20 20 20 20 20	58.0	A 5 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		0.0	35.0		0.0
60.0		58.0	-25.0			16.0		200.0
58.0		8.0	10 March 10			16.0	0.0	200.0
8.0	0.0				0.0	16.0	0.0	200.0
-8.0	0.0	-16.0	-4.0	129.0		1 6 .0	0.0	200.0
		-78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
		-94.0	-38.0	-129.0	16.0	11:0	200.0	600.0
-94.0		-9399. 0	-38.0	-129.0	16.0	11.0	200.0	
		-9399.0			0.0	16.0		200.0
-16.0	-4 .0-	-9399 .0	-4.0	-62.4		0,0	0.0	0.0
86.0	-37.0	82.0	-37.0	125.0	16.0			600.0
82.0	-97.0	-5.Ú	-35.0	-128.0	16.0			600.0
	-35.0	-78.0	-35.0	-128.0	16.0			600.0
110.0	-46.5	82.0	-37.0	-128.0	11.0	11.0		600.0
92.0	-37.0	-16.0	-4.0	-127.0	16.0	16.0		200.0
								See The That BE 1 The

XT= 115.0 YT= -41.0 XB= 115.0 YB= -51.0

GRIDX= 70.0 GRIDY= 70.0 XMAX= 120.0 YMAX= 130.0

INCX= 10 INCY= 10 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.27 EFS= 1.08 H(X)= 90.00 G(Y)= 90.00 R= 138.37

THE MIN. EFS= 1.08 FS= 1.27 H(X)= 90.00 G(Y)= 100.00 R= 148.21

-SBU 31.666 UNTS.

RUH COMPLETE.

0.312 UNTS. SBU READY. OLD, SLOPE2 READY. FTN READY. GET. TAPE5=JMH30 READY. RUN 84/07/31. 09.10.29. PROGRAM SLOPE2 110 JSF ASH POND "J", R TEST @STA.41+75,RIPRAP1000BERM10/@1065 DEPTH OF ROCK = 49.0 FT) PAILURE ABOVE THE BERM . 05 THESE ARE THE INPUT DATA LINES $\times 1$ Y1 X2 Y2 F2 F1 C2 C1 -9399.0 -132.0 -112.0 -49.0-49.0 -1000.0 0.0100.0 -192.0-49.0 0.0 9999.0 -49.0 -1000.035.0 100.0 -112.0-49.0 9399.0 0.0 9999.0 -49.0 -1000.0 -9399.0 11.0 100.0 600.0 9999.0 -46.5 -129.5-46.5-62.4 -128.50.00.0 0.0 0.0 **-46.5 -110.0** -46.5 + 135.035.0 35.0 0.0 0.0 -112.0-49.0-110.0 -46.5 -128.0 35.0 11.0 0.0 600.0 -110.0-105.5-46.5-41.5125.0 35.0 11.0 0.0 600.0 -105.5-100.0 -41.5-39.5125.0 35.011.0 0.0 600.0 -100.0 -39.5-86.0 -37.0 125.0 **95.**0 -86.0 11.0 0.0 600.0 -37.0-60.0-26.0 123.0 35.0 16.0 -132.0 0.0 200.0 -49.0-128.5-46.5 -135.0 0.0 35.0 -128.50.0 -46.50.0 -117.0-39.0135.0 0.0 35.0 Û.Û 0.0 -117.0-39.0 -107.0-39.0 135.0 0.0 35.0 0.0 -107.0-86.0 0.0 -39.0 -25.0135.0 0.0 35.0 0.0 0.0 -86.0 -58.0 -25.0-25.00.0 35.0 0.0 135.0 -60.00.0 -58.0 -26.0 123.0 35.0 16.0 0.0 200.0 -25.0-58.0-25.0 -8.0 123.0 0.0 16.0 0.0 0.0-8.0 200.0 0.08.0 123.0 0.0 16.0 0.0 0.0 200.0 8.0 0.0 16.0 -4.0 123.0 16.0 000 200.0 0.0 16.0 -4.0 78.0 –35.0 –127.0 0.0 16.0 0.0 79.0 84.0 -39.0 -128.0 16.0 200.0 -35.0 11:0 200.0 600.0 84. O -98.0 9999.0 -38.0 -128.0 -30.0 7377.0 30.0 120.0 10.0 11.0 0.0 -35.0 -127.0 0.0 16.0 0.0 0.0 -4.0 +62.4 0.0 0.0 10.0 16.0 - 11:00 200.0 600.0 0.0 200.0 79.0 16.0 200.0 0:0 -**4.**0 - -97.0:44 -82.0+ -37.0 - 125.0: -86.0 16.0 ... 11.0 .. 20020 -37.01 5.0 -35.0 78.0 600,0 -82.0 -35.0 -128.0° 16.0 11.0 200.0 600.0 5.0 -35.0 -128.0 16.0 11:0 200;0 600;0 -**46.**5 -02.0 -37.0 -120.0 11.0 -110.0 11.0 -82.0 -97.0 600.0 600.0 16.0 -**4.**0 -127.0 16.0 16.0 200.0 200.0 XT= 8.0 YT= -10.0 XB= -40.0 Y**B=** −35.0 GRIDX= 50.0 GRIDY= 25.0 XMAX= 100.0 YMAX= INCX= 10 INCY= 10 INCR= 10 THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO DE PRINTED IS 0.00 TEST POINTS

THE MIN. FS-

THE MIM. EFS# 1.18

1.45

EFS=

F5=

1.18

1.45

 $H(X) = -60.00 \setminus -6(Y) = -$

H(X)= 60.00 G(Y)= 35.00 R= 68.78

35.00% P= 68.78

FOR SIDE TWO

							-1		
	X1	٧1	. 5K	ya.	ld .	F2	F1	CS	C1
93	99.0	- 49. 0	132.0	-49. 0	-1000.0	0.0	100.0	0.0	9999.0
1	32.0	-49.0	112.0	-49.0	-1000.0	35.0	100.0	0.0	9999.0
_1	12.0		-9399.0	E	-1000.0	the state of the s	100.0	600.0	9999.0
99	99.0	-4 6 .5	120.5		-62.4	0.0	0.0	0.0	0.0
1	28.5	-46.5	110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
1	12.0	-49.0	110.0	-46.5	-128.0	35.0	11.0	0.0	600.0
1	10.0	-4 6 .5	105.5	-41.5	125.0	35.0	11.0	0.0	600.0
1	05.5	-41.5	100.0	-39.5	125.0	35.0	11.0	0.0	600.0
1	00.0	-39.5	96.0	-37.0	125.0	35.0	11.0	0.0	600.0
	9 6. 0	-37.0	60.0	-26.0	123.0	35.0	16.0	0.0	200.0
1	32.0	-49. 0	128.5	-46.5	-135.0	0.0	35.0	0.0	0.0
1	20.5	-46. 5	117.0	-39.0	135.0	0.0	35.0	$0 \downarrow 0$	0.0
1	17.0	-39.0	107.0	-39.0	135.0	0.0	35.0	0.0	0.0
1	07.0	-39.0	8 6 .0	-25.0	135.0	0.0	35.0	0.0	0.0
	86:0	-25.0	58.0	-25.0	135.0	0.0	35.0	0.0	0.0
	60.0	-26.0	58.0	-25.0	123.0	35.0	16.0	0.0	200.0
	59.0	-25.0	8.0	0.0	123.0	0.0	16.0	0.0	200.0
		$\Omega_{\rm co}\Omega_{\rm co}$:- a ₄ :0−0; 0	4. OJO:	123:0	0.0	16.0	0.0	200.0
	-8.0	ប៉ុន្តិ	-16.0	-4.0	123.0	0.0	16.0	0.0	200.0
	16.0	-4. Ū	-79.0	-35.0	-127.0	0.0	1 6 .0	0.0	200.0
-	78.0	-35.0	-94.0	-38.0	-128.0	16.0	11.0	200.0	600.0
	84.0	-38.0	-9399.0	-38.0	-128.0	16.0	11.0	200.0	600.0
	78.0	-35.0	-939 9 .0	-35.0	-127.0	0.0	16.0	0.0	200.0
	16.0	-4.0	-9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
	86.0	-37.0	82.0	-37.0	125.0	16.0	11.0	200.0	600.0
	82.0	-37.0	-5.0	-95.0	-128.0	1 6 .0	11.0	200.0	600.0
	-5.0	-35.0	-79.0	-35.0	-128.0	16,0	11.0	200.0	600.0
1	10.0	-46.5	82.0	-97.0	-128.0	11.0	11.0	600.0	600.0
	82.0	-37.0	-16.0	-4.0	-127.0	16.0	16:0	200.0	200.0
		450.5	AND SECTION OF SECTION						

XT= 80.0 YT= -27.0 XB= 115.0 YB= -51.0

GRIDX= 10.0 GRIDY= 10.0 XMAX= 90.0 YMAX= 80.0

INCX= 10 INCY= 10 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIM. FS = 1.12 EFS = 1.96 H(X) = 50.00 G(Y) = 20.00 R = 55.77

THE MIN. EFS= .96 FS= 1.12 H(X)= 50.00 G(Y)= 20.00 R= |55.77

SBU 55.412 UNT9.

RUN COMPLETE. BYE

THE ESTIMATED COST OF THIS JOB IS: \$ 8.46

KXFDPDC LOG OFF 09.14.34. SBU = 139.894 TIO = 21956

IAF COMMECT TIME 00.27.32. LOGGED OUT.

EI,THPE5=_MH31 READY. MUS 84/07/31. 11.18.20. PROGRAM SLOPE2 110 USF ASH POND "U" R TEST @STA. 41+75,RIPRAP1080,BERM10/@1070 (ERQF= .05 DEPTH OF ROCK= 49.0 FT) FAIWRE ABUE BERM THESE ARE THE IMPUT DATA LINES X1 Y1 X2 Y2 W F2 F1 C2 C1 0.0 9999.0 -9399.0 -49.0 -132.0 -49.0 -1000.0 0.0 100.00.0 9999.0 --132.0 -49.0 -112.0 -49.0 -1000.0 35.0 100.0 11.0 100.0 600.0 9999.0 -112.0 -49.0 9399.0 -49.0 -1000.0 9.0 9.0 9.0 0.0 0.0 -9399.0 -46.5 -128.5 -46.5 -62.4 0.0 0.0 -128.5 -46.5 -110.0 -46.5 -135.0 35.0 35.0 600.0 35.0 11.0 Ú.Ú -49.0 -110.0 -46.5 -128.0 -105.5 -41.5 125.0 35.0 11.0 0.0 600.0 -112.0 -110.0 -45.5 -39.5 125.0 35.0 11.0 600.0 0.0 -100.0-105.5-41.5-37.0 125.0 35.0 11.0 -26.0 123.0 35.0 16.0 mill. D 0.0 -99.5 -86.N -100.00.0 200.0 -37.0 -60.0 -86.0-46.5 -135.0 0.0 35.0 0.0 0.0-49.0 -128.5 -132.0 35.0 0.0 0.0 -35.0 135.0 0.0 -46.5 -111.0 -128.535.0 0.0 0.0 -35.0 135.0 O.O -35.0 -101.0-111. Ū 0.0 0.0 35.0 -25.0 135.0 0.0 -35.0 -96.0 -101.035.0 0.0 0.0 0.0 -25.0 135.0 -25.0 -59**.**0 -86.0 35.0 <u>16.0</u> 0.0 200.0 -26.0 -59.0 -25.0 123.0 -60.016.0 0.0 200.0 -25.0 -8.0 0.0 123.0 0.0 -58.0 200.0 0.0 0.0 123.0 0.0 16.0 **9.**0 -8.0 0.0 0.0 200.0 0.0 16.0 8.0 0.0 16.0 -4.0 123.0 200.0 0.0 16.0 -4.0 78.0 -35.0 -127.0 16.0 84.0 -38.0 -128.0 16.0 11.0 200.0 600.0 -35.0 78.Û 600.0 200.0 16.0 11.0 -30.0 -128.0 -38.0 9399.0 34.0 0.0 200.0 16.0 --35.0 -127.D O.O -35.0 9399.0 78.0 Ū.Ū 0.0 0.0 0.0 -4.0 -62.4 -4.0 9399.0 16.0 16.0 600.0 11.0 200.0 -97.0 -92.0 -37.0 12**5.**0 -96.0 600.0 200.0 16.0 11.0 -35.0 -128.0 -27.0 5.0 -A2_0 600.0 200.0 11.0 70.0 16.0 -35.0 -128.0 -35.05.0 600.0 -600.011.Ü 11.0 -37.0 -128.0 -82.0 -46.5 -110.0200.0 16.0 200.0 16.0 -4.0 -127.0 -37.0 16.0 -82.0 XT = 8.0 YT = -10.0 XB = -40.0 YB = -35.0GRIDX= 50.0 GRIDY= 25.0 XMAX= 100.0 YMAX= 75.0 INCX= 10 INCY= 10 INCR= 10 THE MAXIMUM F.S. TO BE PRINTED IS 9.00 THE MINIMUM E.F.S. TO BE PRINTED IS 0.00 THE MIN. FS= 1.45 EFS= 1.10 H(X)= 60.00 G(Y)= 35.00 R= 60.70 THE MIN. EFS= 1.18 FS= 1.45 H(X)= 60.00 G(Y)= 35.00

₁()

×1			YA	e emergencia com a describir de la proposición en		en er er er stembier der bei er	e en en en en Englande en en	
		. , _	-		7 1		San Ban	0.2
9399.0	-49.0	132.0	-49. n	-1000 0	$\Omega = \Omega$	100.0	B B	gaga A
132.0	-49.0	112.0				100.0		
112.0	-49. Û	-9399. n		-1000.0		100.0		
9399.0	-46.5	128.5				0.0		
128.5	-46.5	110.0	-46.5	-135.0	95.0	35.0	Ů. Ú	
112.0	- 4 9.0	110.0	-46.5			11.0	0.0	
110.0	-46.5	105.5	-41.5	125.0		11.0	0.0	
105.5	-41.5	100.0	-39.5	125.0	35.0	11.0	0.0	600.0
100.0	-3 9 .5	86.0	-37.0	125.0	35.0	11.0	0.0	600.0
86.0	-37.0	60.0	-26.0	123.0	35.0	16.0	0.0	200.0
132.0	-49. 0	128.5	-46. 5	-135.0	0.0	35.0	0.0	0.0
128.5	-46 .5	111:0	-95.0	135.0	0.0	95.0	0 - 0	0.0
111.0	-35.0	101.0	-35.0	135.0	0.0	35.0	0.0	0.0
101.0	-35.0	86.0	-25.0	135.0	0.0	35.0	0.0	0.0
86.0	-25.0	59.0	-25.0	135.0	0.0	35.0	0.0	0.0
60.0	-2 6 .0	58.0	-25.0	123.0	35.0	16.0	0.0	200.0
58.0	-25.0	9.0	» 0 : 0	123.0	0.0	16.0	0.0	200.0
8.0	0.0	-8.0	0.0	123.0	0.0	16.0	0.0	200.0
-8.0	0.0	-16.0	-4.0	123.0	0.0	16.0	0.0	200.0
-16.0	-4.0	-78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
-78.0	-35.0	-84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
-84.0		-9399.0	-39.0	-128.0	16.0	11.0	200.0	6 00.0
-78.0		-9999. 0	-35.0	-127.0	0.0	16.0	0.0	200.0
-16.0 86.0		-9 399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
82.0	-37.0		-37.0	125.0	16.0			600.0
	-97.0	-5.0	-35.0	-128.0	16.0	11.0	200.0	600.0
-5.0	-35.0	-78.0	-35.0	-128.0	16.0	11.0	200.0	600.0
110.0 82.0	-46.5	92.0	- 97.0	-128.0	11.0	11.0	600.0	600.0
oc. U	-37.0	-16.0	-4.0	-127.0	1 6 .0	16.0	200.0	200.0

XT= 80.0 YT= -27.0 XB= 115.0 YB= -51.0

GRIDX= 10.0 GRIDY= 10.0 XMAX= 80.0 YMAX= 80.0

IMCX= 10 IMCY= 10 IMCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIM. FS= 1.12 EFS= .96 H(X)= 50.00 G(Y)

THE MIM. EFS= .96 FS= 1.12 H(X)= 50.00

SBU 56.005 UNTS.

- RUN COMPLETE.

READY. RUN PROGRAM SLOPE2

84/07/31. 11.26.03.

110 USF ASH POND "J", R TEST @STA.41+75.RIPRAP1080.BERM10/@4070 .05 DEPTH OF ROCK= 49.0 FT) (ERQF= FALURE THRU THE BERM

THESE ARE THE IMPUT DATA LINES

×1	Y1	X5	Y2	i,d	, F2	. F1	C2	C1
-9399.0	-49.0	-132.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-132.0	-49.0	-112.0	-49.0	-1000.0	35.0	100.0	0.0	9999.0
-112.0	-49. N	9399.0	-49.0	-1000.0	11.0	100.0	600.0	9999.0
-9399. n	-46.5	-128-5	-46.5	-62.4	0.0	0.0	0.0	0.0
-128.5	-46.5	-110.0	-46.5		35.0	35.0	0.6	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	35.0	11.0	0.0	600.0
-110.0	- 46 .5	-105.5	-41.5	125.0	35.0	11.0	0.0	600.0
-105.5	-41.5	-100.0	-39.5	125.0	35.0	11.0	0.0	600.0
-100.0	-39.5	-86.0	-37.0	125.0	35.0	11.0	0.0	600.0
-86.0	-37.0	-60.0	-2 6. 0	123.0	35.0	16.0	0.0	200.0
-132.0	-49.0	-128.5	-46.5	-135.0	0.0	35.0	0.0	0.0
-128.5	-46.5	-111.0	-35.0	135.0	0.0	35.0	0.0	0.0
-111.0	-35.0	-101.0	-35.0	135.0	0.0	35.0	0.0	0.0
-101.0	-35.0	-86.0	-25.0	135.0	0.0	35.0	0.0	0.0
-86.0	-25.0	-58.0	-25.0	135.0	0.0	35.0	0.0	0.0
-60.0	-2 6 .0	-59.0	-25.0	123.0	35.0	16.0	0.0	200.0
-58.0	-25.0	-8 .0	0.0	123.Û	0.0	16.0	0.0	200.0
-9.0	0.0	8.0	0.0	123.0	0.0	16.0	0.0	200.0
8.0	0.0	16.0	-4.0	123.0	0.0	16.0	0,0	200.0
16.0	-4.0	78.0	-35.0	-127.0	0.0	16.0	0.0	200.0
78.0	-35.0	84.0	-38.0	-128.0	16.0	11.0	200.0	600.0
84.0	-38.0	9399.0	-38.0	-128.0	16.0	11.0	200.0	600.0
78.0	-35.0	93 99 .0	-35.0	-127.0	0.0	16.0	0.0	200.0
16.0	-4. 0	9 3 99 .0	-4.0	-6 2.4	0.0	0.0	0.0	0.0
-86.0	-37.0	-82.0	-97.0	125.0	16.0	11.0 11.0	200.0 200.0	600.0 600.0
-82.0 5.0	-97.0 -95.0	5.0 78.0	-35.0 -35.0	-120.0 -120.0	16.0 16.0	11.0	200.0	600.0
-110.0	-46.5	-82.0	-37.0	-128.0	11.0	11.0	600.0	
-110.0 -82.0	-37.0	16.0	-4.0	-127. N	16.0	16.0	200.0	200.0
	-01 • U	EC. C	TEU	11-1-1	10.0	aws u	E0010	

8.0 $YT = -10.0 \times B = -40.0$ YB = -35.0 $\times T =$

GRIDX= 50.0 GRIDY= 25.0 $\times MH = 100.0$

INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIM. FS=---1.45-- EFS=-60.00G(Y) = 35.00 R = 68.78

FOR SIDE THE

THESE ARE THE IMPUT DATA LINES

×ı	Y1	%2	YZ.		E9			
		A STATE OF					CE	C1
9399.0	-49. 0	132.0	-49.0 -	-1000 0	0.0	+ 6.6.		
132.0	-49. 0	112.0	-49.0 -	-1 0 A A . A	95.0	100.0	0.17 0.0	
112.0	-49.0	-9 3 99. 0	- 4 9.0 -	-1000. A	11.0	100.0	600.0	9999.0
9399.0 128.5	-46.5	128.5	-46.5	-62.4	ō.ŏ	0.0	0.0	9999.0
112.0	-46.5	110.0	-46.5	-135.0	35.0	35.0	0.0	
110.0	-49.0 -46.5	110.0	-46.5		35.0	11.0	0.0	0.0 600.0
105.5	-41.5	105.5	-41.5	125.0	35.O	11.0	0.0	600.0
100.0	-3 9 .5	100.0	-39. 5	125.0	35.0	11.0	n naide a flace	600.0
86.0	-37.0	9 6 .0			35.0	11.0	0.0	600.0
132.0	-49.0	60.0	-26 .0	123.0	35.0	16.0	0.0	200.0
128.5	-46.5	128.5	-46.5		0.0	35.0	0.0	0.0
111.0	-35.0	111.0	-35.0	135.0	0.0	35.0	0.0	0.0
101.0	-35.0	101.0	-95.0.	135.0	0.0	35.0		0.0
86.0	-3J.0 -25.0	8 6 .0	-25.0	135.0	θ . θ	35.0	0.0	0.0
60.0	-25.0 -26.0	58.0	- 25.0 \	195.0	0.0	35.0	0.0	0.0
58.0	-25.0	5 8 .0	-25.0	123.0	35.0	16.0		200.0
8.0	0.0	-8.0 -8.0	0.0	123.0	θ . θ	16.0	O.Ŏ	200.0
-8.0	0.0	-16.0	0.0	123.0	0.0	16.0		
-16.0	-4.0	-78.0	-35.0 -	123.0	u. u 0: 0:	16.0	A A	200 0
-78.0	-35.0	-84.0		_1C.* 0	0.0	16.0	and Brobbs and	⊇aa a
-84.0		-939 9 .0		100.U 100.n	16.0	11.0	200.0	600.0
-78.0	-35.0 -	-9399_n	-35 a .	107 O	16.0	11.0	200.0	600.0
-16.0		~ ~	-4 A		0.0 0.0			200.0
8 6 .0	-97.0	82.n	_a, , ,	125 0	0.0 16.0	, U. U	/V. 0. 0	0.0
82.0	-97.0	-5 <u>-</u> ñ	-95 n -	150.0 150.6	16.0	11.0	200.0	600.0
-5.0	-35.0	-78 ñ	-35 A -	160.0	16.0	11.0	200.0	600.0
110.0		82 n	-27 6	120.U	16.0	11:0	200.0	600.0
82.0	-37 n	-16 n	_4 0	100.0	11:0	11.0	600.0	600.0
	There's Was		· · · · · · · · · · · · · · · · · · ·	127.0	16.0	1 6 .0	200.0	200.0
XT= 105.								
A)- 105.	ነ ነ	= -37.0	×B=	105.0	YB=	-52.0	•	
GRIDX=	10.0	GBITH						
			10.0	XMHX=	80.0	YM A X:	= 80.0	
INCX= 10	INCY	= 10	INCR= 5					
THE MAXIM	MM F.S	TO BE DO:	NTED TO					
		· u be thi	ILLER TZ	0.00				

TEST POINTS

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

THE MIN. FS= 1.31 EFS= 1.10 H(X) = 70.00 G(Y) = 50.00 R= 98.79

THE MIN. EFS= 1.10 FS= 1.31 H(X) = 70.00 G(Y) = 50.00 R= 98.79

BU 24.937 UNTS.

RUN COMPLETE.

```
84/07/21. 09.39.08. AA2D5DA
SN214 . *TVA* CHATTANDOGA,TN. NBS
FAMILY: KVA
                                            1.4/531.462/2AB
USER NAME: KXFDPDC + PASSWORD
经基础证据证明
TERMINAL: 23, NAMIAF
RECOVER/ CHARGE: CHAR, A3501PE, +CD2+JSF
___ENTER USER-ID (FIRST INITIAL PLUS LAST NAME)
? RPOWELLL
                ***** ATTENTION INTERACTIVE USERS *****
 IF YOU ARE EXPERIENCING VERY SLOW RESPONSE TIME AT CONSISTENTLY GREATER
 THAN 15 SECONDS, PLEASE REMAIN ON LINE AND CALL THE COMPUTER SERVICES
 STAFF AT #2383, KNOXVILLE. KNOWING YOUR TTY NUMBER WOULD BE USEFUL.
 REMAIN ON-LINE: !!!!!!!
                                                             MAY 29, 1984.
 THE FOLLOWING IS A LIST OF THE PROGRAMS AVAILABLE ON KVA WHICH HAVE
 BEEN VALIDATED FOR SAFETY-RELATED ANALYSIS AND DESIGN AS REQUIRED BY
 ENDES EP3.23;
                  TVA IN-HOUSE PROGRAMS-
  BOLT
            EADHI
                        TRIPE
                                                                     TVA WELDDA
                                   FRAMS
                                              GLOBAL
                                                          CASI
  AMCHOR
            WEDATA
                       EMVELOPE
                                   U-BOLT
                                              SPECTRA
                                                          DBASQN
                                                                     SPIPE
  MW
            BAP222
                       MMBDMMT
                                   COMAN
                                              COM624
                                                          STANCE
                                                                     DL42
  DDLUG
            CASDBAR
                       POPPA
                                              CIP
                                   AIS
                                                          CTORC
                                                                     PLTDL42
  CSS AMALYSIS
                  CDC PROGRAMS-
            CD2000
  DIS
                                   UNIPLOT
                       EDL
                                              GTSTRUDL
                                                         STARDYNE
  BASEPLATE II
 ALL USERS MUST OBTAIN CONTROLLED DOCUMENTATION FOR THE ABOVE PROGRAMS
 BEFORE USING THEM. FOR MORE INFO CONTACT THE COMPUTER SERVICES STAFF.
 READY.
DLD:RDP30
 READY.
200 -86,-37,-60,-26,123,35,27,0,0
210 -118.5,-46.5,-86,-25,135,0,35,0,0
220 -86,-25,-58,-25,135,0,35,0,0
230 -60,-26,-58,-25,123,35,27,0,0
240 -58,-25,-8,0,123,0,27,0,0
390 20,20,100,100,10,10,10
420 25,5,120,100,10,10,10
REPLACE
 READY.
FTH
 READY.
                            Ripsup 10 wide @ Channel Bottom to El. 1080
OLD, SLOPE2
 READY
GET. TAPE5=RDP30
 READY.
RUN
 84/07/21. 09.57.36.
ROGRAM SLOPE2
PROGRAM.
110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75
 (ERQF=
               . 05
                        DEPTH OF ROCK=
                                            49.0 FT)
                  THESE ARE THE IMPUT DATA LINES
     \times 1
              Υ1
                       X2
                                Y2
                                                           F1
                                                                     C2
                                                                             C1
 -9399.0
            -49.0
                    -122.0
                              -49.0 -1000.0
                                                   0.0
                                                         100.0
                                                                     0.0
                                                                          9999.0
  -122.0
            -49.0
                              -49.0 -1000.0
                    -112.0
                                                  35.0
                                                                          9999.0
                                                         100.0
                                                                     0.0
                              -49.0 -1000.0
  -112.0
            -49.0
                    9399.0
                                                 25.0
                                                         100.0
                                                                     0.0
                                                                          9999.0
 -9399.0
                    -118.5
            -46.5
                              -46.5
                                       -62.4
                                                  0.0
                                                           0.0
                                                                     0.0
                                                                              0.0
                                      -135.0
                                                           35.0
  -118.5
            -46.5
                    -110.0
                              -46.5
                                                 35.0
                                                                     Û. Û
                                                                              0.0
            -49.0
  -112.0
                   -110.0
                              -46.5
                                      -128.0
                                                 35.0
                                                          25.0
                                                                     0.0
                                                                              0.0
                                                 35.0
                    -105.5
  -110.0
            -46.5
                              -41.5
                                       125.0
                                                           25.0
                                                                     0.0
                                                                              0.0
  -1.05.5
            -41.5
                    -100.0
                                                                     0.0
                              -39.5
                                       125.0
                                                 35.0
                                                          25.0
                                                                              0.0
  -100.0
            -39.5
                              -37.0
                                                 35.0
                    -86.0
                                       125.0
                                                          25.0
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                                                                              Ũ.Ũ
                    -60.0
   -86.0
            -37.0
                              -26.0
                                       123.0
                                                 35.0
                                                          27.0
                                                                     0.0
                                                                              0.0
  -122.0
            -49.0
                   -118.5
                              -46.5
                                      -135.0
                                                  0.0
                                                           35.0
                                                                     0.0
                                                                              0.0
                                                           35.0
                                                                              0.0
                                      135.0
                                                                     0.0
  -118.5
            -46.5
                     -86.0
                              -25.0
                                                  0.0
                     -58.0
            -25.0
                                       135.0
                                                  0.0
                                                          35.0
                                                                     0.0
                                                                              0.0
   -86.0
                              -25.0
                              -25.0
                                                 35.0
                                                          27.0
                                                                     0.0
                                                                              0.0
   -60.0
            -26.0
                     -58.0
                                       123.0
                                                          27.0
            -25.0
                                                  0.0
                                                                     0.0
                                                                              0.0
   -58.0
                      -8.0
                                0.0
                                       123.0
              0.0
                       8.0
                                                          27.0
    -8.0
                                       123.0
                                                   0.0
                                                                     0.0
                                                                              0.0
                                0.0
     8.0
                      16.0
              0.0
                               -4.0
                                      123.0
                                                  0.0
                                                          27.0
                                                                     0.0
                                                                              0.0
    16.0
             -4.0
                      78.0
                              -35.0
                                      -127.0
                                                  0.0
                                                          27.0
                                                                     0.0
                                                                              Ŭ. O
    78.0
            -35.0
                      84.0
                              -38.0
                                      -128.0
                                                 27.0
                                                          25.0
                                                                     0.0
                                                                              0.0
            -38.0
                   9399.0
                              -38.0
                                     -128.0
    84.0
                                                 27.0
                                                          25.0
                                                                     0.0
                                                                              0.0
    78.0
            -35.0
                    9399.0
                              -35.0
                                     -127.0
                                                  0.0
                                                          27.0
                                                                     0.0
                                                                              0.0
    16.0
            -4.0
                    9399.0
                                                  0.0
                                                          0.0
                                                                     0.0
                                                                              0.0
            -37.0
   -86.0
                     -85.0
                              -37.0
                                                          25.0
                                      125.0
                                                 27.0
                                                                     0.0
                                                                              0.0
```

XT= 8.0 YT= -5.0 XB= -40.0 YB= -35.0

-35.0

-35.0

-37.0

GRIDX= 20.0 GRIDY= 20.0 XMAX= 100.0 YMAX= 100.0

-4.0 -127.0

-128.0

-128.0

-128.0

27.0

27.0

25.0

27.0

25.0

25.0

25.0

27.0

0.0

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0.0

INCX= 10 INCY= 10 INCR= 10

-37.0

-35.0

-37.0

-46.5

-82.0

-110.0

-82.0

5.0

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

5.0

78.0

-82.0

16.0

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.09 EFS= .87 H(X)= 80.00 G(Y)= 70.00 R= 103.98 THE MIN. EFS= .87 FS= 1.09 H(X)= 80.00 G(Y)= 70.00 R= 103.98

FOR SIDE TWO

122.0 -49.0 112.0 -49.0 -1000.0 35.0 100.0 0.0 99 112.0 -49.0 -9399.0 -49.0 -1000.0 25.0 100.0 0.0 99	
9399.0	999.0 999.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

XT = 8.0 YT = -5.0 XB = -70.0 YB = -45.0

GRIDX= 25.0 GRIDY= 5.0 XMAX= 120.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

Shallow Failure

THE MIN. FS= 1.04 EFS= .91 H(X)= 45.00 G(Y)= 15.00 R= 42.07 MIN. EFS= .90 FS= 1.05 H(X)= 45.00 G(Y)= 5.00 R= 38.34 77.389 UNTS.

FLETE.

OLD, RDP30 READY. 380 8,-2,-40,-35 410 80,-27,80,-52 420 50,0,125,100,10,10,5 REPLACE READY. OLD:SLOPE2 READY. FTH READY. GET, TAPE5=RDP30 READY. RUN 84/07/21. 10.13.06. PROGRAM SLOPE2 110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 . 05 DEPTH OF ROCK= 49.0 FT) (ERQF=

THESE ARE THE INPUT DATA LINES

×1	Y1	X2	YE	l, l	F2	F1	C2	C1
-9399.0	-49.N	-122.0	-49 ₋ 0	-1000.0	0.0	100.0	0.0	9999.0
-122.0	-49.0	-112.0		-1000.0	35.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0		-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-118.5	-46.5	-62.4	0.0	0.0	0.0	0.0
-118.5	-46.5	-110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	35.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	125.0	35.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	125.0	35.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	125.0	35.0	25.0	Ū.Ū	0.0
-86.0	-37.0	-60.0	-26.0	123.0	35.0	27.0	0.0	0.0
-122.0	-49.0	-118.5	-46.5	-135.0	0.0	35.0	Ũ. Ũ	0,0
-118.5	-46.5	-86.0	-25.0	135.0	0.0	35.0	0.0	0.0
-86.0	-25.0	-58.0	-25.0	135.0	0:0	35.0	0.0	0.0
-60.0	-26.0	-58.0	-25.0	123.0	35.0	27.0	0.0	0.0
-58.0	-25.0	-8.0	0.O	123.0	0.0	27.0	0.0	0.0
-8.0	0.0	8.0	0.0	123.0	0.0	27.0	0.0	0.0
8.0	0.0	16.0	-4.0	123.0	0.0	27.0	0.0	0.0
16.0	-4.0	78.0	-35.0	-127.0	0.0	27.0.	0.0	0.0
78.0	-35.0	84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
8 4. Û	-38.0	9399.0	-38.0	-128.0	27.0	25.0	0.0	0.0
78.0	-35.0	9399.0	-35.0	-127.0	0.0	27.0	0.0	0,0
16.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	$0 \downarrow 0$	0.0
-86.0	-37.0	-82.0	-37.0	125.0	27.0	25.0	0.0	0.0
-82.0	-37.N	5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	78.Õ	-35.0	-128.0	27.0	25.0	0.0	Ũ"Ũ
-110.0	-46.5	-82.0	-37.0	-128.0	25.0	25.0	0.0	0.0
-88.0	-37.0	16.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 8.0 YT= -2.0 XB= -40.0 YB= -35.0

GRIDX= 20.0 GRIDY= 20.0 XMAX= 100.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

shallow Failure THE MIN. FS= 1.06 EFS= .88 H(X)= 30.00 G(Y)= 20.00 R= 31.12 THE MIN. EFS= .86 FS= 1.06 H(X)= 60.00 G(Y)= 50.00 R= 73.55

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

Χ1	Y1	X 2	4,5	(_t)	F2	F1	CB	C1
9399.0	-49.0	122.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
122.0	-49.0	-112.0		-1000.0	35.0	100.0	0.0	9999.0
-112.0	-49.0	-9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
9399.0	-46.5	118.5	-46.5	-62.4	0.0	0.0	0.0	0.0
118.5	-46.5	110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
112.0	-49.0	110.0	-46.5	-128.0	35.0	25.0	0.0	Õ.Õ
110.0	-46.5	105.5	-41.5	125.0	35.0	25.0	0.0	0.07
105.5	-41.5	100.0	-39.5	125.0	35.0	25.0	0.0	0.02
100.0	-39.5	86.U	-37.0	125.0	35.0	25.0	0.0	0.0
86.0	-37.0	60.0	-26.0	123.0	35.0	27.0	0.0	ō.o.
122.0	-49.0	118.5	-46.5	-135.0	0.0	35.0	0.0	0.0
118.5	-46.5	86.0	-25.0	135.0	O.O	35.0	0.0	0.0
86.0	-25.0	58.0	-25.0	135.0	0.0	35.0	0.0	0.0
60.0	-26.0	58.0	-25.0	123.0	35.0	27.0	0.0	0.07-
58.0	-25.0	8.0	0.0	123.0	O.O	27.0	0.0	0.0%
8.0	0.0	-8.0	0.0	123.0	0.0	27.0	0.0	0.0
-8.0	0.0	-16.0	-4.Û	123.0	0.0	27.0	0.0	0.0
-16.0	-4.0	-78.0	-35.0	-127.0	O.O	27.0	0.0	0.0
-78.0	-35.0	-84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
-84.0	-38.0	-9399.0	-38.0	-128.0	27.0	25.0	0.0	0. 0
-78.0	-35.0	-9399.0	-35.0	-127.0	0.0	27.0	0.0	0.00
-16.0	-4.0	-9399.0	-4. D	-62.4	0.0	0.0	0.0	0.0
86.0	-37.0	82.O	-37.0	125.0	27.0	25.0	0.0	0.0
82. 0	-37:0	-5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
-5.0	-35.0	-78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
110.0	-46.5	82.0	-37.0	-128.0	25.0	25.0	0.0	0.0
82.0	-37.0	-16.0	-4.0	-127.0	27.0	27.0	0.0	0.0 5
				*				

XT= 80.0 YT= -27.0 XB= 80.0 YB= -52.0

GRIDX= 50.0 GRIDY= 0.0 XMAX= 125.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS Love Stope Failure
Mostly in Riphap

THE MIN. FS= .97 EFS= .86 H(X) = 120.00 G(Y) = .10 R= 48.27

THE MIN. EFS= .86 FS= .97 $H(\vec{X})$ = 120.00 $G(\vec{Y})$ = .10 R= 48.27

SBU 107.034 UNTS.

RUN COMPLETE.

1 3

OLD, RDP30 READY. 420 80,50,130,120,10,10,5 REPLACE READY. HTT READY. OLD, SLOPE2 READY. GET.TAPE5=RDP30 PEADY. RUN

-84/07/21. 10.44.47. PROGRAM SLOPE2

110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 DEFTH OF ROCK= 49.0 FT) .05 (EROF=

THESE ARE THE INPUT DATA LINES

$\times 1$	Y1	XS	Y2	l _s J	F2	F1	CB	C 1
-9399.0	-49.0	-122.0	-49.0	-1000.0	0.0	100.0	0.0	9999.0
-122.0	-49.0	-112.0	-49.0	-1000.0	35.0	100.0	0.0	9999.0
-112.0	-49.0	9399.0	-49.0	-1000.0	25.0	100.0	0.0	9999.0
-9399.0	-46.5	-118.5	-46.5	-62.4	0.0	0.0	0.0	0.0
-118.5	-46.5	-110.0	-46.5	-135.0	35.0	35.0	0.0	0.0
-112.0	-49.0	-110.0	-46.5	-128.0	35.0	25.0	0.0	0.0
-110.0	-46.5	-105.5	-41.5	125.0	35.0	25.0	0.0	0.0
-105.5	-41.5	-100.0	-39.5	125.0	35.0	25.0	0.0	0.0
-100.0	-39.5	-86.0	-37.0	125.0	35.0	25.0	0.0	0.0
-86.0	-37.0	-60.0	-26.0	123.0	35.0	27.0	0.0	0.0
-122.0	-49.0	-118.5	-46.5	-135.0	0.0	35.0	0.0	0.0
-118.5	-46.5	-86.0	-25.0	135.0	0.0	35.0	0.0	0.0
-86.0	-25.0	-58.0	-25.0	135.0	0.0	35.0	0.0	0.0
-60.0	-26.0	-5g.O	-25.O	123.0	35.0	27.0	0.0	0.0
-58.0 -8.0	-25.0	-8.0	0.0	123.0	0.0	27.0	0.0	0.0
	0.0	8.0	Ü.Ü	123.0	0.0	27.0	0. O	0.0
8.0	Ü. Ü	16.0	-4.O	123.0	0.0	27.0	0.0	0.0
16.0	-4.0	78.0	-35.0	-127.0	0.0	27.0	ō.ŏ	0.0
78.0	-35.0	84.0	-38.0	-128.0	27.0	25.0	0.0	0.0
84.0	-38.0	9399.0	-38.0	-128.0	27.0	25.0	0.0	0.0
78.0	-35.0	9399.0	-35.0	-127.0	0.0	27.0	0.0	0.0
16.0	-4.0	9399.0	-4.0	-62.4	0.0	0.0	0.0	0.0
-86.0	-37.0	-82.0	-37.0	125.0	27.0	25.0	0.0	0.0
-82.0	-37.0	_5.0	-35 . 0	-128.0	27.0	25.0	0.0	0.0
5.0	-35.0	78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
-110.0	-46.5	-82.0	-37.0	-128.0	25.Ü	25.0	0.0	0.0
-82.0	-37.0	16.0	-4.0	-127.0	27.0	27.0	0.0	0.0

 $\times T =$ 8.0 YT= -5.0 XB= −40.0 YB = -35.0

GRIDX= 50.0 GRIDY= 50.0 XMAX= 100.0 YMAX= 100.0

1.09

IMCX= 10INCY= 10 IMCR= 10

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.09 EFS= H(X) = 80.00.87 G(Y) = 70.00R= 103.98 .87 THE MIN. EFS= FS=

H(X) = 80.00

G(Y) = 70.00

R = 103.98

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

×1	Y1	X2	Y2	W	FB	F1	CB	C1
9399.0	-49.0		-49.Ü	-1000.0	0.0	100.0	0.0	9999.0
122.0	-49.0		-49.0	-1000.0	35.0	100.0	0.0	9999.0
112.0	-49.0		-49.0	-1000.0	25.0	100.0	Ũ.O	9999.0
9399.0	-46.5	118.5	-46.5	-62.4	0.0	0.0	Û.Ü	0.0
118.5	-46.5		-46.5	-135.0	35.0	35.0	0.0	0.0
112.0	-49.0		-46.5	-128.0	35.0	25.0	0.0	0.0
110.0	-46.5		-41.5	125.0	35.0	25.0	0.0	0.0
105.5	-41.5		-39.5	125.0	35.0	25.0	0.0	Ō, Ō
100.0	-39.5		-37.0	125.0	35.0	25.0	û. Ô	0.0
.86.0	-37.0		-26.0	123.0	35.0	27.0	0.0	0.0
122.0	-49.0		-46.5	-135.0	0.0	35.0	0.0	0.0
118.5	-46.5	86.0	-25.0	135.0	0.0	35.0	0.0	0.0
86.0	-25.0		-25 . 0	135.0	0.0	35.0	0.0	0.0
60.0	-26.0	58.0	-25.0	123.0	35.0	27.0	0.0	0.0
58.0 8.0	-25.0	§. Ū	0.0	123.0	Ü.O	27.0	0.0	0.0
-8.0	0.0		0.0	123.0	0.0	27.0	0.0	0.0
-16.0	0.0 -4.0	-16.0	-4.0	123.0	0.0	27.0	0.0	0.0
-78.0	-35.0	-78.0	-35.0	-127.0	0.0	27.0	Û. Û	0.0
-84.0			-38.0	-128.0	27.0	25.0	0.0	0.0
-78.0	-35.0		-38.0	-128.0	27.0	25.0	0.0	0.0
-16.0		-9399.0 -9399.0	-35.0	-127.0	Ü. Ü	27.0	0.0	0.0
86.0	-37.0		-4.0	-62.4	0.0	0.0	0.0	ů. á
82.0	-37.0	82.O	-37.0	125.0	27.0	25.0	0.0	0.0
-5.0	-35.0	-5.0	-35.0	-128.0	27.0	25.0	0.0	0.0
110.0	-46.5	-78.0	-35.0	-128.0	27.0	25.0	0.0	0.0
82.0	-37.0	82.0	-37.0	-128.0	25.0	25.0	0.0	Ō.Ō
with a U	. Tores	-16.0	-4.0	-127.0	27.0	27.0	0.0	0.0

XT= 80.0 YT= -27.0 XB= 80.0 YB= -52.0

GRIDX= 80.0 GRIDY= 50.0 XMAX= 130.0 YMAX= 120.0

INCX= 10 INCY= 10 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

· Deep Failure in Fall Dite

THE MIN. FS= 1.06 EFS= .90 H(X)= 100.00 G(Y)= 80.00 R= 128.87 THE MIN. EFS= .90 FS= 1.06 H(X)= 100.00 G(Y)= 80.00 R= 17

SBU 51.771 UNTS.

RUM COMPLETE.

Riprop to El. 1080 pROGRAM²¹.slope2.23. 110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 (EROF= .05 DEPTH OF ROCK= 49.0 FT) THESE ARE THE INPUT DATA LINES W SY W F2 F1 C2 $\mathbb{C} 1$ YT = -10.0 XB = -40.0 YB = -35.0XT= 8.0 GRIDX= 50.0 GRIDY= 50.0 XMAX= 100.0 YMAX= 100.0 INCX= 10 INCY= 10 INCR= 10 THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00 TEST POINTS THE MIN. EFS= .90 FS= 1.14 H(X)= 70.00 G(Y)= 50.00 R= 86.29FOR SIDE TWO

THE MIN. FS = 1.14 EFS = .90 H(X) = 70.00 G(Y) = 50.00 R = 86.29

	Т	HESE ARE	THE IMP	UT DATA L	INES			
×1	Υ1	X2	Y2	W	F2	F1	C2	C1
00000000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000		MANNON WO WO WOW WAS ALLOWED WAS ALLOWED WAS A LONG OF THE WAS A L	TITE TO COUNTY TO COUNTY COUNT		999 999
XT= 80.0		T = -27.0	×B	= 80.0	A.B=	-52.0		
		GRIDY=	20.0	= XMAX=	100.0	YMAX=	100.]
INCX= 10	INC		INCR=	5				
THE MAXIMU			INTED I					
THE MAXIMU	JM E.F.	S. TO BE	PRINTED	IS 0.	Ū Ū			

TEST POINTS

THE MIN. FS= 1.14 EFS= .95 H(X)= 70.00 G(Y)= 40.00 R= 87.75THE MIN. EFS= .95 FS= 1.14 H(X)= 70.00 G(Y)= 40.00 R= 87.75 SBU 78.690 UNTS. RUN COMPLETE.

READY. TN. 17 WEADY. _D, SLOPE2 READY. ET, TAPE5=RDP30 READY.

Riprep to El. 1000 10' Beam @ Toe to El. 1065

34/07/27. 10.16.29. ROGRAM SLOPE2

10 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 (ERQF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

	TH	HESE ARE I	HE THE	at municipat	1 have feet				
×1	Y1	X2	Y2	. W	F2	F1	ca e	C1	
-939.0 -132.0 -112.0 -9399.0 -112.0 -9399.0 -128.5 -110.0 -105.5 -100.0 -128.5 -107.0 -107.0 -86.0 -86.0 -88.0	00005500555005000000000000000000000000	-132.0 -112.0 9399.0 -128.5 -110.0 -105.0 -100.0 -105.0 -60.5 -107.0 -88.0 -128.0 -58.0 -58.0 -58.0 -78.0 9399.0 9399.0 9399.0 -82.0 -86.0 -86.0	-49.0	-1000.0 -1000.0 -1000.0 -62.4 -135.0 -125.0 125.0 125.0 135.0 135.0 135.0 133.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0 123.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	100.0 100.0 100.0 0.0 0.0 0.0 35.0 35.0 25.0 25.0 25.0 25.0 27.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25		9999.0 9999.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	
XT= 8.	. 0 ' \	/T= -10.0) XI	B = -40.0	YE=	-35.0°			
GRIDX=	50.0	GRIDY=	25.0	XMAX=	100.0	YMAX=	75.	0	
INCX= 10	INC	CY= 10	INCR=	10					
		. TO BE PF	RINTED	IS 0.00		* **			
				D IS 0.	0.0				
1 1 1 mm 1 11 11 11 11 11 11 11 11 11 11									

TEST POINTS

THE 1	MIN.	FS=	1.15	EFS=	.91	H (X) =	70.00	6 (Y) =	45.00	₽=	82.89
TUE 1	m T N	FFS=	.91	FS=	1.15	H (%) =	70.00	G (Y') =	45.00	R=	82.89

×1	Υ1	X2	Y2	M	F2	F ₁	C2	C 1
9399.0 132.0 9399.0 128.5 112.0 100.0 105.5 100.0 138.5 117.0 107.0 86.0 107.0 107.0 86.0 107.0 107.0 86.0 110.0 82.0 110.0 82.0 110.0 82.0	-35.0	132.0 112.0 -9399.0 128.5 110.0 105.5 100.0 60.0 128.5 117.0 107.0 86.0 -8.0 -78.0 -8.0 -9399.0 -9399.0 -9399.0 -9399.0 -9399.0 -9399.0 -16.0 -78.0 -78.0 -78.0 -78.0 -78.0 -78.0 -78.0 -78.0 -78.0	-49.0	-1000.0 -1000.0 -1000.0 -1000.0 -1000.0 -135.0 -125.0 -125.0 -135.0 -135.0 -135.0 -135.0 -135.0 -123.0	0.000000000000000000000000000000000000	100.0 100.0 100.0 0.0 0.0 0.0 0.0 0.0 0.	0.0 9	
XT= 115.	.0 Y	T = -41.0	ΧB	= 115.0	Y'E=	-51.0		
GRIDX=	50.0	GRIDY=	0.0	XMAX=	120.0	YMAX=	100.0	
INCX= 10	INC	Y= 10	INCR=	5				
THE MAXI	MUM F.S.	TO BE PRI	I datm	0.00				

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

97.51 .96 (H(X)= 80.00 G(Y) =50.00 THE MIN. FS= 1.15 EFS= R = 97.5150.00 FS= 1.15 H(X) = 80.00G(Y) =THE MIN. EFS= .96 35.125 UNTS. 3BU

RUN COMPLETE.

TERMINAL 21 TIME OUT.

IAF CONNECT TIME 01.09.48. -OGGED DUT. -x78:

CREDIT 3.1.00
2102-128.5,-46.5;-117:-39,135,0,35,0,0
2102-128.5,-346.5;-117:-35,135,0,35,0,0
2102-17:5,-346.5;-117:-35,135,0,35,0,0
2122-17:7,-39:-107:-39:135;0,35;0,0
2122-17:7,-35;-101;-35;135;0;35;0,0
2142-17:7,-39:-86:725;135;0,35;0,0
2142-17:7;-36;-86:725;135;0,35;0,0
2142-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-36;-86:725;135;0,35;0,0
2140-17:7;-86:75;135;0,35;0,0
2140-17:7;-86:75;135;0,35;0,0
2140-17:7;-86:75;135;0,35;0,0
2140-17:7;-86:75;135;0,35;0,0
2140-17:7;-86:75;135;0,35;0,0
2140-17:7;-86:75;135;0,35;0,0
2140-17:7;-86:75;135;0,35;0,0
2140-17:7;-86:75;135;0,0
2140-17:7;-86:75;135;0,0
2140-17:7;-86:75;136;0,0
2140-17:7;-86:75;136;0,0
2140-17:7;-86:75;136;0,0
2140-17:7;-86:75;136;0,0
2140-17:7;-86:75;136;0,0
2140-17:7;-86:75;136;0 FIR OLDY DEPANY GETATHPES=RDP30 READY. PUN PROGRAM SLOPES.08. 110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 (EROF= .05 DEPTH OF ROCK= 49.0 FT) THESE ARE THE INPUT DATA LINES F1 F2 X2 Υ2 Y1 9999.0 9999.0 9999.0 0.0 0.0 100.0 -110:0 -12:0 -82:0 YT = -10.0 XB = -40.0YB= -35.0 XT= 8.0 GRIDX= 50.0 GRIDY= 50.0 XMAX= 100.0 YMAX= 100.0 INCX= 10 INCY= 10 INCR= 10 THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS: 0.00 TEST POINTS EFS= $.90 \cdot H(X) = .70.00 \cdot G(Y) = .50.00$ THE MIN. FS= 1.14 $FS = 1.14 \quad H(X) = 70.00 \quad G(Y) = 50.00$ R= 86.29 THE MIN. EFS= .90 FOR SIDE TWO

	THESE ARE	THE IMPUT	DATA LI	MES			
X1 Y1	X2	Ye	· Id	FZ	F1	C2	C1
97 97 97 97 97 97 97 97 97 97 97 97 97 9		11111111111111111111111111111111111111		MUNDONO O O OU NOUNDONO O OO OOOOOOOOOOOO	00000000000000000000000000000000000000		999 999 999
XT= 80.0	YT= -27.0		80.0 XMAX=	YB= 100.0	-52.0 YMAX=	100.	· 1
GRIDX= 20.0	GRIDY=	20.0	APIDA-	100.0	1111117	1	u ⁺

TEST POINTS

THE MAXIMUM E.F.S. TO BE PRINTED IS

INCX= 10 INCY= 10 INCR= 5
THE MAXIMUM F.S. TO BE PRINTED IS

THE MIN. FS= 1.17 EFS= .99 H(X)= 50.00 G(Y)= 20.00 R= 55.77

THE MIN. EFS= .99 FS= 1.17 H(X)= 50.00 G(Y)= 20.00 R= 55.77

SBU 77.616 UNTS.

RUN COMPLETE.

0.00

0.00

A/07/25. 10.17.16. AA3C5DA HOLY: *TVA* CHATTANOOGA,TN. BOTLY: KVA SEC NAME: KXFDPDC ALSUNDA BERNAME. SEC NAMIAE NOS 1.4/531.462/2AB TERMINOL:
RECUVER: CHORGE: CHARLESSOIPE: CD2*JSE
RECUVER: ***** ATTENTION INTERACTIVE USERS *****
IF YOU ARE EXPERIENCING VERY SLOW RESPONSE TIME AT CONSISTENTLY GREATER
THAN 15 SECONDS, PLEASE REMAIN ON LINE AND CALL THE COMPUTER SERVICES
STAFF AT #2383, KNOXVILLE. KNOWING YOUR TTY NUMBER WOULD BE USEFUL.
REMAIN ON-LINE!!!!!!! THE FOLLOWING IS A LIST OF THE PROGRAMS AVAILABLE ON KVA WHICH HAVE BEEN VALIDATED FOR SAFETY-RELATED ANALYSIS AND DESIGN AS REQUIRED BY ENDES EP3.23; TVA IN-HOUSE PROGRAMSBOLT EADHI TPIPE FRAMS
ANCHOR WBDATA ENVELOPE U-BOLT
MV BAP222 MNBDMNT CONAN
DDLUG CASDBAP POPPA AIS
CSS ANALYSIS GLOBAL SPECTRA COM624 CIP CASD DBASQN STANCE CTORC CDC PROGRAMSDIS CD2000 EDL UNIPLOT GTSTRUDL STARDYNE
BASEPLATE II
ALL USERS MUST OBTAIN CONTROLLED DOCUMENTATION FOR THE ABOVE PROGRAMS
BEFORE USING THEM. FOR MORE INFO CONTACT THE COMPUTER SERVICES STAFF.

READY. DLD,RDP30 READY. 390 50,25,100,75,10,10,10 410 105,-37,105,-52 420 50,10,110,100,10,10,5 REPLACE READY. FIN

READY. OLD SLOPE2 READY. GET.TAPE5=RDP30 READY. RUN

Ripsap to El. 1080 10' Beam to El. 1070

TVA WELDDA SPIPE DL42 PLTDL42

84/07/25. 10.28.30. PROGRAM SLOPE2

110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

X1	Y1	X2	Y2	W	F2	F1	02	C1
-939.0 -112.0 -9392.0 -112.0 -9398.0 -112.0 -1105.0 -1105.0 -128.0 -128.0 -128.0 -128.0 -128.0 -138.0 -141.0 -101.0 -1	99.055055005000000000000000000000000000	-132.0 -132.0 -132.0 -110.0	00055555500500000000000000000000000000	-1000.0 -1000.0 -1000.0 -1000.0 -1385.0 -1385.0 -1385.0 -1385.0 -1385.0 -1385.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0 -1388.0	0.000000000000000000000000000000000000	1000.000000000000000000000000000000000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0

XT= 8.0 YT= -10.0 XB= -40.0 YB= -35.0 GRIDX= 50.0 GRIDY= 25.0 XMAX= 100.0 YMAX= 75.0 INCX= 10 INCY= 10 INCR= 10 THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.15 EFS= .91 H(X)= 70.00° G(Y)= 45.00 R= 82.89THE MIN. EFS= .91 FS= 1.15 H(X)= 70.00 G(Y)= 45.00 R= 82.89

THESE ARE THE INPUT DA	TA LINES
IMENE HIVE THE	Fa Fi C2 Ul
Y1 XC '-	
-78.0 -9399.0 -38.0 -17.0 -84.0 -35.0 -17.0 -78.0 -35.0 -9399.0 -4.0 -78.0 -37.0 1 -4.0 -37.0 1 -37.0	
07 0 XB=	105.0 YB= −52.0
XI= 100.0	XMAX= 110.0 YMAX= 100.0
GRIDX= DU.V	
TNCV = 10 $INCV = 10$	0.00
THE MAXIMUM F.S. TO BE PRINTED 15	0.00
THE MAXIMUM E.F.S. TO BE PRINTED I	0.00

TEST POINTS

THE MIN. FS= 1.21 EFS= 1.00 H(X)= 70.00 G(Y)= 50.00 F THE MIN. EFS= 1.00 FS= 1.21 H(X)= 70.00 G(Y)= 50.00 SBU 43.403 UNTS. RUN COMPLETE.

OLD.RDP30
READY.
410 80.5; -70: -45
420 80.5; 100; 100, 10, 10, 5
REPLACE
READY.
FIN
READY.
DLD:SLOPE2
READY.
GET, TAPE5=RDP30
READY.
RUN 84/07/25. 10.41.45. PROGRAM SLOPE2

10' Beam to El 1070

110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 (EROF= .05 DEPTH OF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

	×1	٧1	XS	Y2	Ĺţ)	F2	F1	CE	C1
	990.00 990.00 990.00 990.00 900.00	00005505550050000000000000000000000000	-132.0 -132.0 -132.0 -1398.5 -110.0 -1100.0 -1100.0 -1200.0 -1211.0 -1	99966619766555555000000000000000000000000000000	-1000.0 -1000.0 -1000.0 -1000.0 -138.0 -138.0 -135.0 -135.0 -135.0 -135.0 -135.0 -135.0 -135.0 -136.	00000000000000000000000000000000000000	00000000000000000000000000000000000000		9999 0000000000000000000000000000000000
	XT= 8.(= -10.0	×B=	-40.0	YB=	-35.0		
		50.O	GRIDY=	25.0	XMAX=	100.0	YMAX=	75.0	
	IMCX= 10		'= 10	INCR= 1	. 0			E THAT HE TUT	
	THE MAXIMU	IM F.S.	TO BE PRI	NTED IS	0.00				
7	THE MAXIMU	M E.F.S	. TO BE F	FINTED	IS 0.0	Û			

TEST POINTS

THE MIN. FS= 1.15 EFS= .91 H(X) =70.00 6 (Y) = 45.00 82.89 THE MIN. EFS= .91 FS= 1.15 H(X) =70.00 G(Y) =45.00 F = 82.89

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

X1	Y1.	XS	42	W	F2	F1	02	01
939.0 132.0 9398.0 110.0 9398.0 110.0 100.0 132.0 111.0 101.	9.0055055500500000000000000000000000000	132.0.05.00.00.00.00.00.00.00.00.00.00.00.0	00055555005000000000000000000000000000	-1000.0 -1000.0 -1000.0 -138.0 -135.0 -135.0 -135.0 -135.0 -135.0 -135.0 -135.0 -135.0 -136.0	0.000000000000000000000000000000000000	00000000000000000000000000000000000000		999990000000000000000000000000000000000

XT= 8.0 YT= -5.0 XB= -70.0 YB= -45.0

GRIDX= 20.0 GRIDY= 5.0 XMAX= 100.0 YMAX= 100.0

INCX= 10 INCY= 10 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

THE MIN. FS= 1.05 EFS= .92 H(X)= 50.00 G(Y)= 25.00 R= 51.62 THE MIN. EFS= .90 FS= 1.06 H(X)= 40.00 G(Y)= 5.00 R= 38.54 SBU 89.546 UNTS. RUN COMPLETE.

```
OOL ON ONE-KBM, KXFDPDC

1.4/531.58
1.6/BERNET CENTER SN214 NOS
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
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1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
1.4/531.58
                                                                                 1.4/531.523/15AD
  ATE II HAS BEEN CORRECTED ON FAMILY
A CHATTANOOGA ALL USER'S SOON AS
NG BASEPLATE II ON KVA AS SOON AS
BLE.
   J.30. WARMING
  EXPLAIN, NUFUSAGE+EXPLAIN, NOS-PLOTTING
  T 3.1.00

19399,-49,-112,-49,-1000,0,100,0,9999

19399,-49,-122,-49,-1000,0,100,0,9999
   bP30
    50
-9399,-46,5,-110,-46.5,-62.4,0,0,0,0
-110,-118,5,-118.5,-46.5,-62.4,0,0,0,0
-9399,-46.5,-118.5
        12,-49,-110,-46.5,-128,0,25,0,150

12,-49,-110,-46.5,-128,35,25,0,150

18,-48,-110,-46.5,-125,125,35,25,0,150

10,-46.5,-100,-39.5,125,35,25,0,150

05.5,-41.5,-100,-39.5
         05.5,-41.5,-100,-32.0,125,0,0

00,-39.5,-85,-30,135,0,35,0,0

100:-36.5,-36,5,-29,135,0,35,0,0

18.5,-46.5,-29,135,0,35,0,0

35:-30,-67,-29,135,0,35,0,0

18.5,-30/-92,-29,135,0,35,0,0

18.5,-30/-92,-29,135,0,35,0,0
49
8.-5,-40,-35
20,10,100,70,5,5,5
0.0
8.-5,-70,-45
25,15,120,120,5,5,5
                                                                                                 Add 10' Riphop @ Chemiel Bottom to EL 1076
                                                                                                L= 150
          Distopes
           ÄĎŸ
T.TAPE5=RDP30
AĎY.
       84/07/13.13.43.06.
PROGRAM SLOPE2
       110 JOHN SEVIER ASH POND "J" OF ROCK TEST OF FTS
```

THESE ARE THE INPUT DATA LINES C2 C1FE F1 X2 Y2 $\times 1$ 0.00.0 100.0 0.0 0.0 150.0 0.0 0.0 0.0 0.0 Ŏ.Ŏ 150.0 0.0 150.0 150.0 150.0 150.0 150.0 YT = -5.0 XE = -40.0YB= -35.0 XT= 8.0 XMAX= 100.0 YMAX= 70.0 GRIDX= 20.0 GRIDY= 10.0 INCR= 5 INCY= 5 INCX= 5 THE MAXIMUM F.S. TO BE PRINTED IS 0.00THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00 TEST POINTS

THE MIN. FS= 1.69 EFS= 1.35 H(X)= 60.00 G(Y)= 30.00 R= 67.69 THE MIN. EFS= 1.35 FS= 1.70 H(X)= 60.00 G(Y)= 25.00 R= 65.04

FOR SIDE TWO

	THESE ARE	THE INPU	T DATA LI	NES			
×1	Y1 × X2	Y2	(J	F2	F1	C2	C 1
93.00 93.00 93.00 93.00 93.00 93.00 93.00 93.00 93.00 93.00 110 100 100 100 100 100 100 100 100	-49.0 122.0 0 1119.0 0 129.0 0 129.0 0 129.0 0 129.0 0 0 129.0 0 0 129.0 0 0 129.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000000000000000000000000000000000000	1000.0 1000.0 1000.0 1000.4 -1300.0 1000.0 1	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	100.0 100.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	9999.0 9999.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0
8,1000 86.0 82.0 -5.0 110.0 82.0	-37.0 82.0 -37.0 -5.0 -35.0 -78.0 -46.5 82.0 -37.0 -16.0	-37.0 -35.0 -357.0 -34.0	125.0 -128.0 -128.0 -128.0 -127.0	27.0 27.0 27.0 25.0 27.0	25.0 25.0 25.0 27.0	150.0 150.0 150.0 150.0 150.0	150.0 150.0 150.0 150.0 150.0
XT= 8. GRIDX= INCX= 5 THE MAXIM	0 YT= -5.0 25.0 GRIDY= INCY= 5 UM F.S. TO BE PF	15.0	XMAX= 5	YB= 120.0	-45.0 YMAX	= 120.	0
	**						

TEST POINTS

THE MIN. FS= 1.24 EFS= 1.06 H(X)= 50.00 G(Y)= 20.00 R= 58.8 THE MIN. EFS= 1.05 FS= 1.25 H(X)= 45.00 G(Y)= 15.00 R= 57/80 SBU 557.786 UNTS. RUN COMPLETE.

```
SBU 0.337 U
READY.
RDP30
ILLEGAL COMMAND.
OLD.RDP30
READY.
 370 47
380 8,-5,-40,-35
390 20,10,100,70,5,5,5
400 0,0
410 8,-5,-70,-45
420 25,15,120,120,5,5,5
430 0,0
65600
                                                          All 12 Ny cape Channel Bottom to EL 1076
    ŘĚÁDÝ.
EIM.
                                                         6=0
    RÉADY.
OLD, SLOPE2
READY.
GET, TAPE5=RDP30
READY.
RUN
    ₽84/07/13.514.05.46.
    110 JOHN SEVIER ASH POND "J", R BAR TEST & STA. 41+75
(ERQF= .05 DEPTH OF ROCK= 49.0 FT)
```

X1 9.0005005000500000000000000000000000000	TH 0005505550050000000000000000000000000	X2 -1119.00 -1110.05 -1110.05 -1100.00 -1106.00 -11966.00 -11966.00 -11966.00 -11966.00	00055555500050000000000000000000000000	T DATA LIN 1000.00	#E 000000000000000000000000000000000000	F 000000000000000000000000000000000000	0.000000000000000000000000000000000000	C1 9999.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00
XT= 8 GRIDX= INCX= 5 THE MAXI THE MAXI	20.0 IN MUM F.S		: 10.0 IMCR= PRINTED	%MAX= 5 IS 0.00	100.0	YMAX=	70.1	
IHE DUCT	Ferman I I ame II I							

TEST POINTS

THE MIN. FS= 1.09 EFS= .87 H(X)= 80.00 G(Y)= 70.00 R= 103.98 THE MIN. EFS= .87 FS= 1.09 H(X)= 80.00 G(Y)= 65.00 R= 100.43

FOR SIDE TWO

\$1	
SBU LIMIT CONTINUE OR CR KEY TO SIDE: ENTER'S TO CONTINUE OR CR KEY TO SIDE: ENTER'S TO CONTINUE OR CR KEY TO SIDE: 27.0 25.0 0.0 0.0 35.1000 25.0 0.0 0.0 82.0 -37.0 -128.0 27.0 25.0 0.0 0.0 82.0 -37.0 -35.0 -128.0 25.0 25.0 0.0 0.0 110.0 -46.5 92.0 -37.0 -127.0 27.0 27.0 0.0 82.0 -37.0 -16.0 -4.0 -127.0 27.0 27.0	ł
XT= 8.0 YT= -5.0 XB= -70.0 YB= -45.0 GRIDX= 25.0 GRIDY= 15.0 XMAX= 120.0 YMAX= 120.0 INCX= 5 INCY= 5 INCR= 5 THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00	J

TEST POINTS

THE MIN. FS= .94 EFS= .81 H(X)=50.00 G(Y)=15.00 R= 51.53 THE MIN. EFS= .81 FS= .94 H(X)=50.00 G(Y)=15.00 R= 51.53 SBU 556.688 UNTS. RUN COMPLETE.

```
1.4/531.523/15AD
       BASEPLATE II HAS BEEN CORRECTED ON FAMILY
KVA IN CHATTANOOGA. ALL USERS SHOULD START
RUNNING BASEPLATE II ON KVA AS SOON AS
POSSIBLE.
READY.
                      07.03.13. WARMING
 TYPE EXPLAIN, NOTICE+EXPLAIN, CDSN/IAF IMPACT
RCDUT, 10
READY.
DLD, RDP30
READY
DLHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75
11400 -11101 -1400 -1700 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -1000 -
EAADY.

LNH

100 2

100 2

100 0 0.100.0.99999

110 0 0.100.0.99999

110 0 0.100.0.99999

110 0 0.100.0.99999

110 0 0.100.0.99999

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110
             OLD, SLOPE2
READY.
GET, TAPE5=RDP30
READY.
RUN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          No Additional Riprap
High Phredic Surface
                  84/07/10. 14.01.48.
PROGRAM SLOPE2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           6=0
                   110 JOHN SEVIER ASH POND "J", R BAR TEST & STA. 41+75
(EROF= .05 DEPTH OF ROCK= 49.0 FT)
```

THESE ARE THE INPUT DATA LINES $\mathbb{C}1$ CE F1 Y2 X2 Υ1 9999.0 9999.0 100.0 0.0-112.0 9399.0 -110.0 -49.00.0 99696955505000000 4444443033333 ----------25.0 0.0 -9399.0 -112.0 -9392.0 -110.0 -105.0 -106.0 Ü.O Ŏ.Ŏ Ŏ. Ō -110.0 -110.0 -105.5 -100.0 -87.0 -87.0 -87.0 0.000 0.000 0.000 0.000 0.000 0.0 0.0 0.0 Ú. O 0.0 0.0 $0 \cdot 0$ 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 27.00 27.00 27.00 27.00 27.00 27.00 0.00.00.0 -110.0-82.0 -35.0 YB =XB = -40.0-5.0 Y'T= 8.0 XT =75.0 YMAX= XMAX= 100.0 5.0GRIDY= GRIDX= 20.0 INCR= 5 IMCY= 5 INCX= 5 THE MAXIMUM F.S. TO BE PRINTED IS 0.00THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

SBU LIMIT ENTER \$ TO CONTINUE OR CR KEY TO STOP: S,1000

THE MIN. FS= 1.09 EFS= .87 H(X)= 80.00 G(Y)= 70.00 R= 103.98 THE MIN. EFS= .87 FS= 1.09 H(X)= 80.00 G(Y)= 65.00 R= 100.43

FOR SIDE TWO

	THESE ARE T	HE INPUT DA	TA LIMES			
×1 Y1		Y2 W	F2	F1	cs c	
93120.00 -449.00 -449.00 -449.00 -449.00 -449.00 -449.00 -458.	112.0 -9399.0 -9310.0 1105.0 1105.0 105.0	-49.000000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	######################################
XT= 8.0 GRIDX= 25.0 INCX= 5	YT= -5.0 GRIDY= INCY= 5		70.0 YB= (MAX= 120.0		120.0	
THE MAXIMUM F		INTED IS	0.00 0.00			
THE MAXIMUM E	.F.S. TO BE	EKTUIED 12	0.00			

TEST POINTS

THE MIN. FS= .86 EFS= .74 H(X)= 100.00 G(Y)= 70.00 R= 118.71

THE MIN. EFS= .74 FS= .86 H(X)= 95.00 G(Y)= 60.00 R= 108.61

TRU 518.930 UNTS.

(COMPLETE.

OFD.RDP30
READY.-10,-40,-35,5,5,5
380 8.-10,-40,-35,5,5,5
380 50,50,125,100,5,5,5
410 8.-10,-70,-45
420 50,30,130,120,5,5,5
READY.
READY.
READY. RÉADY OLD,SLOPE2 READY GET,TAPE5=RDP30 READY. LONER FIRST TEST Point for Side 1 & Side 2 84/07/10. 14.17.35. PROGRAM SLOPE2 110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. 41+75 (ERQF= .05 DEPTH OF ROCK= 49.0 FT) (ĔŖŎĔ= THESE ARE THE INPUT DATA LINES C1F1 Y2 X2 $\times 1$ 9999.0 25.0 0.0 9999.O -112.0 9395.0 -110.0 9399.0 -112.0 -9399.0 -112.0 0.0 Q.Q Q.Q -110.0 -110.0 -105.0 -106.0 -667.5 -687.0 -647.0 Ŏ. Ō Ō. Ō -110.0 -105.5 -100.0 -86.Ü 100.0 16.0 78.0 84.0 9399.0 9399.0 000000000 37.0555557 20.000000 0.0 ā.0 5.0 -128.0 -127.0 -9<u>2.</u>0 -110.0 16.0 YT = -10.0 XB = -40.0 YB = -35.08.0 XMAX= 125.0 YMAX= 100.0 XT= 50.0 GRIDY= 50.0 GRIDX= INCR= 5 INCY= 5 INCX= 5 THE MAXIMUM F.S. TO BE PRINTED IS THE MAXIMUM E.F.S. TO BE PRINTED IS TEST POINTS R= 86.29 6(Y) = -50.00H(X) = 70.00.90 EFS= THE MIN. FS= 1.14 R= 86.29 6(Y) = 50.00H(X) = 70.001.14 THE MIN. EFS= .90 FS= FOR SIDE TWO THESE ARE THE INPUT DATA LINES C102 F1 FΞ X2 $\forall 1$ $\times 1$ -49.0 -1000.0 9999.0 100.0 0.0-1000.0 -1000.0 -1000.0 -1000.0 -1200.0 -1200.0 -1200.0 -1200.0 -1200.0 -1200.0 -1200.0 -1200.0 -1200.0 -1200.0 Ŏ.Ŏ 25.0 0.0 0.0 9399.0 0.0 0.0 0.0 Ŏ.Ŏ **0.**0 YB= −45.0 XT = 8.0 YT = -10.0 XB = -70.0GRIDX= 50.0 GRIDY= 30.0 XMAX= 130.0 YMAX= 120.0 INCR= 5 INCY= 5 INCX= 5 THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00 TEST POINTS

SBU LIMIT ENTER S TO CONTINUE OR CR KEY TO STOP: S:1000

THE MIN. FS= .86 EFS= .74 H(X) = 100.00 G(Y) = 80.00 R= 128.71

THE MIN. EFS= .74 FS= .86 H(X) = 100.00 G(Y) = 80.00 R= 128.71

SBU 227.820 UNTS.

RUN COMPLETE.

Din.RDP30 READY. 100 40.10.120.80.5.5.5 REPLACE READY. FIN READY. OLD,SLOPE2 READY. GET.TAPE5=RDP30 READY. READY.

84/07/10.14.27.57. PROGRAM SLOPE2 Lower Test Window on Side 1

110 JOHN SEVIER ASH POND "J", R BAR TEST & STA. 41+75 (EROF= .05 DEPTH DF ROCK= 49.0 FT)

THESE ARE THE INPUT DATA LINES

X1	Y1	ΧŻ	Y2	Ы	F2	F1	02 .	C1
-91990.00 -91990.00 -919910.00 -11050.00 -11050.00 -11050.00 -110666.00 -110666.00 -10666.00 -10666.00 -10666.00 -10666.00 -10666.00 -10666.00 -10666.00 -10666.00	00505550000000000000000000000000000000	00005000000000000000000000000000000000	00555500000000000000000000000000000000	00400000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000		99 99 99 99
XT= 8.	. 0 Y	T= -10.0	XB=	-40.0	YB=	-35.0		
GRIDX=	40.0	GRIDY=	10.0	XMAX=	120.0	YMAX=	80.0	l
INCX= 5	INC	:Y= 5	INCR=	5				
THE MAXI	MUM F.S.	TO BE FRO	INTED IS	0.00				

TEST POINTS

THE MAXIMUM E.F.S. TO BE PRINTED IS

H(X) = 70.0050.00 R= 86.29 G(Y) =THE MIN. FS= 1.14 EFS= .90 72.63 G(Y) = 35.00H(X) =THE MIN. EFS= .90 FS= 1.14 65.00 114.747 UNTS. SBU RUN COMPLETE.

```
#EI-038001

PEI-038001

PEI-03
              BASEPLATE II HAS BEEN CORRECTED ON FAMILY KYA IN CHATTANOOGA ALL USERS SHOULD START RUNNING BASEPLATE 11 DN KVA AS SOON AS POSSIBLE. READY.
06.07.14. WARNING

7.11 PLS TYPE EXPLAIN, NJFUSAGE

7.12 PLS TYPE EXPLAIN, NJFUSAGE

7.13 PLS TYPE EXPLAIN, NJFUSAGE

7.14 PLS TYPE EXPLAIN, NJFUSAGE

7.15 PLS TYPE EXPLAIN, NJFUSAGE

7.16 PLS TYPE EXPLAIN, NJFUSAGE

7.17 PLS TYPE EXPLAIN, NJFUSAGE

7.18 PLS TYPE EXPLAIN, NJFUSAGE

7.19 PLS TYPE EXPLAIN, NJFUSAGE

7.10 PLS TYPE EXPLAIN, NJFUSAGE

7.11 PLS TYPE EXPLAIN, NJFUSAGE

7.11 PLS TYPE EXPLAIN, NJFUSAGE

7.12 PLS TYPE EXPLAIN, NJFUSAGE

7.15 PLS TYPE EXPLAIN, NJFUSAGE

7.16 PLS TYPE EXPLAIN, NJFUSAGE

7.17 PLS TYPE EXPLAIN, NJFUSAGE

7.18 PLS TYPE EXPLAIN, NJFUSAGE

7.10 PLS TYPE 
                                    06.07.14. WARNING
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   No Add trans Ripays
            84/07/11. 08.29.49.
PROGRAM SLOPE2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   C = C
```

```
TIO JOHN SEVIER ASH POND "J", R BAR TE
(EROF= .05 DEPTH OF ROCK=
                       THESE ARE THE IMPUT DATA LINES
                                                                                                    C1
                                                                                          CΞ
                                                                            F 1
                                         Y2
                                       9999.0
9999.0
0.0
                                                                           100.0
100.0
   -9399.0
-112.0
-9399.0
-112.0
-105.5
-108.0
                          -112.0
9399.0
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-100.00
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                                                                                          0.0
        5.0
    -110.0
                             16.0
                                             XB = -40.0
                                                                    λ'B=
                                                                           -35.0
                       YT = -10.0
  XT = 
         0.0
                                                                               YMAX= 80.0
                                                      XMAX≕ 120.0
  GRIDX= 40.0 GRIDY=
                                       20.0
                                        INCR= 5
                   IMCY= 5
  INCX= 5
  THE MAXIMUM F.S. TO BE PRINTED IS
  THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00
                    TEST POINTS
```

THE MIN. FS= 1.32 EFS= 1.04 H(X)= 65.00 G(Y)= 50.00 R= 88.47 THE MIN. EFS= 1.04 FS= 1.33 H(X)= 60.00 G(Y)= 35.00 R= 75.01

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

$\times 1^{\circ}$	Y1	X2	Y2	l _t l	F2	F1	C2	C1
91191000000000000000000000000000000000	-41.5 -39.5 -39.0 -30.0	139100.05000000000000000000000000000000000		-100.0 000.4 -100.0 000.4 -100.0 000.0 100	00000000000000000000000000000000000000	00000000000000000000000000000000000000		999.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.

XT= 8.0 YT= -10.0 XB= -70.0 YB= -45.0

GRIDX= 25.0 GRIDY= 25.0 XMAX= 125.0 YMAX= 100.0

INCX= 5 INCY= 5 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

+SBU LIMIT+ ENTER'S TO CONTINUE OR CR KEY TO STOP: S,1000

THE MIN. FS= 1.18 EFS= 1.02 H(X) = 100.00 G(Y) = 80.00 R = 128.71 THE MIN. EFS= 1.02 FS= 1.18 H(X) = 100.00 G(Y) = 80.00 R = 128.71 SBU 260.935 UNTS.

```
NET 038000
(LEASE SIGN ON--KBM, KXFDPDC
EASTERN CYBERNET CENTER SM214 MOS
PASSWORD
                                                                                                                                                                                                                                                                                                                               1.4/531.523/15AD
         ■顧問題問題
TERMINAL:
TERMINAL:
RECOVERY CHARGE: CHAR, A3501PE, +CD2+J3F
ENTER USER-ID (FIRST INITIAL PLUS LAST NAME)
    BASEPLATE II HAS BEEN CORRECTED ON FAMILY
KVA IN CHATTANODGA. ALL USERS SHOULD START
RUNNING BASEPLATE II ON KVA AS SOON AS
POSSIBLE.
READY.
            06.07.14. WARNING
  7/11 PLS TYPE EXPLAIN, NUFUSAGE SEADY 10 SEADY 1
XEDIT 3.1.00

? 140

40 -112,-49,9399,-49,-1000,25,100,0,9999

? W/C/100,0/100,100/

40 -112,-49,9399,-49,-1000.25,100,100,9999

? MJ3HM160

50 -112,-49,-110,-46.5,-128,0,25,0,0
160
T 038000
EASE SIGH DM--KBM, KXFDPDC
4/07/11. 13.41.23.
STERH CYBERNET CENTER SM214 NDS
SSWORD
                                                                                                                                                                                                                                                                                                    1.4/531.523/15AD
 爾爾爾爾爾爾

RMINAL:

COVER/ CHARGE: CHAR, A3501PE, ◆CD2+JSF

EMTER USER-ID (FIRST INITIAL PLUS LAST MAME)

RPOWELL
 ISEPLATE II HAS BEEN CORRECTED ON FAMILY
IA IN CHATTANODGA. ALL USERS SHOULD START
MMING BASEPLATE II ON KVA AS SOOM AS
   .07.14. WARNING
```

```
HI THE EXPLAIN, MUFUSAGE
               ROUT, 10
               READY
               OLD, RDP30
                                                                                                                           Enlarge Thom 6:0 To 6=150
               XEDIT
              XEDIT 3.1.00
              77 140

77 140

140 -112, -49, 9399, -49, -1000, 25, 100, 0, 9999

77 C/100, 0/100, 150/

140 -112, -49, 9399, -49, -1000, 25, 100, 150, 9999
   (f 160
160 -112,-49,-110,-46.5,-128,0,25,0,0
?? C/0,0/0,150/5
160 -112,-49,-110,-46.5,-128,0,25,0,150
170 -110,-46.5,-105.5,-41.5,125,0,25,0,150
180 -105.5,-41.5,-100,-39.5,125,0,25,0,150
190 -100,-39.5,-86,-37,125,35,25,0,150
200 -86,-37,-67,-29,123,35,27,0,150
?? 230
          270 16, -4,78,-30,-127,0,27,0,150
77 280
78,-35,84,-38,-128,27,25,0,0
77 C/0,0/150,150/2
280 78,-35,84,-38,-128,27,25,150,150
290 84,-38,9399,-38,-128,27,25,150,150
77 200
          290 84,-35,9399,-35,-128,27,25,150,

?? 300 3

300 78,-35,9399,-35,-127,0,27,0,0

?? C/0,0/0,150/

300 78,-35,9399,-35,-127,0,27,0,150
       300 78,-35,9399,-30,-12(,0,2,0),2

7? 320

320 -86,-37,-20,-35.5,125,27,25,0,0

7? C/0,0/150,150/5

320 -86,-37,-20,-35.5,125,27,25,150,150

330 -20,-35.5,5,-35,-128,27,25,150,150

340 5,-35,78,-35,-128,27,25,150,150

350 -110,-46.5,-20,-35.5,-128,25,25,150,150

360 -20,-35.5,16,-4,-127,27,27,150,150

7? Q,,RL

ILLEGAL PARAMETER
       ILLEGAL PARAMETER
?? Q,,RL
NO SUCH COMMAND
?? Q,,RL
RDP30 REPLACED
RDP30 IS A LOCAL
                                         IS A LOCAL FILE
        READY.
        OLD, RDP30
        READY.
LNH
100 2
110 JDHN SEVIER ASH PDMD "J", R BAR TEST & STA. 41+75
130 024,0.05
130 -9399,-49,-112,-49,-1000,0,100,0,9999
140 -112,-49,9399,-49,-1100,-85,100,150,9999
150 -9399,-46.5,-110,-46.5,-62.4,0,0.0,0
170 -110,-44,5,-105.5,-41.5,125,0,25,0,150
180 -105.5,-41.5,-100,-39.5,125,0,25,0,150
190 -100,-39.5,-86,-37,125,35,25,0,150
200 -86,-37,-67,-29,123,35,27,0,150
220 -85,-30,-67,-29,123,35,27,0,150
220 -85,-30,-67,-29,123,0,35,0,0
220 -85,-30,123,0,27,0,150
240 -60,-26,-8,0,123,0,27,0,150
250 -8,0,8,0,123,0,27,0,150
260 8,0,16,-4,123,0,27,0,150
270 16,-4,78,-35,-127,0,27,0,150
270 16,-4,78,-35,-127,0,27,0,150
270 16,-4,78,-35,-127,0,27,0,150
270 16,-4,78,-35,-128,27,25,150,150
370 40,-38,9399,-38,-128,27,25,150,150
310 16,-4,9399,-4,-62.4,0,0,0,0
320 -86,-37,-20,-35,5,125,27,25,150,150
330 -20,-35,5,5,-35,-128,27,25,150,150
340 5,-35,78,-35,-128,27,25,150,150
350 -10,-46.5,-20,-35.5,128,25,25,150,150
360 -20,-35.5,16,-4,-127,27,27,150,150
370 49
380 0,-10,-40,-35
390 40,20,120,80,5,5,5
       LNH
        100 2
  380 0,-10,-40,-35
390 40,20,120,80,5,5,5
  400 0.0
410 8,-10,-70,-45
420 25,25,125,100,5,5,5
 430 0,0
 READY.
YOLD:RDP30
NET 038000
PLEASE SIGN OM--KBM,KXFDPDC
```

```
NÉT 038000
PCEASE SIGN ON--KBN,KXFDPDC
      MÉT 038000
PLEASE SIGM ON--KBM.KXFDPDC
84/07/11. 14.07.12.
EASTERN CYBERNET CENTER SM214 MOS
PASSWORD
                                                                                                                              1.4/531.523/15AD
      TERMINAL: 15, TTY
RECOVER/ CHARGE: CHAR, A3501PE, *CD2*JSF
__ENTER USER-ID (FIRST INITIAL PLUS LAST NAME)
      ? RPOWELL
        BASEPLATE II HAS BEEN CORRECTED ON FAMILY
KVA IN CHATTANOOGA. ALL USERS SHOULD START
RUNNING BASEPLATE II ON KVA AS SOON AS
        POSSIBLE.
     READY.
        06.07.14. WARNING
      7/11 PLS TYPE EXPLAIN, NJFUSAGE
    ROUT.10
READY.
     DLD:RDP30
     READY.
    380 8,-5,-40,-35
REPLACE
    READY.
    DLD.RDP30
    READY.
LNH

100 2

110 JOHN SEVIER ASH POND "J", R BAR TEST 9 STA. 41+75

120 024,0.05

130 -9399,-49,-112,-49,-1000,0,100,0,9999

140 -112,-49,9399,-49,-1100,-25,100,150,9999

150 -9399,-46.5,-110,-46.5,-62.4,0,0.0,0

160 -112,-49,-110,-46.5,-128,0,25,0,150

170 -110,-46.5,-105.5,-41.5,125,0,25,0,150

180 -105.5,-41.5,-100,-39.5,125,0,25,0,150

190 -100,-39.5,-86,-37,125,35,25,0,150

200 -86,-37,-67,-29,123,35,27,0,150

210 -100,-39.5,-85,-30,135,0,35,0,0

220 -85,-30,-67,-29,123,35,27,0,150

230 -67,-29,-60,-26,123,0,27,0,150

240 -60,-26,-8,0,123,0,27,0,150

250 -8,0,8,0,123,0,27,0,150

260 8,0,16,-4,123,0,27,0,150

270 16,-4,78,-35,-127,0,27,0,150

290 84,-38,9399,-38,-128,27,25,150,150

300 78,-35,84,-38,-128,27,25,150,150

310 16,-4,9399,-4,-62.4,0,0,0,0

320 -86,-37,-20,-35.5,125,27,25,150,150

330 -20,-35.5,5,-35,-128,27,25,150,150

350 -110,-46.5,-20,-35.5,-128,27,25,150,150

350 -110,-46.5,-20,-35.5,-128,27,25,150,150

370 49

380 8,-5,-40,-35
    LMH
    100 2
  380 8,-5,-40,-35
  390 40,20,120,80,5,5,5
  400 0,0
 410 8,-10,-70,-45
 420 25,25,125,100,5,5,5
430 0,0
READY.
FTM
FEADY.
OLD.SLOPE2
READY.
GET. TAPE5=RDP30
READY.
FUN
                                                                                                   Les Phreche Suntace
   84/07/11. 14.11.17.
ROGRAM SLOPE2
PROGRAM
110 JOHN SEVIER ASH POND "J", R BAR TEST & STA. (ERGF= .05 DEPTH OF ROCK= 49.0 FT)
```

THE MIN. FS= 1.46 EFS= 1.27 HXX2-100.00

THE MIN. EFS= 1.27 FS= 1.46 H(X)=100.00 G(Y)= 80.00 R= 128.71

RUN COMPLETE.

THESE HEE THE INPUT DHIH LIMES $\times 1$ $\forall 1$ XE YΞ F1 02 C1-9399.0 -49.0 -112.0 9999.0 -49.0 -1000.0 0.0100.0 0.0 -49.0 -1000.0 -49.0 -1000.0 -46.5 -62.4 -46.5 -128.0 -41.5 125.0 -37.0 125.0 -29.0 135.0 -30.0 135.0 -49.0 -46.5 9399.0 25.0 0.0 -112.0 -1000.0 -62.4 -125.0 125.0 125.0 125.0 125.0 123.0 123.0 123.0 123.0 -128.0 -128.0 150.0 100.0 9999.0 -110.00.0 -9399.0 $\theta \cdot \theta$ 150.0 150.0 150.0 -112.0 -49.0-110.00.00.0-441.55.05.6 -441.55.05.6 -497.05.6 -110.0-105.50.0 0.0-105.5 -100.0 0.0 0.0-85.0 -85.0 -67.0 -67.0 35.0 35.0 -100.0150.0 0.0-86.0 0.0150.0 ō.o -100.0 0.00.0-30.0 -29.0 -26.0 -85.0 -67.0 -29.0 0.00.0 0.0 -26.0 150.0 0.00.0 -60.0 -8.00.0 150.0 0.0Û.Û 150.0 150.0 -8.0 0.0 8.0 Ú.Ú 0.00.0 16.0 78.0 -4.0 8.0 0.00.0 0.0 -35.0 -38.0 -38.0 150.0 150.0 -4.0 0.0 27.0 27.0 16.0 0.0-35.0 -38.0 -35.0 84.0 78.0 150.0 -128.0 -127.0 -62.4 84.0 9399.0 150.0 150.0 78. Q 9399.0 0.0 150.0 0.0 -4.0 -37.0 -35.5 -35.0 -46.5 -35.0 -35.0 -35.0 -35.0 -35.0 9399.0 16.0 0.00.00.0 0.0125.0 -128.0 -128.0 27.0 27.0 27.0 27.0 25.0 27.0 25.0 25.0 25.0 25.0 27.0 -86.0 -20.0 150.0 150.0 5.0 78.0 -20.Q 150.0 150.0 150.0 150.0 5.0 -110.0 -128.0 -127.0 150.0 150.0 -20.0 -20.0 16.0-4.0150.0 150.0 XT =8.0 YT =-5.0XB = -40.0YE= -35.020.0 GRIDX= 40.0 GRIDY= XMAX= 120.0 YMAX= 80.0 INCX= 5 INCY= 5 INCR= 5 THE MAXIMUM F.S. TO BE PRINTED IS 0.00THE MAXIMUM E.F.S. TO BE PRINTED IS

TEST POINTS

THE MIM. FS= 1.75 EFS= 1.40 H(X) =60.00 5(Y) =R= 67.69 30.00 THE MIN. EFS= 1.39 FS= 1.75 65.04 H(X) = 60.00G(Y) = -25.00 R=

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

X1	Y1	XS	Y2	W	F2	F1	C2	01
9399.0 112.0 9399.0 110.0 105.5 100.0 86.0 100.0 85.0 67.0 67.0 -88.0 -16.0 -78.0 -78.0 -16.0 20.0 110.0 20.0	-46.5 -49.0 -46.5 -49.5 -39.0 -39.0 -39.0 -26.0 -4.0 -35.0 -35.0	112.0 -9399.0 110.0 110.0 105.5 100.0 67.0 68.0 -8.0 -16.0 -784.0 -9399.0 -784.0 -9399.0 -78.0 -78.0 -78.0 -78.0 -78.0 -78.0	-49.0055555000000000000000000000000000000	-1000.0 -1000.0 -1000.0 -62.4 -128.0 125.0 125.0 125.0 123.0 123.0 123.0 123.0 -127.0 -128.0 -127.0 -128.0 -127.0 -128.0 -127.0 -128.0 -127.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	100.0 100.0 05.0 05.0 05.0 05.0 05.0 0 05.0 0 0 0	0.0 150.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 150.0 150.0 150.0 150.0 150.0	9999.0 9999.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0

XT =8.0 YT = -10.0XB = -70.0YB = -45.0GRIDX= 25.0 GRIDY= 25.0 XMAX= 125.0 YMAX= 100.0 INCX= INCY= 5 INCR= 5 THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS

TEST POINTS

SBU LIMIT ENTER S TO CONTINUE OR CR KEY TO STOP: S,1000

THE MIN. FS= 1.46 EFS= 1.27 H(X) = 100.00 G(Y) = 80.00 R= 128.71 THE MIN. EFS= 1.27 FS= 1.46 H(X) = 100.00 G(Y) = 80.00 R= 128.71 SBU 303.892 UNTS.

RUN COMPLETE.

DP30

7 -86,-37,-82,-37,125,27,25,150,150

7 -86,-37,5,-35,-128,27,25,150,150

9 -82,-37,5,-32,-37,-128,25,25,150,150

10 -110,-46.5,-82,-37,-128,25,25,150,150

40 -82,-37,16,-4,-127,27,27,150,150

410 8,-5,-70,-45

420 25,15,120,120,5,5,5

REPLACE
READY.
FIN FTH READY. DLD.SLOPE2 READY. GET. TAPE5=RDP30 High Mirectic Surface

C = 150

No Add time 1 Riphys 84/07/11. 14.25.37. PROGRAM SLOPE2 110 JOHN SEVIER ASH POND "J", R BAR TEST @ STA. (EROF= .05 DEPTH OF ROCK= 49.0 FT) THESE ARE THE IMPUT DATA LINES $\times 1$ Y1 F1 X2 Y2 C2 C1 -49.0 -1000.0 -49.0 -1000.0 -46.5 -62.4 -46.5 -128.0 -41.5 125.0 -39.5 125.0 -37.0 123.0 -29.0 135.0 -29.0 123.0 -29.0 123.0 -29.0 123.0 -29.0 123.0 0.0 123.0 0.0 123.0 -49.0 0.0 25.0 0.0 -9399.0 -112.0 9399.0 0.0 100.0 100.0 9999.0 15<u>0.0</u> -112.0 -9399.0 -112.0 ģģģģ. -110.0-628.0 -1285.0 -1285.0 -1285.0 -1285.0 -1285.0 -1285.0 -1285.0 -1285.0 -1285.0 -1285.0 -1285.0 -1286.0 0.0 0.0 0.0 -110.00.0 150.0 0.0-110.0 -110.0 -105.5 -100.0 -86.0 -100.0 -85.0 -40 0.0150.0 0.0 Ò.Q 150.0 150.0 150.0 0,0 35.00.00 0.0 0.0 0.0 0.0 150.0 0.0150.0 150.0 150.0 150.0 150.0 -60.0 0.0 0.0 78.0 16.0 16.0 78.0 84.0 16.0 0.0 Õ.Õ 0.00 -4.00 -5.88.00 -3.88.54.00 -3.85.47.55.74 0.0 0.0 0.0 0.0 0.0 27.0 27.0 0.0 27.0 27.0 227.0 150.0 150.0 0.0 150.0 $0 \cdot 0$ -86.0 -82.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 -110.0 150.0 -82.0 16.0 -4.0150.0 XT =8.0 YT = -5.0 $\times E = -40.0$ YB= -35.0 GRIDX= 40.0 GRIDY= 20.0 XMAX= 120.0 YMAX= 80.0 INCX= 5 INCY= INCR= THE MAXIMUM F.S. TO BE PRINTED IS 0.00 THE MAXIMUM E.F.S. TO BE PRINTED IS

TEST POINTS

THE MIN. FS= 1.69 EFS= 1.35 H(X)= 60.00 G(Y)= 30.00 R= 67.69

THE MIN. EFS= 1.35 FS= 1.70 H(X)= 60.00 G(Y)= 25.00 R= 65.04

FOR SIDE TWO

THESE ARE THE INPUT DATA LINES

$\times 1$	Y1	X2	Y2	ایرا	F2	F1	C2	C 1
939.0 112.0 112.0 110.0 110.0 100.0 100.0 60.0 100.0 60.0 -16.0 -16.0 -16.0 -16.0 82.0 -10.0 83.0 110.0 83.0	00050555050000000000000000000000000000	112.0 -939.0 110.0 110.0 110.0 105.0 67.0 687.0 687.0 68.0 -168.0 -1784.0 -1784.0 -93999.0 -782.0 -186.0 -186.0	9.66197.900.600.00000000000000000000000000000	-1000.0 -1000.	05000000000000000000000000000000000000	00000000000000000000000000000000000000	0.0 150.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	9999.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0
							4	

XT= 8.0 YT= -5.0 XB= -70.0 YB= -45.0

GRIDX= 25.0 GRIDY= 15.0 XMAX= 120.0 YMAX= 120.0

INCX= 5 INCY= 5 INCR= 5

THE MAXIMUM F.S. TO BE PRINTED IS 0.00

THE MAXIMUM E.F.S. TO BE PRINTED IS 0.00

TEST POINTS

+SBU LIMIT+ ENTER S TO CONTINUE OR CR KEY TO STOP: S,1000

THE MIN. FS= 1.13 EFS= .97 H(X)= 95.00 G(Y)= 90.00 R= 138.83 THE MIN. EFS= .97 FS= 1.13 H(X)= 80.00 G(Y)= 55.00 R= 103.73 SBU 436.113 UNTS.

